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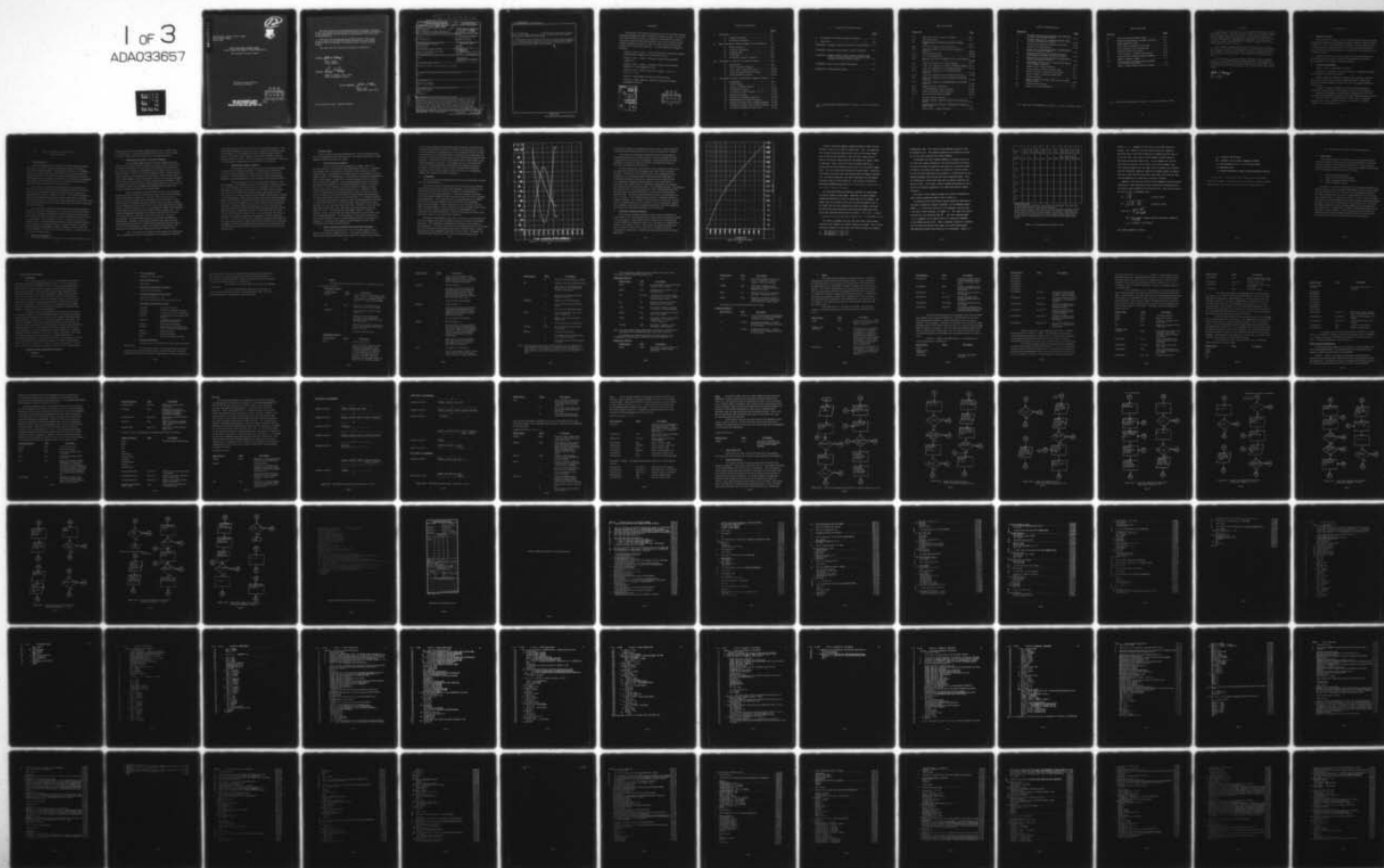
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October 1976

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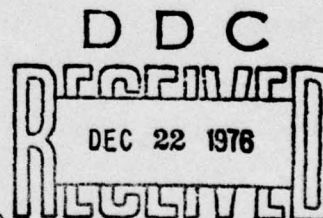


SPACE SURVEILLANCE SOFTWARE SUPPORT  
Project Summary and Computer Program Documentation

PRC Information Sciences Company

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ROME AIR DEVELOPMENT CENTER  
AIR FORCE SYSTEMS COMMAND  
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| 20. ABSTRACT (Continue on reverse side if necessary and identify by block number)<br>The objective of this effort was to modify the RADC trajectory program orbit program and various radar cross section programs were modified to run on the RADC HIS 6180 computer under the GCOS system software. The RADC trajectory program was modified to include the capability of processing multiple (20) radar sites and multiple (20) targets in the program so that various radar parameters could be determined. This type of information is essential in performing radar coverage analyses for systems such as COBRA TALON, SEEK SAIL, COBRA DANE and COBRA JUDY. This portion of the effort is documented in Vol 1. |  |   |

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Line 20 (continued)

Vol <sup>2</sup>VI documents a procedure for punching cards in ASCII format and reading the data onto a HP cassett for subsequent plotting with an HP9820 calculator system.

Vol <sup>3</sup>LII documents some Radar Signature and Radar Scattering computer programs. A three dimensional plot program contained in this volume has been incorporated into the Interactive Radar Simulator for plotting three dimensional antenna patterns and cross section aspect angle histories.



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## ABSTRACT

The objective of the effort documented herein was to provide computer programming support for Space Surveillance system analysis. The two primary tasks of the effort were to complete the modification of the RADC Trajectory Program and to modify various radar cross-section and other computer programs so that they could be accessed from the interactive system for the RADC Radar Simulator. The documentation is organized as follows:

Volume I, Part 1, Book 1 - Project Summary and Computer Program Documentation (Chapters I-III of Volume I, Part 1)

Volume I, Part 1, Book 2 - Computer Program Documentation (Chapter IV)

Volume I, Part 1, Book 3 - Computer Program Documentation (Chapters V-VI and Appendices A-E)

Volume I, Part 2 - RADC Trajectory Program - Numerical/Analytical Data

Volume II - Generalized Data Entry and Plot Program

Volume III - Radar Signature and Radar Scattering Principles Investigation Software

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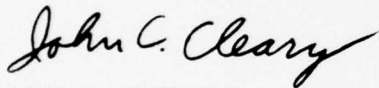
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## EVALUATION

The objective of this effort is to provide RADC systems engineers with the software commonly required for systems studies and the necessary software for plotting the data. The RADC trajectory program was modified to handle multiple targets and multiple radar sites. This program is required to perform coverage analyses for radar surveillance systems and has been used in support of SEEK SAIL, COBRA TALON and COBRA DANE. The cross section programs are used to determine the cross sections of targets that a radar system would be required to detect.

Since the RADC computer facility does not have a means of plotting data, most of the computer data generated was of limited value and extremely time consuming to use. Vol II documents a procedure for punching cards in ASCII format and reading data onto an HP cassette for subsequent plotting with an HP 9820 calculator system. This capability has proven extremely useful.

Vol III documents some Radar Signature and Radar Scattering computer programs. A three dimensional plot program contained in this volume has been incorporated into the Interactive Radar Simulator for plotting three dimensional antenna patterns and imaged wideband cross section data. These programs can serve as a starting point in the Tactical Target Identification Program.



JOHN C. CLEARY  
Project Engineer

## I. Introduction

### A. Purpose and Scope

This document is Volume I, Part 1 of the technical report and computer program documentation for the Space Surveillance Software Support Contract, F-30602-75-C-0167, and is submitted in fulfillment of items A002 and A003 of the contract data requirements list. The work represented herein has been performed by Information Sciences Company (ISC) of Planning Research Corporation (PRC).

Contained herein are a summary of the work done on the project in the modification of the RADC Trajectory Program and others and the documentation for all computer programs modified.

### B. Document Organization

Volume I, Part 1 is organized as follows:

Chapter II is, basically, the project summary. Appropriate exhibits are interleaved with the text material.

Chapters III and IV contain descriptions of the trajectory computer programs and radar cross-section computer programs, respectively. Included are source listings, sample test cases, and sample output from the test cases.

Chapter V contains descriptions of several auxiliary programs developed during the project, while chapter VI gives a list of references.

Appendices A through E contain analyses relating to the trajectory programs and descriptions of several small radar simulation-type programs.

Volume I, Part 1 is subdivided into 3 Books, Book 1 containing Chapters I-III, Book 2 containing Chapter IV, and Book 3 containing Chapters V-VI and Appendices A-E.

## II. Space Surveillance Software Support Project Summary

### A. Project Overview

The essential purpose of the Space Surveillance Software Support project was to provide computer programming support to aid Space Surveillance system analysis. This support took the form of modifying numerous, existing trajectory and radar-cross section programs and implementing them on the Honeywell 635 and 6180 computers at RADC. These programs were written in FORTRAN Y and placed in the appropriate time-sharing CARDIN format so that they could be accessible from the interactive system for the RADC Radar Simulator.

The work on the project was divided into two major task areas. One of these tasks was to bring the modification of the RADC Trajectory Program to a completion; the initial modification of the program was performed under Contract F30602-72-C-0136. This second modification included the capability of processing multiple radar sites and multiple targets in the program so that various radar parameters could be determined. The trajectory program can now accommodate up to 20 different radar sites and up to 20 targets.

The second task consisted of the modification and implementation of a number of trajectory, target model, and radar cross-section programs. There were 12 programs, altogether, involved in the task, and they were made executable via the remote batch system (CARDIN) of the RADC Honeywell computers. The 12 programs were the: Cobra Talon Trajectory Program, Nodal Crossing Prediction Program, Orbit Prediction Program, Cone Program, Cone-Cylinder Program, Frustum Program, Frustum-Cylinder Program, Hemisphere-Cylinder Program, Radar Scatter from Missile Program, Dihedral Corner Reflector Program, Cylinder Program, and Cylinder-Flare Program.

### B. Program Development

The required modifications to the various computer programs and their



implementation on the Honeywell computing system were carried out in a certain manner. The procedure followed with respect to the two major tasks of the project will be described in the following paragraphs.

1. Modification of the RADC Trajectory Program

It was realized initially that the plotting capability had to be restored to the RADC Trajectory Program in order to make full use of it. The XYNECTICS plotter, by which plots of radar data were produced for the version of the program as modified under the original contract, was no longer available. However, the Hewlett-Packard 9820A calculator/plotter, with the capacity to read data cards was available. What was done was to write a short program to read the plot file created by the trajectory program and to punch out the file data onto cards for plotting on the HP9820A. This short program served as the basis of another plot program which could read the plot file created by the multiple site/multiple target version of the trajectory program and which was used quite often.

After checking that the first modified version of the trajectory program executed correctly, a detailed flow-chart of the major processing within the program was drawn up. This flow-chart was to serve as a basic reference for making further modifications to the program. It was thought that the modification involving multiple radar sites would be easier (less complicated) to include first in preference to that involving the multiple targets, and this is what was done. The multiple site addition was thoroughly tested using the results produced from prior, valid computer runs. The additional capability of printing out a message to the effect that an object was not detected by a radar site, when this was the case, was also incorporated. Next, the multiple target (or trajectory) capability was implemented. Basically, this involved putting an outer loop around the processing of the program; the multiple site modification had been made to process a single target only. Again, the multiple target addition to the program was carefully checked using previous, good computer runs.

After check-out of the multiple target/multiple site modification, other capabilities were added to the program. An atmospheric model for

simulating atmospheric effects on missiles was included and tested. This model was essentially the one that was in the original, unmodified version of the program. The generation of circular orbit trajectories with the program was tested, and the option to select either inertial velocity or burnout velocity was added. Finally, inclusion of radar parameter difference computations for multiple sites and trajectories was worked on.

## 2. Modification of Other Programs

The discussion here generally refers to all programs modified except the RADC Trajectory Program. These programs consisted of 3 trajectory-type programs and 9 target model or radar cross-section programs. The basic procedure which was followed in modifying these programs and implementing them on the Honeywell system is given below.

The existing source deck for a program was loaded on a disc file, compiled, and compilation errors were eliminated. Routines common to several programs were removed from the programs and processed separately. An attempt was then made to execute the error-free object form (also on a disc file) of the program using a given input test case. The results were compared against results obtained from previous, reliable runs of the program. If the results compared favorably, then the program inputs were converted to NAMELIST format, where it had not already been done so, in order to facilitate the use of the CARDIN system for program execution. When the results did not check out, a search was made for program and/or load errors, and after being found and corrected, then the input conversion to NAMELIST was made. The NAMELIST conversion was also tested through computer runs. The last thing that was done to a program was to produce plots of its computations as a final output and check-out. In most cases this meant adding a subroutine to the program to place the required data on a file so that it could be punched onto cards later. In addition, it should be mentioned that each program was executed in the CARDIN system by means of their respective job streams which had been placed on file.

### C. Program Usage

This is a general discussion indicating how to use the programs which have been implemented under this contract. The reader should refer to other chapters of this volume for more detail.

#### 1. RADC Trajectory Program

After the user selects the appropriate missile, radar, etc. input parameters, he must decide what input options to exercise. Basically, these options will be determined by what type of run he desires and what output he wants. Incidentally, in choosing values for the missile parameters (initial velocity, re-entry angle, etc.), the reader is referred to the appendices, Part 2 of this volume, section II.E, and other documents which may have been produced on the subject. By selecting appropriate values for the main processing switch, NSWTCH, and the plotting options, IPLOT1 or IPLOT2, the user can, for the most part, control the flow of a program execution and the output from it for immediate and/or later use. NSWTCH = 0 will cause the computation of trajectory parameters only, the printout of them, and the storage on a file of those needed for determining radar parameters. No radar computations will be made when NSWTCH = 0. By setting NSWTCH = 1, the program will produce trajectory data, storing appropriate parameters on a file as for NSWTCH = 0, and will calculate radar parameters (range, azimuth, etc.) for each of the input radar sites. NSWTCH = 2 will cause the generation of radar data, only, from trajectory data placed on file when NSWTCH = 0 or 1. By setting either plot option, IPLOT1 or IPLOT2, equal to .TRUE., the user can have radar data placed on a plot file for later access in producing plots. For this purpose, cards would be punched out from the file through the use of a short auxiliary program (1st program of Chapter V), and they would be plotted on the HP9820A by means of the Generalized Data Entry and Plot Program.

#### 2. Other Trajectory Programs and Target Model Programs

Most of these programs do not have any input options so that their use is relatively straight-forward. The possible exceptions are the Cobra Talon Trajectory Program which requires the setting of such switches



as those for selecting the nominal trajectory and inertial velocity and the Orbit Prediction Program which has a switch for putting data on a plot file. The basic procedure in running any one of the programs would be to choose desired values for the input parameters, enter them in the appropriate job stream file, and execute the job stream via CARDIN and the Honeywell 6180 computer. A plot file is created automatically when a target model (cross-section) program is executed. If one desires the file to be punched onto cards, the BPUNCH subsystem of CARDIN can be utilized as each file is written in BCD format. For the Cobra Talon and Orbit Prediction Programs, if it is desired to punch out their plot files, the appropriate auxiliary punch programs would be employed.

#### D. Conclusions

There are several accomplishments of this project which have resulted from the work performed:

The RADC Trajectory Program has been made into a more efficient tool for the performance of radar system analysis. It can now process up to 20 different radar sites and up to 20 targets (or trajectories) and determine radar coverage parameters. Data from multiple trajectories can be permanently stored on a file and used many times over for computing radar parameters. This would result in considerable saving of computer time as the trajectory generation is by far the most time-consuming process in the program. Plots of radar data can now be made on the HP 9820A calculator/plotter. Refer to Figure II-1 for an example of such a plot. Also, the RADC Trajectory Program has been implemented on the Honeywell 6180 CARDIN subsystem, so that it is executable by means of the interactive system for the RADC Radar Simulator.

The target model programs have been checked out on the Honeywell 635 and 6180 computers and made accessible through the remote batch CARDIN subsystem. The capability of storing data for plotting was also added to these programs. The Cobra Talon Trajectory Program had several corrections made to it while it was being implemented on the CARDIN system. It also was given the added capability to generate circular orbits. In addition, the Orbit Prediction Program (as well as the Cobra Talon Program) was



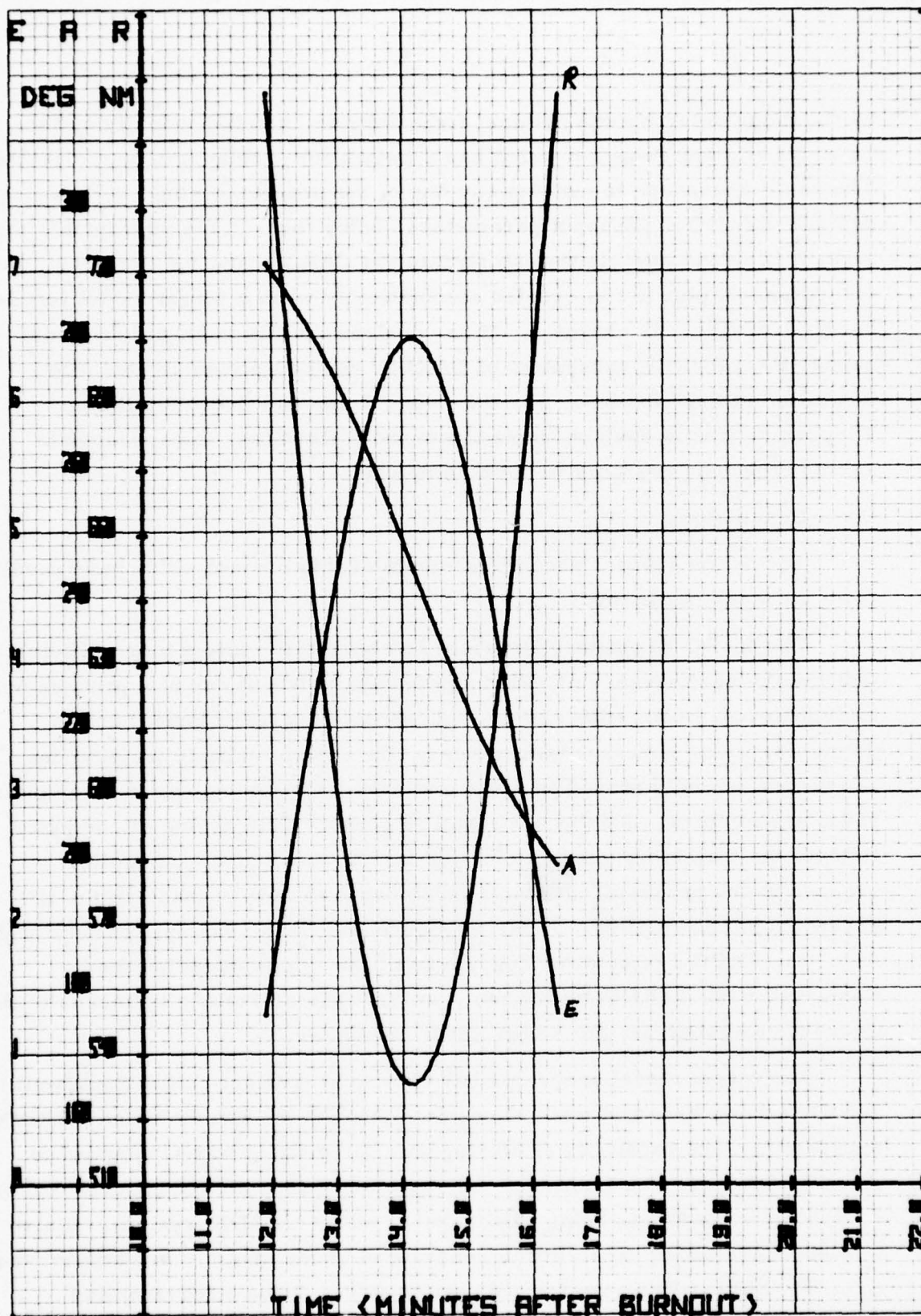


Figure II-1. Plot from RADC Trajectory Program

provided the capacity for obtaining plots of its results, and both it and the Nodal Crossing Prediction Program were made executable via CARDIN.

In the course of modifying and implementing the many programs involved in this project, several computer runs were attempted in which a spaceborne radar system was simulated. A plot from one of the runs, showing the decrease in range of a missile as it approaches impact at the radar, is illustrated in Figure II-2.

Several observations concerning the RADC Trajectory Program can be made; some of them may also apply to the Cobra Talon Trajectory Program. Most of the major trajectory and radar computations in the program are currently performed in double precision floating point. It might be worthwhile to perform an experiment on the program with the computations changed to single precision. If the experiment is successful, the benefit would be a significant reduction in both computer processing time and required memory. In the modified program, the trajectory data stored on file was in single precision; radar computations made with this data showed no noticeable difference from those made with double precision data. The basic integration time for trajectory iterations was set at 0.01 min. In the original program this time changed according to certain conditions, e.g., altitude of missile below a certain level. Results from the modified program were compared, in several instances, against corresponding results from the original program for which the integration time varied and no significant difference was discovered.

#### E. Trajectory Computer Programs

The trajectory computer programs deserve special attention here because they are the most important and widely used of the programs worked on for this project. This section could be considered as an introduction to their detailed description in chapter III and the analyses of Appendices A through E and Volume I, Part 2. Most of the following paragraphs have been excerpted from the "Cobra Talon Study Computer Programs" document (see References). Updates have been inserted in the text where appropriate.

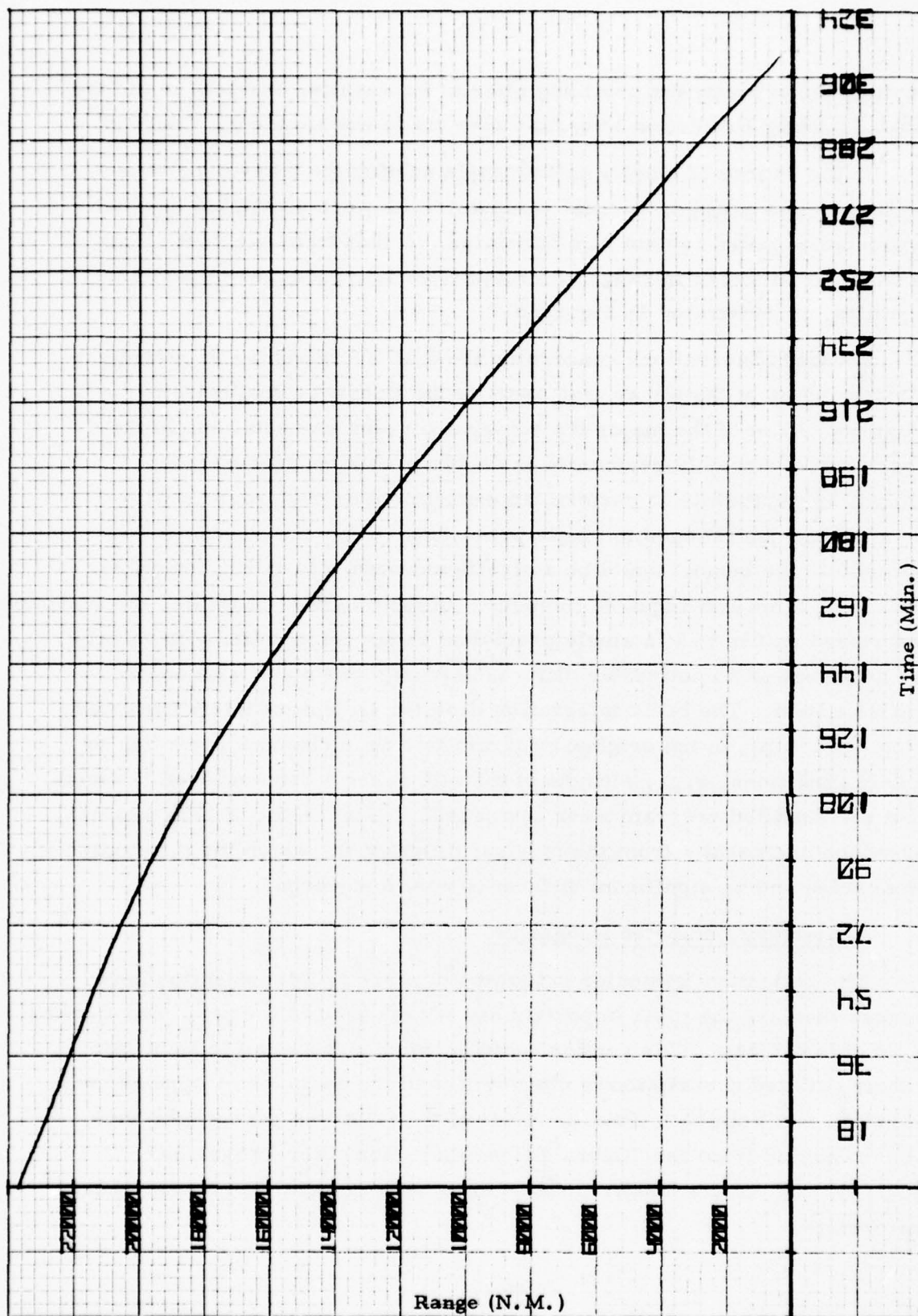


Figure II-2, Spaceborne Radar



A missile trajectory computer program developed at RADC\* had been modified to zero-in on a specific impact point. This is accomplished by utilizing the position and velocity vectors at the actual impact point as new initial conditions. Then the actual impact point is moved to the desired impact point and run backwards to burnout, which is time zero. Thus, a new set of initial burnout conditions is obtained for the third trajectory which zeros in on the desired impact point. This is of particular interest for reentry radars. Additional trajectories can be run which are perturbed from the nominal trajectory (i.e., the third trajectory); the radar differences from the nominal trajectory (3rd) are then printed out. This option is obtained by setting the FORTRAN variable KZ=0 in the Cobra Talon Program and = F in the RADC Trajectory Program.

In a study which OCSA was required to perform, the launch point and missile capability were known. Therefore, the above computer program was modified\*\* so that the launch point was not changed. The impact point was allowed to stay where the missile capability put it. This means that the first trajectory was made the nominal trajectory. The second and third trajectories were skipped and additional trajectories were perturbed from the first trajectory. This option is obtained by setting KZ=1 in the Cobra Talon Program and = T in the RADC version.

The original program\*\*\* was such that every time initial burnout conditions were changed, the computer program was changed. This computer program was changed to accept input data without changing the computer

- \* See Reference 4, Page VI-2
- \*\* See Reference 3, Page VI-2
- \*\*\* See Reference 4, Page VI-2



program every time. This allows the time-sharing system to be used for production runs. The computer program was also modified to print-out all the input conditions for future reference.

To determine the radar coverage parameters a separate version of the trajectory computer program was utilized which prints the missile trajectory and radar coverage data every tenth of a trajectory minute. In addition, the radar slant range is printed out in nautical miles. For the case where differences are calculated, a second version of the computer programs prints out data for every trajectory minute. Also, the differences in radar slant range from the nominal trajectory are printed in feet. The original computer program was modified to calculate the total angular separation in the radar beam from the nominal trajectory.

The outputs of the computer program can be used to determine the radar systems information needed to fill in Table II-1 .

To simulate missile trajectories, burnout velocities referenced to the earth's surface are required; therefore, set the FORTRAN variable INERTL = 0. If satellite orbits are to be simulated, inertial velocities must be used; therefore, set INERTL = 1. This causes the earth's rotation ( $\omega$ ) to be subtracted from  $\dot{\lambda}$ , the total longitude angle velocity component of the vehicle which is in subroutine ICERBM(P) as the FORTRAN variable XD(3). When a simulated trajectory is required for a specified inclination (INC) angle, the missile heading angle BETA measured clockwise from north has to be calculated. Figure II-3

| LAUNCH<br>AZ     | INIT<br>DET<br>RANGE | MIN.<br>DET<br>RANGE | MAX<br>DET<br>RANGE | FINAL<br>DET<br>RANGE | MAX<br>EL<br>ANGLE | TOT<br>AZ<br>ANGLE | MAX<br>RANGE<br>RATE | MAX<br>EL<br>RATE | MAX<br>AZ<br>RATE | TOT<br>OBS.<br>TIME |
|------------------|----------------------|----------------------|---------------------|-----------------------|--------------------|--------------------|----------------------|-------------------|-------------------|---------------------|
| ° FR<br>TRUE NO. | NM                   | NM                   | NM                  | NM                    | DEG                | DEG                | NM/<br>SEC           | DEG/<br>SEC       | DEG/<br>SEC       | MIN                 |
| 100              |                      |                      |                     |                       |                    |                    |                      |                   |                   |                     |
| 120              |                      |                      |                     |                       |                    |                    |                      |                   |                   |                     |
| 170              |                      |                      |                     |                       |                    |                    |                      |                   |                   |                     |
| 190              |                      |                      |                     |                       |                    |                    |                      |                   |                   |                     |
| 200              |                      |                      |                     |                       |                    |                    |                      |                   |                   |                     |
| 230              |                      |                      |                     |                       |                    |                    |                      |                   |                   |                     |

EXPLANATORY NOTES:

1. Unless otherwise specified, the numbers in parenthesis list time (min. after burnout) at which value would be observed.
2. The total Az Angle is the az angle required by radar to observe missile from horizon to horizon (0.5° el. angle). The numbers in parenthesis indicate initial and final detection azimuths (true North) from radar site.
3. The Total Observation Time is the time target would be within radar field-of-view. In parenthesis are cited initial and final observation times.

TABLE -II-1. Radar Systems Information Chart

Section III. B. documents the PRC version of the RADC Trajectory Program. PRC's effort was directed towards making the program run more efficiently on HIS 6180 and making the program relatively easy to use for the user. This version of the program can handle multiple trajectories for multiple radar sites. To save computer run time the trajectories of interest can be stored on disc and/or magnetic tape. Then coverage parameters for the radar sites of interest can be handled. Since the trajectory simulation requires the greatest amount of computer time this is more efficient and allows other radar sites which may come into consideration at a later date to be easily included.

Appendix A discusses the ejection velocity geometry used for multiple trajectories. Other appendices discuss procedures for determining burn-out velocity input parameters for the missile case. The inertial velocity for orbital cases is determined from\*

$$V_I = \sqrt{\frac{\mu}{a}} \quad (\text{circular orbit})$$

$$V_I = \sqrt{\mu \left( \frac{2}{r} - \frac{1}{a} \right)} \quad (\text{elliptical orbit})$$

$$\text{where } r = \frac{a(1-e)^2}{1 + e \cos \theta}$$

$\theta$  = true anomaly = angular position along orbit referenced to perigee

$$\mu = 5.0675004 \times 10^{19} \text{ ft}^3/\text{min}^2$$

\* See "Radar Handbook" by Skolnik

$$\mu = 1.407639 \times 10^{16} \text{ ft}^3/\text{sec}^2$$

$$RE = 2.0925640 \times 10^7 \text{ ft (earth's equatorial radius)}$$

$$e = \text{orbit eccentricity ( } e = 0 \text{ for circular orbit)}$$

$$a = \text{semi-major axis}$$

$$r = \text{distance from earth's center to satellite/missile position}$$

Section III. C. documents the Cobra Talon version of the RADC Trajectory Program. This version has the capability of handling multiple targets ejected from the nominal trajectory for a single radar site.



### III. Description of Trajectory Computer Programs

#### A. Introduction

This section provides a description for four (4) simulation-type computer programs which have been written in FORTRAN Y to execute under the Honeywell 6180 GCOS operating system. These programs, basically, generate trajectories for missiles and satellites and determine radar coverage parameters and are the following:

1. RADC Trajectory Program
2. Cobra Talon Trajectory Program
3. Nodal Crossing Prediction Program
4. Orbit Prediction Program

Program 1 is a second modification of the general perturbation program of George A. Ellis, the initial modification of which was done under Contract F30602-72-C-0136. Program 2 is essentially the version of Mr. Ellis' program which was used in conjunction with the Cobra Talon radar study by John C. Cleary and Leonard C. Gratch. Refer to sections III. B and III. C for documentation and further references on these programs. Programs 3 and 4 were developed under the direction of Mr. Cleary for predicting the path of an earth-orbiting satellite and determining radar look-angles for it. Sections III. D and III. E document these programs and mention a reference for them. All the programs have been put in the appropriate time-sharing CARDIN format by PRC/ISC so that they are executable by means of the RADC Interactive Radar Simulator.

## B. RADC Trajectory Program

### 1. Introduction

This computer program is a second modification of the general perturbation program (PROGRAM TRAJ) of George A. Ellis, previously modified under Contract F30602-72-C-0136. The previous modification retained much of the mathematics and basic processing methodology of the Ellis program but differed primarily in its input/output capabilities and increased modularity. More input flexibility and capacity for generating trajectory data (relative to a radar site) for use with an off-line plotter were major characteristics of the first modified version. This second refinement of the program brought the modification of the RADC Trajectory Program to completion. The capacity for accommodating multiple DSSR sites and multiple targets has been added to the program, while still maintaining the capabilities of the first modification.

The basic function of the program is to generate the trajectory of a ballistic missile or an earth-orbiting satellite. It predicts the position, velocity, and acceleration of the vehicle and can compute radar parameters (range, azimuth, elevation, etc.) relative to a number of radar sites. The user has the option of producing just trajectory data and no radar data, or both trajectory and radar data, or just radar data from trajectory data stored during a previous run. The reader is referred to a number of documents describing prior versions of the program. Several of these are: "Missile/Satellite Trajectory Program" April 1974, a user's guide by R. Conti, PRC; "Simulation Program for Three Degrees of Freedom Trajectories", Technical Memorandum No. EMA-TM-66-5, Sept. 1966, by George A. Ellis, et al; "Cobra Talon Study Computer Programs", Technical Memorandum RADC/OC-TM-71-4, May 1971, by John C. Cleary and Leonard C. Gratch. Also, refer to the analytical description in Volume I, Part 2 of this report.

### 2. Computer Program Operating Environment

#### a. Computer

Honeywell 6180.

b. Source Language

FORTTRAN Y under GCOS.

c. Memory Requirement

40K words.

d. Typical Processing Time Required

0.12 hours (432 seconds)

e. Peripheral Equipment Requirement

One disc file (file code: 08)

Three disc or tape files (file codes: 09, 10, 11)

f. Non-system Subroutines Required

|        |   |
|--------|---|
| ATMOSP | Atmospheric model.  |
| BALCOF | Ballistic coefficient subroutine.                                 |
| CONVER | Conversion to radar coordinates.                                  |
| EQTNX  | Computation of acceleration components.                           |
| ICERBM | Computation of geocentric spherical components.                   |
| INITAL | Initialization subroutine.  |
| INTRAJ | Input trajectory and radar data stored on files for computations. |
| INPUT  | Input subroutine.   |
| OUTPUT | Output subroutine.  |
| RKG    | 4th Order Runge-Kutta-Gill.                                       |

g. Program Limitations

The program can accommodate no more than 20 perturbed trajectories.

The maximum number of trajectories which can be generated will vary with the selection of the nominal trajectory. When the nominal trajectory for the trajectory perturbations is the first trajectory,

the first trajectory and up to 20 perturbed trajectories can be generated, for a total of 21. When the nominal trajectory is the third trajectory, there will be generated the first, backward, and third trajectories, and up to 20 perturbed trajectories, for a total of 23.

The program can accommodate no more than 20 different radar sites.

For the radar parameter difference calculations, no more than 10 different trajectories, 10 different radar sites, and 5 different sightings of a trajectory by a site are allowed.



### 3. Inputs

The following two sets of inputs (INPUT1 and INPUT2) are for the program controls.

#### NAMelist INPUT 1

| <u>Symbol Name</u> | <u>Units</u> | <u>Description</u>  |
|--------------------|--------------|---|
| NTRAJ              | None         | Total number of trajectories simulated. If KZ = T, the actual number of trajectories simulated will be NTRAJ-2. NTRAJ cannot exceed 23. |
| TM                 | Min.         | Maximum time allowed for any trajectory from start to finish.   |
| NSWTCH             |              | Main processing switch for the program.   |
|                    | 0            | Produce trajectory data only. The data for each trajectory generated will be placed on a file for later access.                         |
|                    | 1            | Produce both trajectory and radar data. The trajectory data will be placed on a file.   |
|                    | 2            | Produce radar data only.  |

#### NAMelist INPUT 2

| <u>Symbol Name</u> | <u>Units</u> | <u>Description</u>   |
|--------------------|--------------|--|
| IOUT1              |              | Printout option No. 1.   |
|                    | T            | Print out the 13 trajectory parameters from the radius of the missile (or satellite) trajectory to the acceleration in longitude for each time point of each trajectory. The time points are spaced by OUTINC, and each trajectory is considered relative to a geocentric coordinate system. |

| <u>Symbol Name</u> | <u>Units</u> | <u>Description</u>  |
|--------------------|--------------|---|
|                    | F            | Print out the 7 trajectory parameters from the radius to atmospheric density for each time point of each trajectory generated.  |
| IPLOT1             |              | Plotting option 1.  |
|                    | T            | Produce a plot file of the 8 radar parameters from slant range to inertial phi for each time point each detected trajectory. This plot file consists of data produced from all input radar sites.                       |
|                    | F            | Do not produce this plot file.  |
| IPLOT2             |              | Plotting option 2.  |
|                    | T            | Produce a plot file of the 13 radar, parameters (calculated for each site) from slant range to heading angle for each time point of each detected trajectory.   |
|                    | F            | Do not produce this plot file.  |
| IOUT2              |              | Printout option 2.  |
|                    | T            | Print out the 13 radar parameters from slant range to heading angle for each time point of each detected trajectory. The radar parameters of each trajectory are computed relative to the input radar site coordinates. |
|                    | F            | Print out the 8 radar parameters from slant range to the inertial phi angle for each time point of each detected trajectory.  |
| KAT                |              | Atmospheric model option.   |
|                    | T            | Use the atmospheric model. Atmospheric effects will be considered in the generation of the trajectories.  |

| <u>Symbol Name</u> | <u>Units</u> | <u>Description</u>  |
|--------------------|--------------|---|
| KZ                 | F            | Do not use the atmospheric model.   |
|                    |              | Nominal trajectory selection switch.  |
|                    | T            | Select the 1st trajectory as the nominal trajectory for the trajectory perturbations. |
| SPHERE             | F            | Select the 3rd trajectory as the nominal trajectory.                                  |
|                    |              | Spherical earth model option.   |
|                    | T            | Use the spherical model of the earth.   |
| IOUT3              | F            | Do not use the spherical model.   |
|                    |              | Printout option for radar parameter differences.                                      |
|                    | T            | Print out the radar parameter differences.  |
| OUTINC             | F            | Do not print out the differences.   |
|                    | Min.         | Increment between time points for printout.   |
|                    |              | Inertial velocity option.   |
| INERTL             | T            | The initial missile velocity input is the inertial velocity.                          |
|                    | F            | The initial velocity is the burnout velocity.   |

Note: The spherical model of the earth is the only one currently present in the program, so that the value of SPHERE has no effect on a program run. Also, IPLOT1 and IPLOT2 cannot be simultaneously true. Only one can be true and the other false, or both can be false.

The following set of inputs are for the initial state vector of the interceptor and the subsatellite parameters.

#### NAMelist INPUT3

| <u>Symbol Name</u> | <u>Unit</u> | <u>Description</u>  |
|--------------------|-------------|---|
| GAM                | Deg.        | Re-entry angle of the missile with respect to the vertical.                               |
| BETA               | Deg.        | Heading angle of missile w.r.t. relative north.   |
| VO                 | Ft./Sec.    | Velocity of the missile relative to burnout at epoch or inertial velocity of the missile. |
| HX                 | Ft.         | Height of missile at burnout or initialization of trajectory.                             |
| THE                | Deg.        | Geocentric latitude at burnout, + north and - south of equator.                           |
| GLAM               | Deg.        | Geocentric longitude at burnout, east of Greenwich.                                       |
| THES               | Deg.        | Geocentric latitude of the target (subsattellite), + north and - south of equator.        |
| GLAMS              | Deg.        | Geocentric longitude, east of Greenwich, of the target.                                   |

Note: The inputs GAM through GLAM above could also be interpreted as parameters for an orbiting satellite, rather than a missile.

The following set of inputs describes the radar sites for which computations are to be made. INPUT4 is not read if NSWTCH = 0.

#### NAMelist INPUT4

| <u>Symbol Name</u> | <u>Unit</u> | <u>Description</u>   |
|--------------------|-------------|--|
| NSITE              | None        | The number of radar sites to be simulated. NSITE cannot exceed 20. |



| <u>Symbol Name</u> | <u>Unit</u> | <u>Description</u>  |
|--------------------|-------------|---|
| SLAT               | Deg.        | Geocentric latitudes of the radar sites, + north and - south of equator. SLAT is an array.        |
| SLONG              | Deg.        | Geocentric longitudes of the radar sites, west of Greenwich. SLONG is an array.                   |
| SALT               | Ft.         | Altitudes of the radar sites above sea level. SALT is an array.                                   |
| ELIM               | Deg.        | Maximum co-latitude of the elevation angle for which objects are detected by all the radar sites. |

If NTRAJ > 3, the velocity perturbations are input:

NAMelist INPUT5

| <u>Symbol Name</u> | <u>Unit</u> | <u>Description</u>  |
|--------------------|-------------|---|
| A                  | Ft./Sec.    | Out of trajectory plane perturbation, + ejected to the left of the nominal trajectory. A is an array. |
| B                  | Ft./Sec.    | In plane perturbation, + ejected backwards from nominal trajectory. B is an array.                    |
| C                  | Ft./Sec.    | In plane perturbation, + ejected backwards from nominal trajectory. C is an array.                    |

#### 4. Output

The output from the RADC Trajectory Program is a variable depending upon the selection of the program options. First, a printout of the input parameters for the program run is produced, this printout and the input parameters, themselves, varying according to the values of the options. Then follows the printout of the results of the program execution. The main processing switch for the program (NSWTCH) has a great deal of control over the type of output coming from the program. If NSWTCH=0, only trajectory data will be printed out. If NSWTCH=1, both trajectory and radar data will be produced. And if NSWTCH=2, only radar data will be outputted. The following lists indicate what printout is produced with what option values.

When NSWTCH=0 or 1 and IOUT1=.FALSE., the following printout of trajectory parameters for every trajectory generated is produced:

| <u>Symbol Name</u>      | <u>Units</u> | <u>Description</u>  |
|-------------------------|--------------|---|
| NTRJ                    | None         | Number of trajectory. When KZ=T, the second trajectory will be numbered 4.  |
| TIME1+(I/IO)<br>*OUTINC | Min.         | Formula for the calculation of a trajectory time point for printout. The value calculated (and printed out) represents the time from burn-out of the missile along its trajectory or time from the initiation of the satellite orbit or missile path, if that is appropriate. |
| OUTTRJ(1)               | Ft.          | Earth-centered radius of the trajectory or the distance of the missile or satellite from the earth center at the time point above.  |

| <u>Symbol Name</u> | <u>Units</u>           | <u>Description</u>   |
|--------------------|------------------------|--|
| OUTTRJ(2)          | Deg.                   | Position in latitude of the missile/satellite in its trajectory at the above time point. |
| OUTTRJ(3)          | Deg.                   | Position in longitude of the missile/satellite, east of Greenwich.                       |
| OUTTRJ(4)          | Ft.                    | Altitude above sea level of the missile.   |
| OUTTRJ(5)          | Ft./Sec.               | Inertial velocity of the missile/satellite along its trajectory.                         |
| OUTTRJ(6)          | Ft. <sup>2</sup> /Slug | Ballistic coefficient at the time point.   |
| OUTTRJ(7)          | Slug/Ft. <sup>3</sup>  | Atmospheric density at the trajectory time point for the missile/satellite altitude.     |

The trajectory parameters corresponding to the next time point to be printed out are stored in OUTTRJ(8) - OUTTRJ(14), and so on for each time point to be printed. NTRJ is printed at the top of a page of printout. The time point - OUTTRJ(7) are printed out on one line of a page, next time point - OUTTRJ(14) on the next line, etc., up to 52 lines per page. NTRJ will start the next page. Each successive time point printed out will differ by OUTINC from the previous one. This may not hold true for the very last time point as it may differ from the previous one by 0.01 min. or more.

If IOUT1 = .TRUE. and NSWTCH=0 or 1, the following trajectory parameters are printed out:

| <u>Symbol Name</u> | <u>Units</u> | <u>Description</u>               |
|--------------------|--------------|----------------------------------|
| NTRJ               |              |                                  |
| TIME1+(I/IO)       |              |                                  |
| *OUTINC            |              |                                  |
| OUTTRJ(1)          |              | Described for IOUT1 =<br>.FALSE. |

| <u>Symbol Name</u> | <u>Units</u>            | <u>Description</u>   |
|--------------------|-------------------------|--|
| OUTTRJ(2)          |                         |  |
| OUTTRJ(3)          |                         |  |
| OUTTRJ(4)          |                         |  |
| OUTTRJ(5)          |                         |  |
| OUTTRJ(6)          |                         |  |
| OUTTRJ(7)          |                         |  |
| OUTTRJ(8)          | Ft. /Sec.               | Geocentric radial velocity component of the missile/satellite at the time point. |
| OUTTRJ(9)          | Deg. /Sec.              | Geocentric latitude velocity component of the missile/satellite.                 |
| OUTTRJ(10)         | Deg. /Sec.              | Geocentric longitude component of velocity of the missile/satellite.             |
| OUTTRJ(11)         | Ft. /Sec. <sup>2</sup>  | Geocentric radial acceleration component of the missile/satellite.               |
| OUTTRJ(12)         | Deg. /Sec. <sup>2</sup> | Geocentric latitude component of acceleration of the missile.                    |
| OUTTRJ(13)         | Deg. /Sec. <sup>2</sup> | Geocentric longitude component of acceleration of the missile.                   |

What was said above for the printout when IOUT1 = .FALSE. essentially holds for IOUT1 = .TRUE. The difference is that storage of the trajectory parameters is not the same. The trajectory parameters corresponding to the next time point to be printed out are stored in OUTTRJ(14)-OUTTRJ(26), and so on for each time point to be printed out.

The number and types of trajectories generated are basically controlled by the input variables NTRAJ and KZ. If only one trajectory is desired, NTRAJ would be set equal to one. If perturbed trajectories are desired with the nominal trajectory as the first trajectory, NTRAJ would be set  $\geq 4$  and KZ = .TRUE. The trajectories on the printout would be



numbered in the order 1, 4, 5, \_ \_ \_ , number 4 representing the first perturbed trajectory. If perturbed trajectories are desired with the nominal trajectory as the third trajectory, NTRAJ would be set  $\geq 4$  and KZ = .FALSE. In this case the trajectories would be numbered 1, 2, 3, 4, \_ \_ . Trajectory 2 is the so called "backwards" trajectory, with time going in descending order.

Now if NSWTCH = 1 or 2, the following set of radar parameters will be printed out for each radar site and each trajectory detected by the sites. For NSWTCH=1, the radar data will follow the appropriate trajectory data printout. For NSWTCH=2, there will be no trajectory data printout, only radar data. There will be no radar data printout for the second trajectory and if a trajectory is not visible to a radar site, a message to that effect will be produced. For IOUT2 = .FALSE., the radar parameters printed out are:

| <u>Symbol Name</u>       | <u>Units</u> | <u>Description</u>   |
|--------------------------|--------------|--|
| NTRJ                     | None         | Trajectory number.   |
| ISITE                    | None         | Radar site number.   |
| SC1                      | Deg.         | Position in latitude of the radar site.  |
| SC2                      | Deg.         | Position in longitude of the radar site.   |
| TIME2+(I/IO1)<br>*OUTINC | Min.         | Trajectory time point. See description for IOUT1 = .FALSE. under trajectory data output. |
| OUTRAD(1)                | N. M.        | Radar slant range to the missile/satellite for the time point.                           |
| OUTRAD(2)                | Ft. /Sec.    | Slant range rate for the time point.   |
| OUTRAD(3)                | Deg.         | Radar elevation angle for the missile/satellite at the time point.                       |
| OUTRAD(4)                | Deg. /Sec.   | Elevation angle rate.  |

| <u>Symbol Name</u> | <u>Units</u> | <u>Description</u>                                  |
|--------------------|--------------|---|
| OUTRAD(5)          | Deg.         | Radar azimuth angle, measured clockwise from north. |
| OUTRAD(6)          | Deg./Sec.    | Azimuth angle rate.                                 |
| OUTRAD(7)          | e.r.u.       | Trajectory radius in earth radii units.             |
| OUTRAD(8)          | Deg.         | Inertial phi angle.                                 |

The radar parameters corresponding to the next time point to be printed out are stored in OUTRAD(9)-OUTRAD(16), and so on for each time point to be printed. NTRJ, ISITE, SC1, SC2 are printed at the top of a page of printout. The time - OUTRAD(8) are printed out on one line of a page, next time point - OUTRAD(16) on the next line, etc., up to 52 lines per page. NTRJ, ISITE, SC1, SC2 will start the next page. Each successive time point printed out will differ by OUTINC from the previous one, except that the difference between the first and second time points and the next-to-last and last could be less than OUTINC.

What was said in the previous paragraph applies to one sighting of the missile/satellite by a radar site. Each sighting of the missile/satellite by a site will have a group of printouts similar to what is described above. The first time printed out for a group represents the initial time of sighting by the radar for the current sighting (or current period in which the missile/satellite is in the radar coverage). The last time represents the time at which the missile was last visible to the radar for the current sighting. The printout of radar parameters, in this way, can reflect when a missile moves in and out of the radar coverage.

When IOUT2 = .TRUE.' and NSWATCH=1 or 2, the following radar parameters are printed out:

| <u>Symbol Name</u> | <u>Units</u> | <u>Description</u> |
|--------------------|--------------|--------------------|
| NTRJ               |              |                    |
| ISITE              |              |                    |
| SC1                |              |                    |
| SC2                |              |                    |

| <u>Symbol Name</u>       | <u>Units</u>            | <u>Description</u>  |
|--------------------------|-------------------------|---|
| TIME2+(I/IO1)<br>*OUTINC |                         | Described under IOUT2 =<br>. FALSE.                           |
| OUTRAD(1)                |                         |   |
| OUTRAD(2)                |                         |   |
| OUTRAD(3)                |                         |   |
| OUTRAD(4)                |                         |   |
| OUTRAD(5)                |                         |   |
| OUTRAD(6)                |                         |   |
| OUTRAD(7)                |                         |   |
| OUTRAD(8)                |                         |   |
| OUTRAD(9)                | Ft. /Sec. <sup>2</sup>  | Radar slant range accelera-<br>tion of the missile/satellite. |
| OUTRAD(10)               | Deg. /Sec. <sup>2</sup> | Radar elevation angle accel-<br>eration.                      |
| OUTRAD(11)               | Deg. /Sec. <sup>2</sup> | Radar azimuth angle accel-<br>eration.                        |
| OUTRAD(12)               | Deg.                    | Missile re-entry angle.                                       |
| OUTRAD(13)               | Deg.                    | Missile heading angle.  |

Essentially what was said for the printout for IOUT2 = .FALSE. holds true for IOUT2 = .TRUE., except that the storage of data is different. For example, time point - OUTRAD(13) is printed on one line, next time point - OUTRAD(26) printed on the next line, etc.

#### Radar Parameter Differences

The radar parameter difference calculations, as of this writing, have not been fully implemented. The following discussion will describe the output as it will be produced from the calculations.

If IOUT3 = .TRUE., the program will compute radar parameter differences and print them out, after the last set of trajectory and/or radar data printed out. The differences will be out-putted for each radar site and for each perturbed trajectory when NTRAJ  $\geq$  4 in a manner basically

similar to the printout of the radar parameters discussed previously. The differences represent the values obtained by subtracting the radar parameters for the perturbed trajectories from the corresponding parameters for the nominal trajectory (trajectory #1 or #3).

Radar data required for the computations must be stored on the plot file and is identical to the data that is placed on the file for producing plots. Normally, this data would be stored on the file as the result of the execution of the parts of the program preceeding the parameter difference portion. This data could also be stored from a prior execution of the program and used in the difference computations. However, this latter procedure is not recommended since all program inputs required by the computations should be identical to the corresponding ones that were used when the plot file was created. When IOUT3 = true, therefore, IPLOT1 or IPLOT2 should be set = true and NSWTCH = 1 or 2. It should be pointed out that the input variable KZ will determine which trajectory will be the nominal trajectory for the computations. With KZ = true, the nominal trajectory would be the first trajectory; with KZ = false, it will be the third trajectory. The following list defines the output parameters when IOUT2 = false.

| <u>Output Parameter</u> | <u>Units</u> | <u>Description</u>   |
|-------------------------|--------------|--|
| NTRJ                    | None         | Trajectory number.   |
| ISITE                   | None         | Radar site number.   |
| SC1                     | Deg.         | Position in latitude of the radar site.  |
| SC2                     | Deg.         | Position in longitude of the radar site.   |
| Time                    | Min.         | Time from burnout or from initiation of the trajectory of the target (or missile/satellite). Each time printed out will be a time at which both the nominal trajectory and the current perturbed trajectory were detected by the current site. |
| Slant Range             | N.M.         | Difference in radar slant (nominal trajectory slant range - perturbed trajectory slant range) for time.  |



| <u>Output Parameter</u> | <u>Units</u> | <u>Description</u>  |
|-------------------------|--------------|---|
| Sl Range Rate           | Ft. /Sec.    | Difference in radar slant range rate.   |
| Elevation               | Deg.         | Difference in the radar elevation look-angles to the trajectories (nominal-perturbed) or targets. |
| Elevation Rate          | Deg. /Sec.   | Difference in radar elevation angle rate.   |
| Azimuth                 | Deg.         | Difference in radar azimuth angle, measured clockwise from north.                                 |
| Azimuth Rate            | Deg. /Sec.   | Difference in radar azimuth angle rate.   |

If IOUT2 = true, the following list of output parameters is produced.

| <u>Output Parameter</u>          | <u>Units</u>            | <u>Description</u>                                |
|----------------------------------|-------------------------|---|
| NTRJ                             |                         | Described in the previous list.                   |
| ISITE                            |                         |   |
| SC1                              |                         |   |
| SC2                              |                         |   |
| Time                             |                         |   |
| Slant Range                      |                         |   |
| Sl Range Rate                    |                         |   |
| Elevation                        |                         |   |
| Elevation Rate                   |                         |   |
| Azimuth                          |                         |   |
| Azimuth Rate                     |                         |   |
| Sl Range Rate Dot                | Ft. /Sec. <sup>2</sup>  | Difference in radar slant range acceleration.     |
| Elevation Rate Dot               | Deg. /Sec. <sup>2</sup> | Difference in radar elevation angle acceleration. |
| Azimuth Rate Dot                 | Deg. /Sec. <sup>2</sup> | Difference in radar azimuth angle acceleration.   |
| Angular Separation in Radar Beam | Deg.                    | Total angular separation in the radar beam.       |

### Plot File

The previous paragraphs under Output have dealt with the printout on listing paper from a program execution. The following paragraphs will describe the plot file which can be created on disc or tape if the user exercises the appropriate input options. By setting either IPLOT1 or IPLOT2 = .TRUE. (when NSWATCH = 1, 2) data will be placed on the file so that off-line plots of radar parameters (range, azimuth, elevation, etc.) can be produced. The plots can be drawn, from data cards punched out from the file, on the Hewlett-Packard 9820A calculator/plotter through the use of the Generalized Data Entry and Plot Program. See Volume II for a detailed description of this program. The Plot Program XYNETICS Plotter, developed for the first modified version of the trajectory program, can handle the case of one trajectory and one radar site, only. The format of the file for each generated trajectory which is subject to a radar search and detected by the radar is given below. Logical records nos. 1 through 7, ..., n contain the data for one sighting of the trajectory (or target) by a radar site. They will be repeated for each additional sighting by the site; they will also be repeated for each sighting of the trajectory by each additional radar site, if multiple sites are to be processed. Refer to Figure III-1 which illustrates the layout of the file.

Logical Record No. 1

| <u>Symbol Name</u> | <u>Units</u> | <u>Description</u>  |
|--------------------|--------------|---|
| TIME3              | Min.         | Initial time of sighting missile trajectory at the radar site.  |
| IPLOT2             |              | Plotting option 2.  |
|                    | T            | Plots for 13 different radar trajectory parameters can be produced. A total of 12 plots can be drawn. |
|                    | F            | Plots for 8 radar trajectory parameters can be produced. A total of 7 plots can be drawn.             |
| IO2                | None         | Number of radar parameters which can be plotted. IO2=8 if IPLOT2 if false, 13 for IPLOT2 true.        |

Radar Site 1, 1st Sighting:

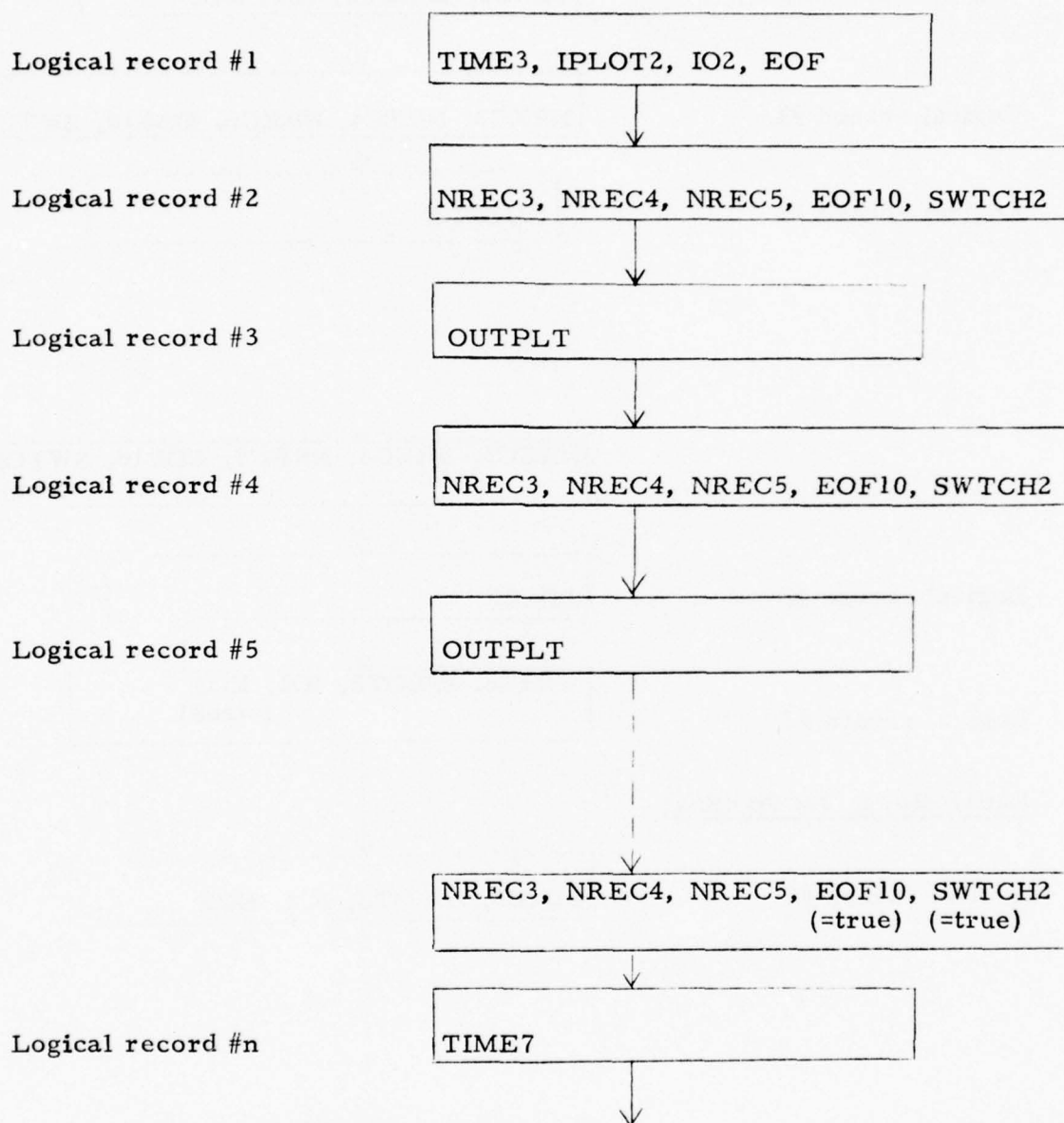


Figure III-1. Plot File Format for Each Trajectory. (1 of 2)

Radar Site 1, 2nd Sighting:

Logical record #1

TIME3, IPLOT2, IO2, EOF

Logical record #2

NREC3, NREC4, NREC5, EOF10, SWITCH2

Logical record #3

OUTPLT

NREC3, NREC4, NREC5, EOF10, SWITCH2  
(=true) (=true)

Logical record #n

TIME7

Logical record #1

TIME3, IPLOT2, IO2, EOF  
(=true)

Radar Site 2, 1st Sighting:

Logical record #1

TIME3, IPLOT2, IO2, EOF

Last record on file

TIME3, IPLOT2, IO2, EOF  
(=true)

Figure III-1. Plot File Format for Each Trajectory (2 of 2)



| <u>Symbol Name</u> | <u>Units</u> | <u>Description</u>   |
|--------------------|--------------|--|
| EOF                |              | Switch variable to denote the end of data for the current radar site and the current trajectory. |
|                    | T            | There is no more data on the file for the current site and trajectory.                           |
|                    | F            | Radar data follows for the current site and trajectory.  |

Note that the description of IPLOT2 above is somewhat different from that given under Inputs. The description above is given mainly from the standpoint of a plot program.

Logical Record No. 2, 4, 6, ---

| <u>Symbol Name</u> | <u>Units</u> | <u>Description</u>  |
|--------------------|--------------|---|
| NREC3              | None         | Number of time points in the radar trajectory data on the following record.   |
| NREC4              | None         | Total number of time points in the following record of radar data and all previously input records of data for the current sighting of the missile trajectory by the radar. |
| NREC5              | None         | Number of the following record of radar data for the current sighting.  |
| EOF10              |              | Switch variable to signal the end of the set of data for the current missile sighting.  |
|                    | T            | No more radar data follows for the current sighting.  |
|                    | F            | More data follows for the current sighting.   |
| SWTCH2             |              | Switch variable for plot program to read last time missile is visible to the radar for the current sighting.  |
|                    | T            | Read in this last time from the file.   |
|                    | F            | Do not read in this last time from the file.  |

Note: In the current version of the program, NREC4 and NREC5 are not used, and the last time of missile visibility to the radar is not written on the plot file. This means SWTCH2 will always be false, and when EOF10 is true, logical record no. 2, 4, 6, --- will be the last record on the file for one sighting of the missile by the radar. The very last record on the file will be logical record no. 1 with EOF true following data for the last trajectory and final sighting by the last radar site.

Logical record no. 3, 5, 7, ---

| <u>Symbol Name</u> | <u>Units</u> | <u>Description</u>  |
|--------------------|--------------|---|
| OUTPLT             |              | Output array for outputting the data on this record. There are NREC3*IO2 data words on this record. The contents of OUTPLT are: |
| OUTPLT(1)          | N.M.         | Radar slant range for 1st time-point of this record.  |
| OUTPLT(2)          | Ft. /Sec.    | Radar slant range rate for 1st timepoint.   |
| OUTPLT(3)          | Deg.         | Radar elevation angle.  |
| OUTPLT(4)          | Deg/Sec.     | Radar elevation angle rate.   |
| OUTPLT(5)          | Deg.         | Radar azimuth angle.  |
| OUTPLT(6)          | Deg/Sec.     | Radar azimuth angle rate.   |
| OUTPLT(7)          | eru          | Trajectory radius in eru.   |
| OUTPLT(8)          | Deg.         | Trajectory inertial phi angle.  |

If IPLOT2 = .TRUE., the following parameters will also be on this logical record:

|            |                         |                               |
|------------|-------------------------|-------------------------------|
| OUTPLT(9)  | Ft. /Sec. <sup>2</sup>  | Slant range acceleration.     |
| OUTPLT(10) | Deg. /Sec. <sup>2</sup> | Elevation angle acceleration. |
| OUTPLT(11) | Deg. /Sec. <sup>2</sup> | Azimuth angle acceleration.   |
| OUTPLT(12) | Deg.                    | Missile reentry angle.        |
| OUTPLT(13) | Deg.                    | Missile heading angle.        |

Note: If IPLOT2 is false, there are only 8 different radar trajectory parameters on this record for each time point; if IPLOT2 is true there will be 13. Each parameter will be repeated every IO2+1 word of OUTPLT; e.g., OUTPLT (IO2+1) contains the slant range for the 2nd time point of the record, OUTPLT (IO2+2) contains the range rate for the 2nd time point, etc. Any pair of consecutive time points for any records containing radar parameter data are separated by the same increment in time. That is, the time increment between consecutive time points has been set at 0.1 min. for all radar data on the plot file.

If SWTCH2 is true (not currently allowed), the following record will be written on the file. It will be the last record on the file for one sighting of the missile by the radar site and is used mainly in the computation of radar parameter differences.

Logical record no. n

| <u>Symbol Name</u> | <u>Units</u> | <u>Description</u>   |
|--------------------|--------------|--|
| TIME7              | Min.         | Last time of sighting (or detection) by the radar site for the current missile sighting. |

#### 5. Main Logic Flow

Figure III-2 is a flow chart of the main logic of the program. It is basically a flow chart for the executive (main program) of the program.

#### 6. Sample Job Stream

The sample job stream following Figure III-2 illustrates the program setup for a 1 radar site and 8 trajectory run. The nominal trajectory for the perturbations was chosen as the 1st trajectory. The job stream is setup to place radar data on the plot file so that plots may be produced later if so desired. In the job stream, file 09 stores trajectory data and file 10 stores the radar data to be plotted. The sample output and sample plots included in this document were produced by executing this sample job stream. The output and plots herein included are for the first 3 trajectories only. Note that the second trajectory is labeled number 4. Also, the input data of the job stream causes circular orbit trajectories to be generated.

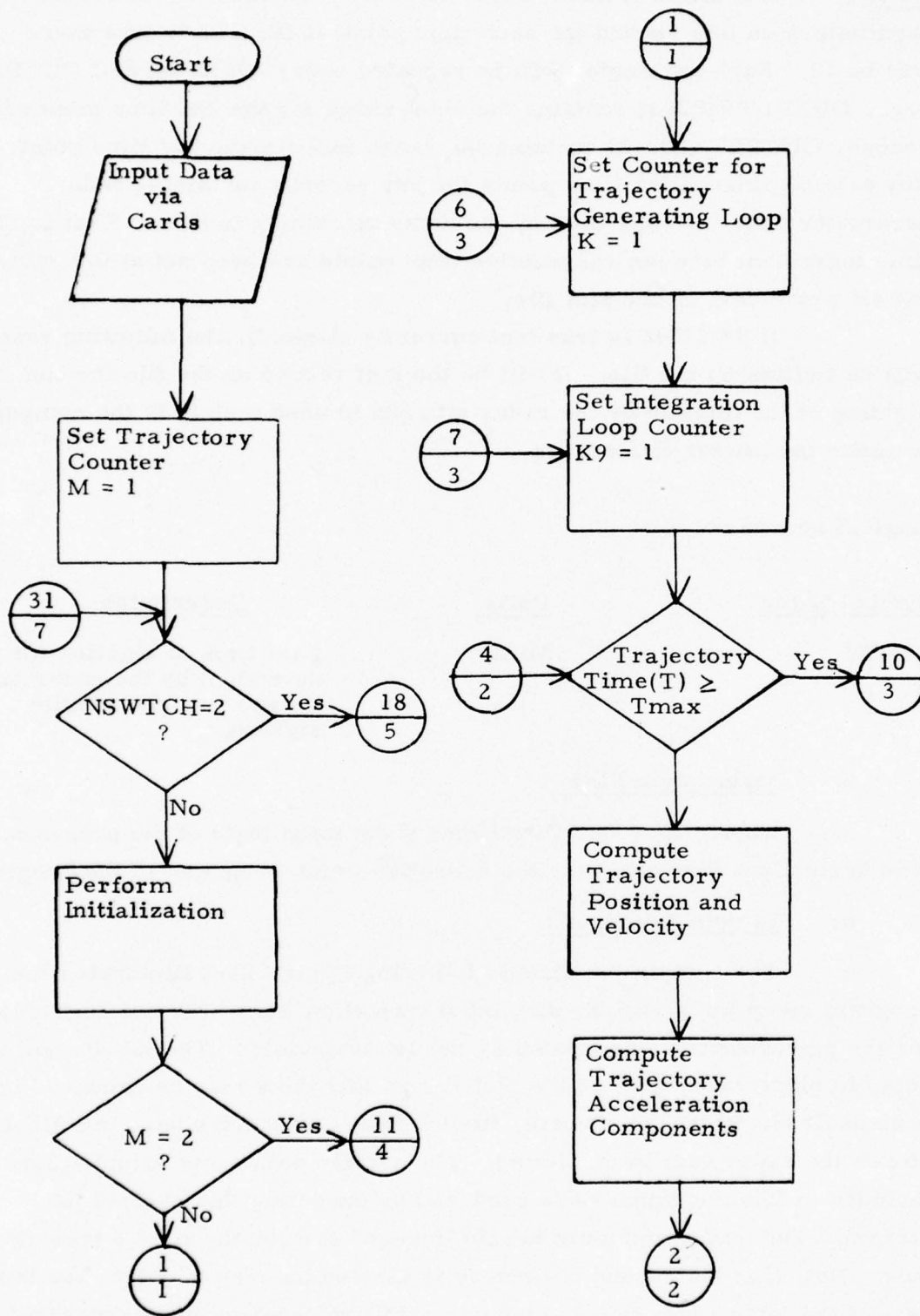


Figure III-2. Logic Flow Diagram for the RADC Trajectory Program (1 of 9)



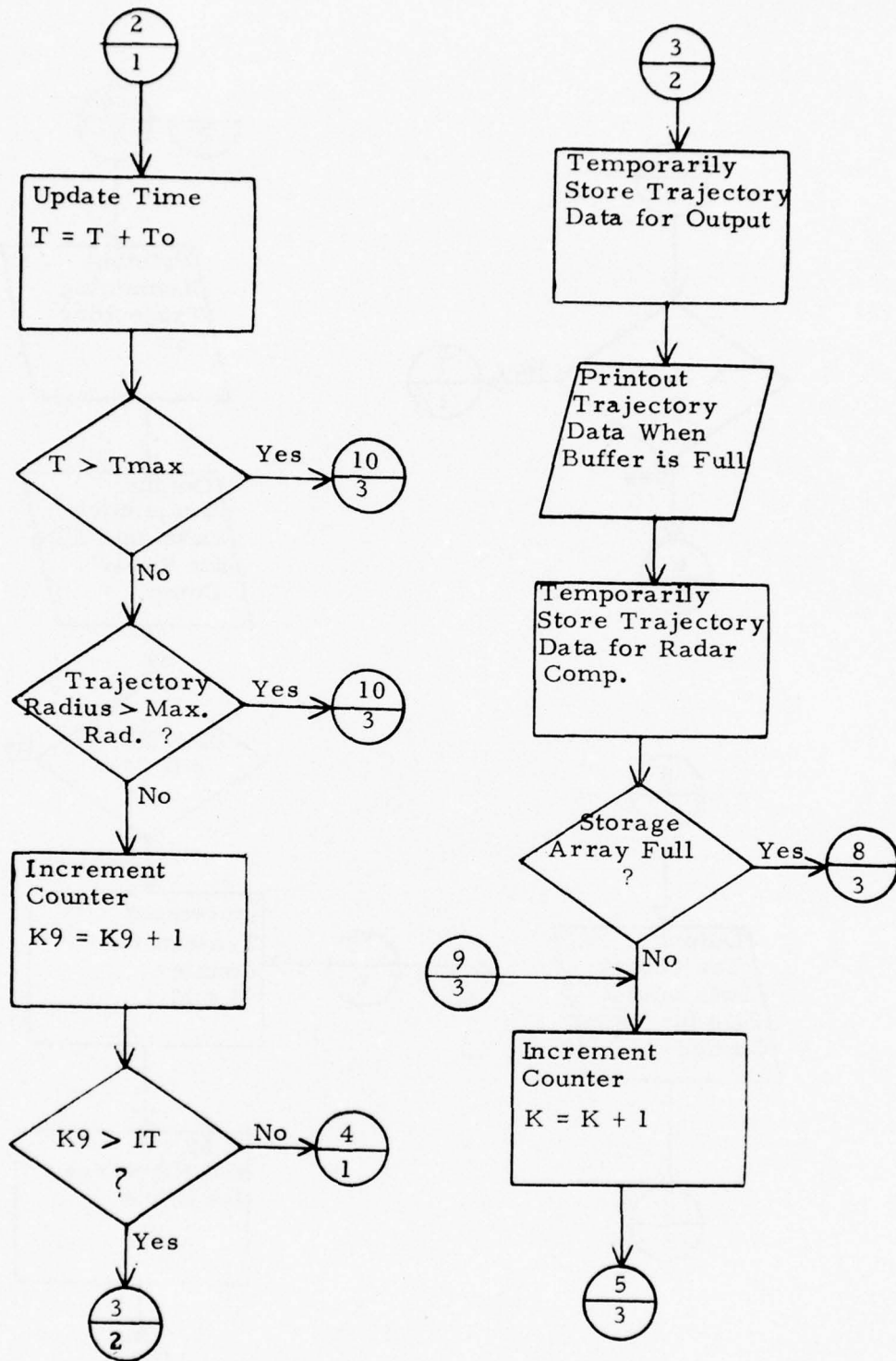


Figure III-2. Logic Flow Diagram for the  
RADC Trajectory Program (2 of 9)

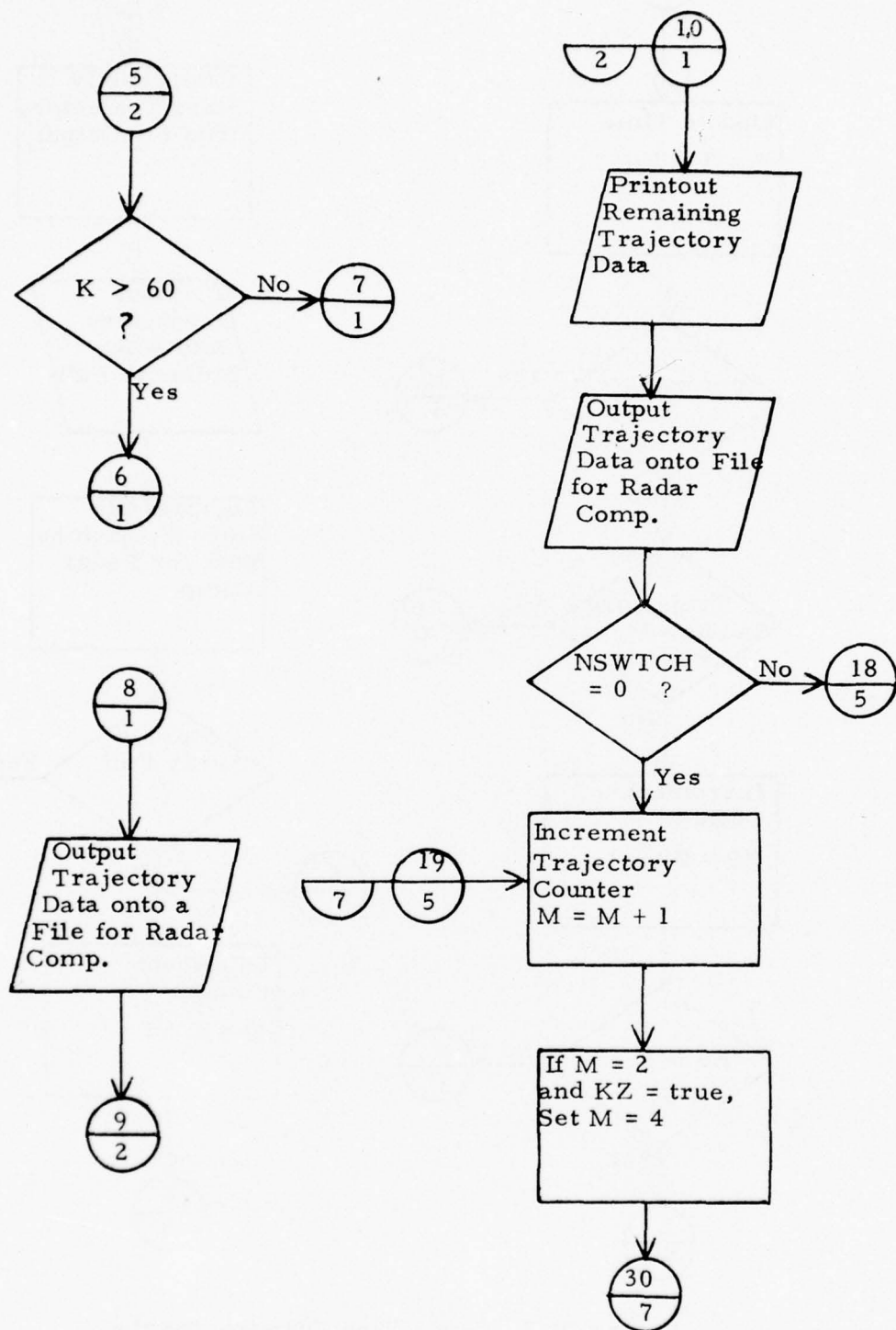


Figure III-2. Logic Flow Diagram for the RADC Trajectory Program (3 of 9)

M = 2 Trajectory

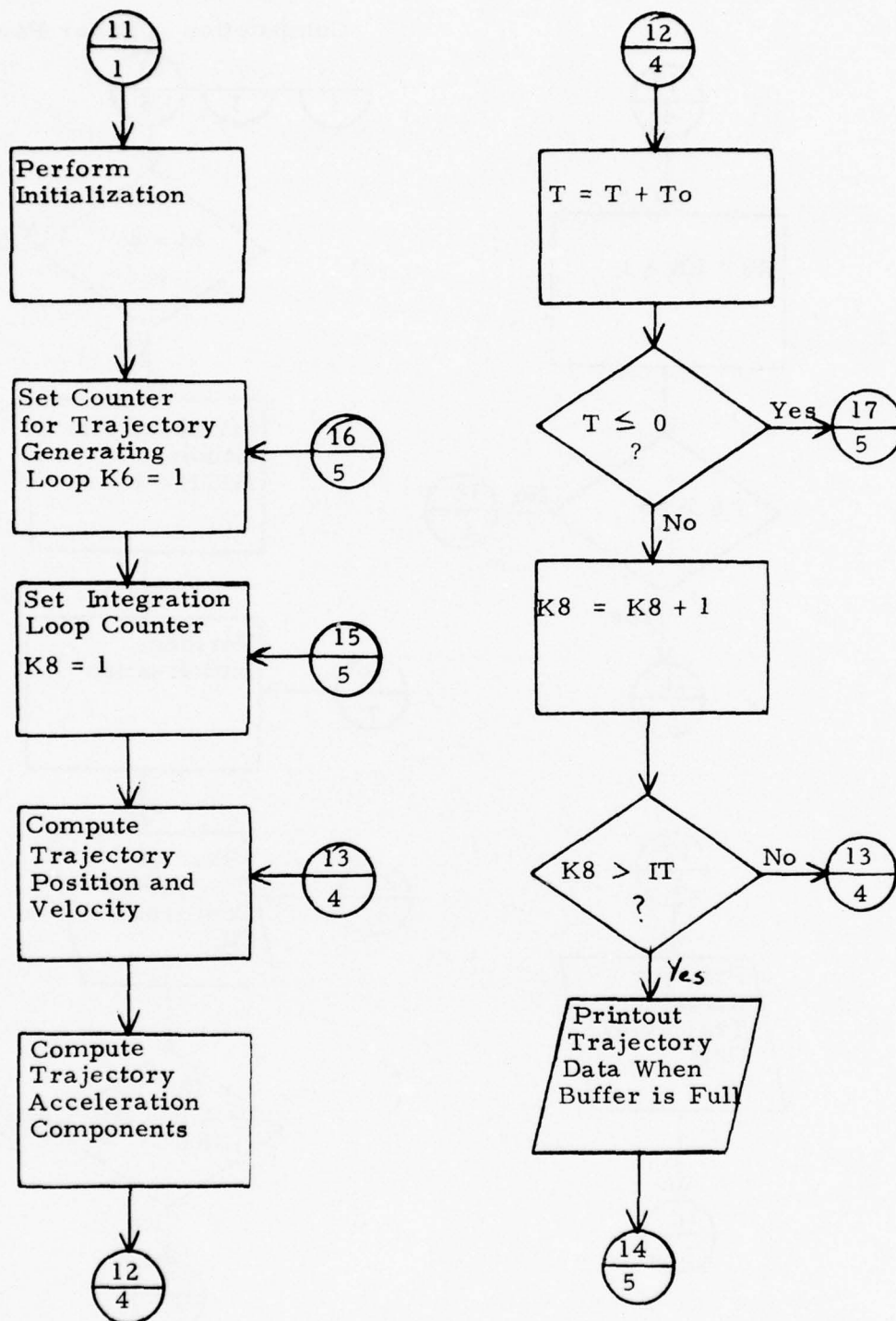


Figure III-2. Logic Flow Diagram for the RADC Trajectory Program (4 of 9)

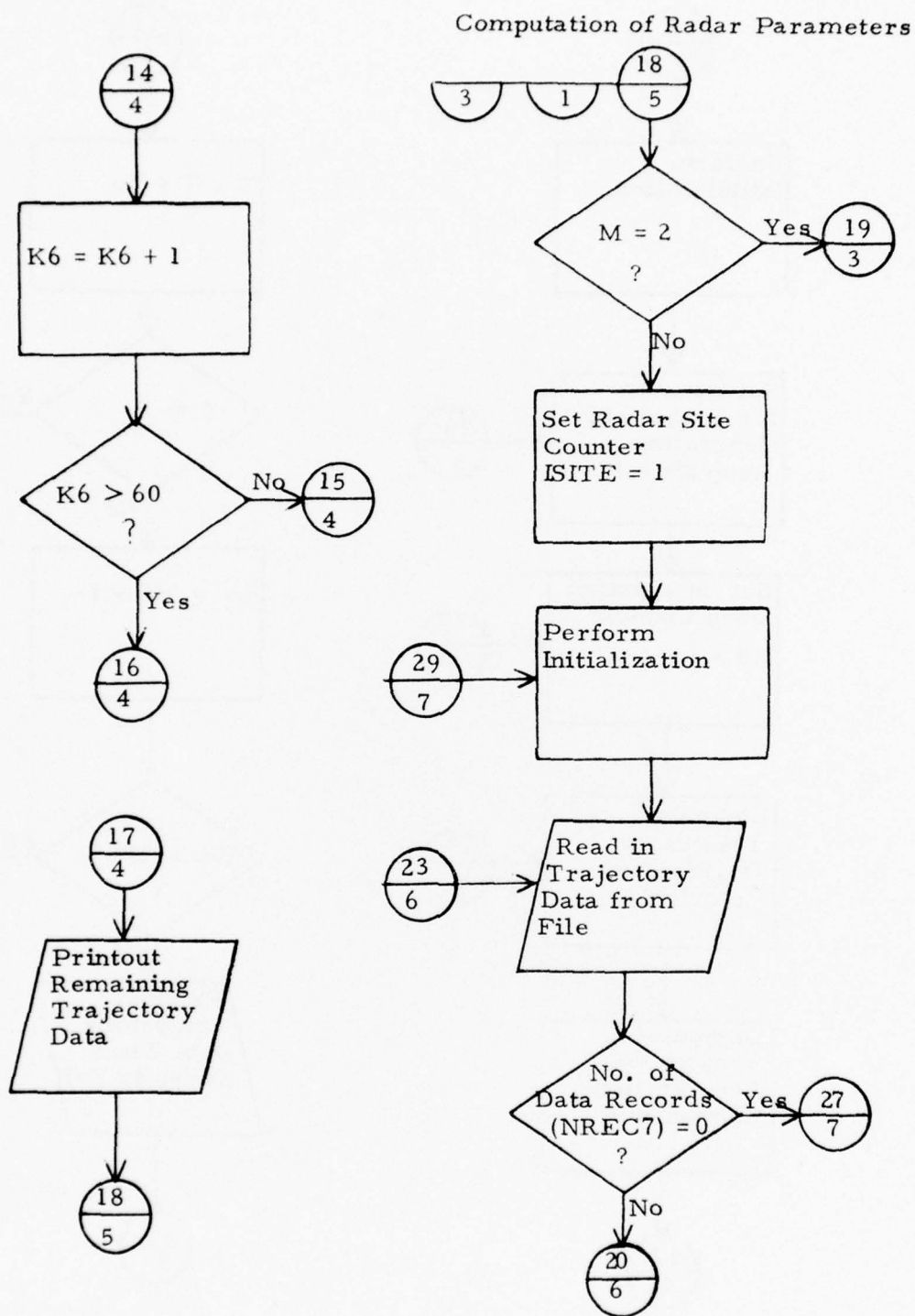


Figure III-2. Logic Flow Diagram for the RADC Trajectory Program (5 of 9)



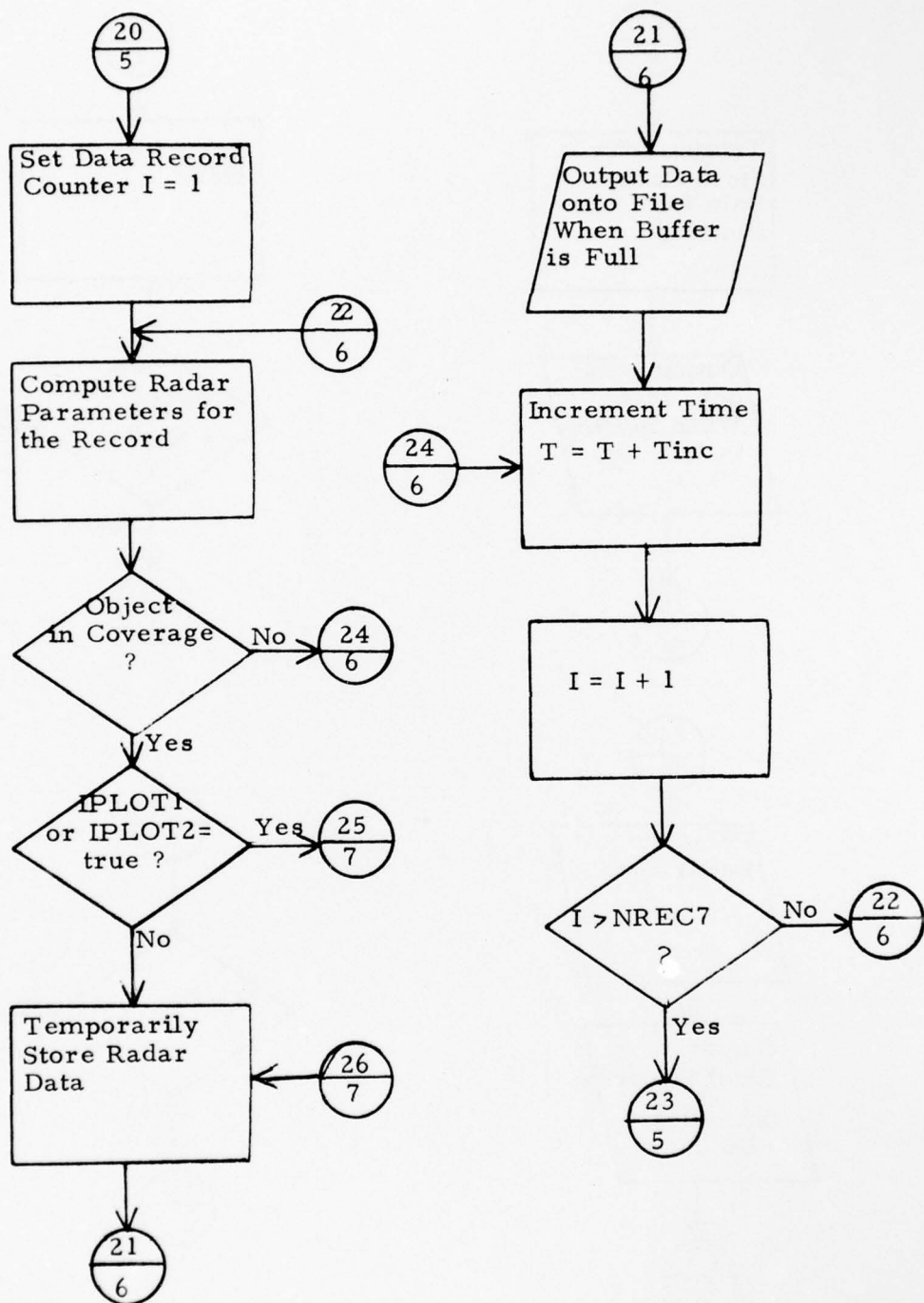


Figure III-2. Logic Flow Diagram for the RADC Trajectory Program (6 of 9)

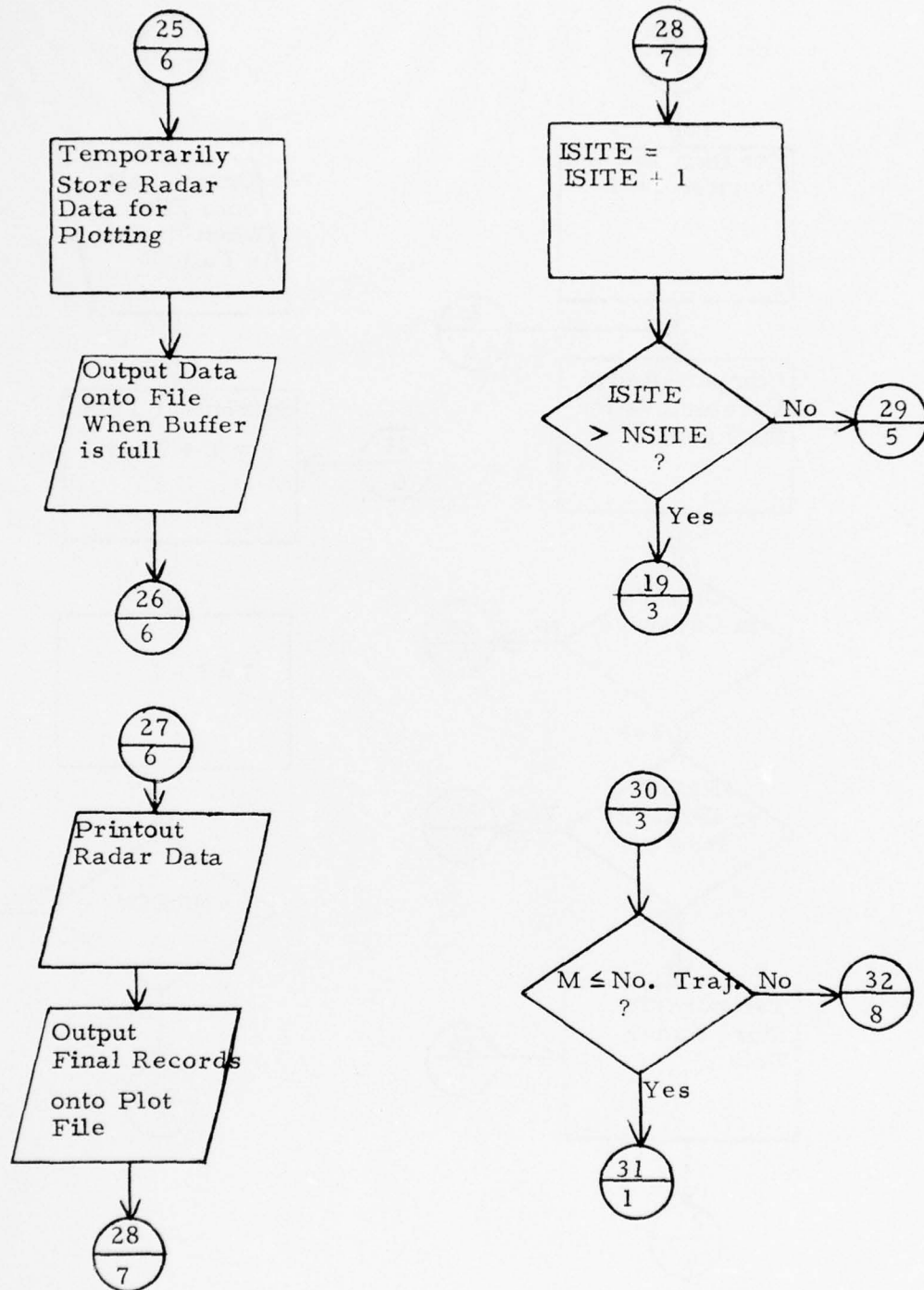


Figure III-2. Logic Flow Diagram for the RADC Trajectory Program ( 7 of 9)

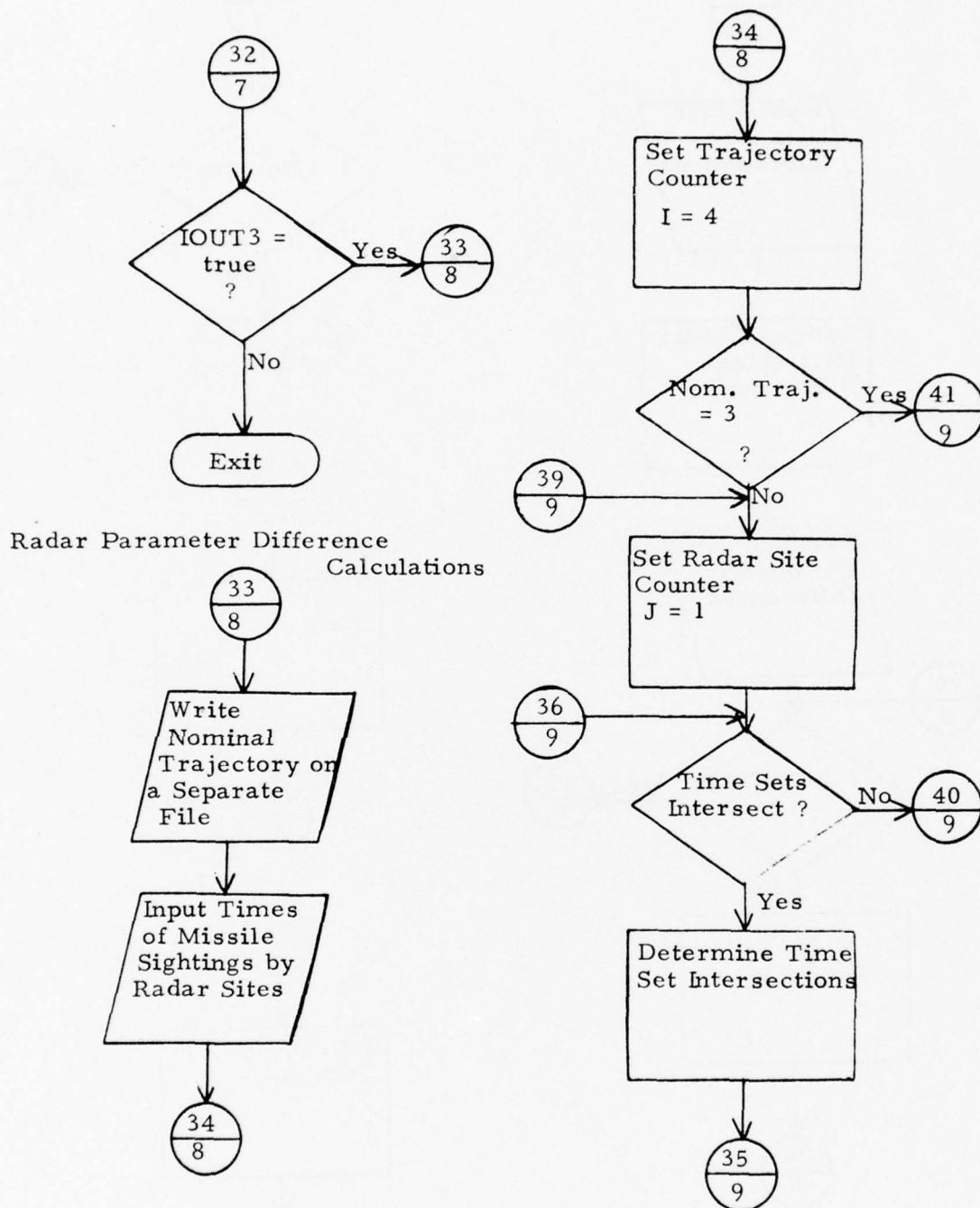


Figure III-2. Logic Flow Diagram for the RADC Trajectory Program (8 of 9)

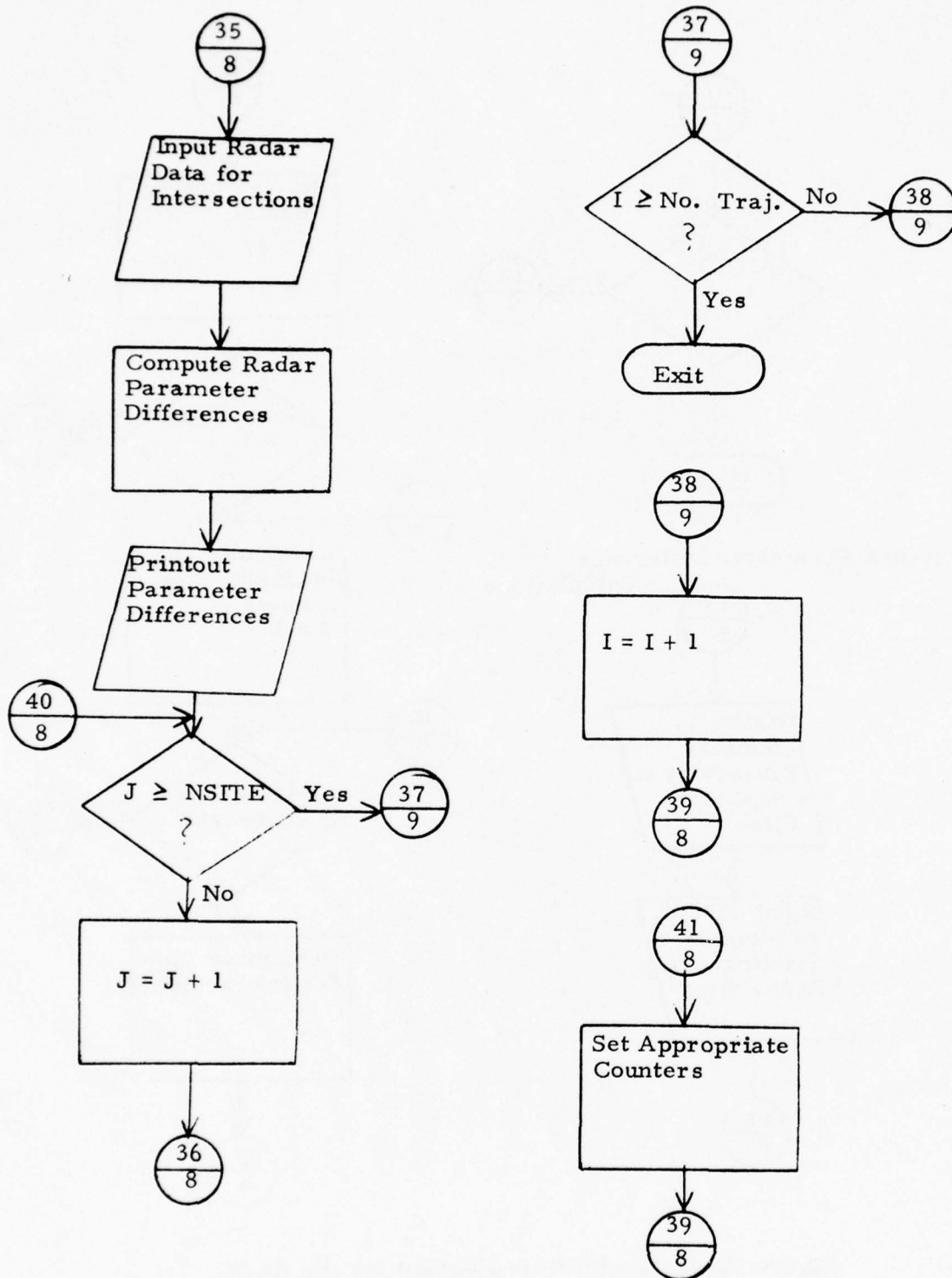


Figure III-2. Logic Flow Diagram for the RADC Trajectory Program (9 of 9)



```

10$:IDENT:CLEARY,CONTI      ,65121104RADC,DSSR
20$:USERID:CLEARYSTHREE
30$:OPTION:FORTAN
40$:SELECT:CLEARY/OMISSATC
50$:SELECT:CLEARY/OSUPC
60$:SELECT:CLEARY/00OUTPUTC
70$:SELECT:CLEARY/0INTRAJC
75$:SELECT:CLEARY/0ATMOSC
77$:SELECT:CLEARY/0EOTNXC
80$:EXECUTE
90$:LIMITS:40,40K,,12000
100$:DISC:03,A12,10L
110$:PRMFL:09,R/0,L,CLEARY/DSTORA
115$:PRMFL:10,R/0,L,CLEARY/DSTORB
120$:DATA:05
130 $INPUT1 NTRAJ=10,TM=20.000,NSWICH=1 $
140 $INPUT2 IOUT1=F,IOUT2=F,IOUT3=F,OUTINC=0.1,KAT=F,KZ=1,
150 SPHERE=1,IPL0T1=T,IPL0T2=F,INERTL=T $
160 $INPUT3 GAM=90.000,BETA=31.8263300,V0=2.55674204,
170 HX=6.3802805,THE=62.700,GLAM=40.3500,THES=-40.000,CLAMS=60.000 $
180 $INPUT4 NSITE=1,
190 SLAT(1)=35.000,SLONG(1)=233.33300,SALT(1)=0.000,FLIM=89.000 $
200 $INPUT5 A(1)=4*0.000,5.000,2*3.53300,
210 B(1)=0.000,5.000,3.53300,-3.53300,1.000,3.53300,-3.53300,
220 C(1)=5.000,1.000,2*3.53300,3*0.000 $
210$:ENDJOB
220***EOF

```

Sample Job Stream for the RADC Trajectory Program

| RADC 635/645 BATCH JOB  |       |  |              |       |
|---|-------|--|--------------|-------|
| SNUMB NUMBER  |       | DATE   | TIME         |       |
|   |       | 7/2/76   | 1330         |       |
| PROGRAMMER  |       | TELEPHONE  |              |       |
| Conti   |       | 339-1360   |              |       |
| RADC ENGINEER   |       | TELEPHONE  | SYMBOL       |       |
| Cleary  |       | 3573   | OCSA         |       |
| TAPES ASSIGNED  |       |  |              |       |
| REEL NO.  | WRITE | READ   | DEN.         | TITLE |
| None  |       |  |              |       |
|   |       |  |              |       |
|   |       |  |              |       |
|   |       |  |              |       |
|   |       |  |              |       |
|   |       |  |              |       |
|   |       |  |              |       |
|   |       |  |              |       |
|   |       |  |              |       |
| PERIPHERALS ASSIGNED <input checked="" type="checkbox"/> READER <input checked="" type="checkbox"/> PRINTER <input type="checkbox"/> PUNCH<br><input checked="" type="checkbox"/> DISC # OF LINKS 40 <input type="checkbox"/> DRUM # OF LINKS _____ |       |  |              |       |
| CORE SIZE 40K   |       | ACTIVITIES 1   |              |       |
| PROCESSOR TIME 0.10   |       | ESTIMATED LINES OF PRINT 5,000                                   |              |       |
| TOTAL RUN TIME 0.25   |       |  |              |       |
| DECKS EXPECTED  |       |  |              |       |
| NO. OF BINARY DECKS   |       | NO. OF COMDECKS  |              |       |
| None  |       |  |              |       |
| BMC   |       | TAPE <input type="checkbox"/> DUMP <input type="checkbox"/> COPY |              |       |
| FROM:   | TO:   | MODE   | NO. OF FILES |       |
|   |       | <input type="checkbox"/> BCD                                     |              |       |
|   |       | <input type="checkbox"/> BINARY                                  |              |       |
| SPECIAL OPERATOR INSTRUCTIONS   |       |  |              |       |
|   |       |  |              |       |
|   |       |  |              |       |
|   |       |  |              |       |
|   |       |  |              |       |
|   |       |  |              |       |
| (Use reverse side if required)  |       |  |              |       |

RADC FORM 0-56 APR 69 PREVIOUS EDITION WILL BE USED

HIS 6000 Batch Submittal Form

Source Listing of the RADC Trajectory Program

|         |  |          |
|---------|--|----------|
| CHISSAT | MISSILE/SATELLITE TRAJECTORY PROGRAM                               | 00000010 |
| C       | INPUT/OUTPUT MOD 2,MULTIPLE SITE/TRAJECTORY VERSION                | 00000020 |
|         |  | 00000030 |
|         |  | 00000040 |
| C       | THIS IS A GENERAL PERTURBATION PROGRAM THAT PREDICTS THE POSITION, | 00000050 |
| C       | VELOCITY,AND ACCELERATION OF A VEHICLE WHETHER AS AN EARTH         | 00000060 |
| C       | ORBITING SATELLITE OR BALLISTIC MISSILE,THE FORMULATION IS BASED   | 00000070 |
| C       | UPON THE NUMERICAL INTEGRATION OF THE SPHERICAL FORM OF THE EARTH. | 00000080 |
| C       | THE 1959 ARDC ATMOSPHERIC MODEL AND                                | 00000090 |
| C       | THE EARTH WIND ARE INCLUDED.                                       | 00000100 |
|         |  | 00000110 |
| C       | THIS ROUTINE DRIVES THE PROGRAM.                                   | 00000120 |
| C       | THE MAIN SUBROUTINE GROUPINGS CALLED ARE                           | 00000130 |
| C       | 1. EQTNX - COMPUTES ACCELERATION COMPONENTS                        | 00000140 |
| C       | 2. CONVER - COMPUTES SENSOR PARAMETERS                             | 00000150 |
| C       | 3. RKG - USING A 4TH ORDER RUNGE KUTTA-GILL, NUMERICALLY           | 00000160 |
| C       | INTEGRATES THE EQUATIONS OF MOTION                                 | 00000170 |
|         |  | 00000180 |
| C       | ALL DATA ASSOCIATED WITH THE MATHEMATICAL MODEL OF THE EARTH ARE   | 00000190 |
| C       | FROM MAKEMSON,B. , BAKER,B.L.M. , AND WESTRON,G.B. ANALYSIS AND    | 00000200 |
| C       | STANDARDIZATION OF ASTRODYNAMIC CONSTANTS.                         | 00000210 |
|         |  | 00000220 |
|         | DOUBLE PRECISION X,XD,XDD,TO,TM                                    | 00000230 |
|         | DOUBLE PRECISION TC,TI,XK,TK                                       | 00000240 |
|         | *T,H,XYZ,RSL,PZ,R,W  | 00000250 |
|         | DOUBLE PRECISION TN,STM  | 00000260 |
|         | DOUBLE PRECISION P1,ZK,B1,GEO                                      | 00000270 |
|         | DOUBLE PRECISION GAM,BETA,HX,VO,THE,GLAM,SC1,SC2,AH,THES,GLAMS     | 00000280 |
|         | *E,ELIM,SLAT,SLONG,SALT  | 00000290 |
|         | COMMON/E/E/ELIM/ELIM/IJ/J/INOM,I,J,JSIGHT,TSTART,TEND              | 00000300 |
|         | COMMON/MS/ GAM,BETA,HX,VO,THE,GLAM,SC1,SC2,AH,THES,GLAMS           | 00000310 |
|         | COMMON/TS/T,H,XYZ,RSL,PZ   | 00000320 |
|         | *7A/R,W/JX/JX/TIME2/TIME2  | 00000330 |
|         | COMMON/BS/ X(3), XD(3), XDD(3)                                     | 00000350 |
|         | *7GEOXK/GEO,XK   | 00000370 |
|         | *7SWSW/SWCH1,SWCH2/SW10/SWCH10                                     | 00000380 |
|         | *7SW3SW4/SWCH3,SWCH4   | 00000390 |
|         | *7SW5SW6/SWCH5,SWCH6   | 00000400 |
|         | *7SW7/SWCH7/SW8/SWCH8/SW9/SWCH9/NSWCH/NSWCH                        | 00000410 |
|         | *7TIME5/TIME5  | 00000420 |
|         | *7TSIGHT/TIME5(10,10,5),TIMESF(10,10,5),NSIGHT(10,10)              | 00000425 |
|         | *7OPTION/IOUT1,IOUT2,KZ,IPL0T1,IPL0T2,KAT,SPHERE,OUTINC,IOUT3      | 00000430 |
|         | *7OUTRJ/OUTTRJ(5000),OUTRAD(5000),OUTPLT(5000)                     | 00000440 |
|         | *7NTRAJ/ITM  | 00000450 |
|         | COMMON/GE/ZK,B1,P1   | 00000460 |
|         | COMMON/AX/TM,M   | 00000470 |
|         | COMMON/INOUT/INCOUT,IOUT,NOFF1,NOFF2,NOFF3,IOUTA                   | 00000480 |
|         | *7TO/TO/IT2/IT2,IT   | 00000490 |
|         | COMMON/NR/NREC1,NREC2,NREC3,NREC4,NREC5,NREC                       | 00000500 |
|         | *7IO/IO,IO1,IO2  | 00000510 |
|         | COMMON/NR7/NREC7,NOFF4   | 00000520 |
|         | *7ISITE/ISITE/SITES/NSITE,SLAT(20),SLONG(20),SALT(20)              | 00000530 |



|     |   |          |
|-----|---|----------|
|     | LOGICAL IOUT1,IOUT2,KZ,IPLOT1,IPLOT2,KAT,SPHERE           | 00000540 |
|     | *,IOUT3,SWTCH1,SWTCH2,SWTCH10                             | 00000550 |
|     | LOGICAL SWTCH3,SWTCH4                                     | 00000560 |
|     | LOGICAL SWTCH5,SWTCH6                                     | 00000570 |
|     | *,SWTCH7,SWTCH8,SWTCH9                                    | 00000580 |
| C   | INPUT DATA  | 00000600 |
|     | CALL INPUT  | 00000610 |
|     | M=1   | 00000620 |
| C   | SET INTEGRATION STEP SIZE AND NUMBER OF INTEGRATION STEPS | 00000630 |
|     |   | 00000640 |
|     |   | 00000650 |
|     |   | 00000660 |
| 260 | TO=0.1D-1   | 00000670 |
|     | IT=10   | 00000680 |
|     | TINC=TO*IT  | 00000690 |
|     | IF(NSWTCH.EQ.2)GO TO 250                                  | 00000700 |
|     |   | 00000710 |
| C   | INITIALIZATION  | 00000720 |
|     | CALL INITAL   | 00000730 |
|     |   | 00000740 |
| C   | INITIALIZE MISSILE/SATELLITE TRAJECTORY                   | 00000750 |
|     | CALL ICEBBM   | 00000760 |
|     | IF(M.EQ.2)GO TO 15  | 00000770 |
|     | CALL EQTNX  | 00000780 |
| 105 | CALL OUTPUT   | 00000790 |
|     | IF(M.EQ.2)GO TO 6   | 00000800 |
|     | CALL STORTR   | 00000810 |
|     |   | 00000820 |
|     |   | 00000830 |
| C   | MAIN PROCESSING LOOP FOR TRAJECTORY GENERATION            | 00000840 |
|     |   | 00000850 |
| 20  | DO 16 K=1,60  | 00000860 |
|     |   | 00000870 |
| C   | INTEGRATION LOOP  | 00000880 |
|     |   | 00000890 |
|     | DO 1 K9=1,IT  | 00000900 |
|     | IF(T.GE.TM-1. D-5)GO TO 21                                | 00000910 |
|     |   | 00000920 |
| C   | PERFORM RUNGE-KUTTA INTEGRATION                           | 00000930 |
|     | CALL RKG  | 00000940 |
|     |   | 00000950 |
| C   | COMPUTE ACCELERATION COMPONENTS                           | 00000960 |
|     | CALL EQTNX  | 00000970 |
|     | T=T+TO  | 00000980 |
|     | IF(T.GT.(TM+1.0D-5).OR.V(1).GT.GEO)GO TO 21               | 00000990 |
| 1   | CONTINUE  | 00010000 |
|     | IOUT = IOUT + IT  | 00010010 |
|     |   | 00010020 |
|     |   | 00010030 |
|     |   | 00010040 |
|     |   | 00010050 |
|     |   | 00010060 |
|     |   | 00010070 |
|     |   | 00010080 |
|     |   | 00010090 |

|     |   |          |
|-----|---|----------|
| C   | STORE TRAJECTORY DATA FOR OUTPUT              | 00001100 |
|     | IF(IOUT.GE.INCOUT)CALL STORTJ                 | 00001110 |
|     |   | 00001120 |
| C   | PRINT OUT TRAJECTORY DATA                     | 00001130 |
|     |   | 00001140 |
|     | IF(NREC1.GE.NOFF1)CALL PRINTT                 | 00001150 |
|     |   | 00001160 |
|     |   | 00001170 |
| C   | STORE TRAJECTORY DATA FOR RADAR COMPUTATIONS  | 00001180 |
|     |   | 00001190 |
|     | CALL STORTR                                   | 00001200 |
|     | IF(NREC7.GE.NOFF7)GO TO 150                   | 00001210 |
|     | GO TO 16                                      | 00001220 |
|     |   | 00001230 |
|     |   | 00001240 |
| C   | OUTPUT TRAJECTORY DATA ON A FILE              | 00001250 |
|     |   | 00001260 |
|     |   | 00001270 |
| 150 | IF(SWCH9)CALL OUTTRI                          | 00001280 |
|     | SWCH9=.FALSE.                                 | 00001290 |
|     | CALL OUTTR                                    | 00001300 |
| 16  | CONTINUE                                      | 00001310 |
|     | GO TO 20                                      | 00001320 |
| 21  | IF(X(1).GT.GEQ)GO TO 2                        | 00001325 |
|     | SWCH3=.TRUE.                                  | 00001330 |
| 2   | CONTINUE                                      | 00001340 |
|     |   | 00001350 |
| C   | PRINT OUT TRAJECTORY DATA                     | 00001360 |
|     |   | 00001370 |
|     | CALL PRINTT                                   | 00001380 |
|     |   | 00001390 |
| C   | OUTPUT TRAJECTORY DATA ON A FILE              | 00001400 |
|     |   | 00001410 |
|     | IF(SWCH9)CALL OUTTRI                          | 00001415 |
|     | IF(NREC7.NE.0)CALL OUTTR                      | 00001420 |
|     | CALL OUTTR                                    | 00001430 |
|     | IF(ITM.GE.2)CALL STORT2                       | 00001431 |
|     | IF(NSWCH.EQ.1)GO TO 17                        | 00001432 |
|     | GO TO 250                                     | 00001435 |
| 60  | CONTINUE                                      | 00001440 |
|     |   | 00001450 |
| C   |   | 00001460 |
| C   | M = 2 TRAJECTORY                              | 00001470 |
| C   |   | 00001480 |
| C   | SET INTEGRATION STEP SIZE AND NUMBER OF STEPS | 00001490 |
| C   |   | 00001500 |
|     | TO=-0.01DC                                    | 00001510 |
|     | IT=10   | 00001520 |
|     | IF(SWCH10)IT=IT2                              | 00001530 |
|     | DO 41 K8=1.IT                                 | 00001540 |
|     | CALL RKG                                      | 00001550 |
|     | CALL EQTNX                                    | 00001560 |
|     | T=T+TO  |          |

|     |                                     |          |
|-----|-------------------------------------|----------|
|     | IF(T.LE.1.D-5)GO TO 86              | 00001570 |
| 41  | CONTINUE                            | 00001580 |
|     | TIME2=T                             | 00001585 |
|     | CALL STORTJ                         | 00001590 |
|     | IF(SWCH10)IT=10                     | 00001600 |
| C   |                                     | 00001610 |
| C   | MAIN PROCESSING LOOP,M=2 TRAJECTORY | 00001620 |
| C   |                                     | 00001630 |
| 70  | DO 18 K6=1,60                       | 00001640 |
|     | DO 40 K8=1,IT                       | 00001650 |
|     | CALL RKG                            | 00001660 |
|     | CALL EQTNX                          | 00001670 |
|     | T=T+TO                              | 00001680 |
|     | IF(T.LE.1.D-5)GO TO 86              | 00001690 |
| 40  | CONTINUE                            | 00001700 |
|     | IOUT=IOUT+IT                        | 00001710 |
|     | IF(IOUT.GE.INCOUT)CALL STORTJ       | 00001720 |
|     | IF(NREC1.GE.NOFF1)CALL PRINTT       | 00001730 |
| 18  | CONTINUE                            | 00001740 |
|     | GO TO 70                            | 00001750 |
| 86  | SWTCH3=.TRUE.                       | 00001760 |
|     | CALL PRINTT                         | 00001770 |
| C   |                                     | 00002000 |
| C   | COMPUTE RADAR PARAMETERS            | 00002010 |
| C   |                                     | 00002020 |
| 250 | IF(M.EQ.2)GO TO 17                  | 00002025 |
|     | DO 500 ISITE=1,NSITE                | 00002030 |
|     | CALL INITIAL                        | 00002040 |
| C   |                                     | 00002060 |
| C   | INPUT TRAJECTORY DATA               | 00002070 |
| C   |                                     | 00002080 |
|     | CALL INTRAJ                         | 00002090 |
| 100 | CALL TRAJIN                         | 00002100 |
|     | IF(NREC7.EQ.0)GO TO 200             | 00002110 |
|     | JX=1                                | 00002120 |
|     | DO 300 I=1,NREC7                    | 00002130 |
|     | CALL TRAJX                          | 00002140 |
|     | CALL CONVER                         | 00002160 |
|     | SWTCH5=.TRUE.                       | 00002170 |
|     | IF(E.GT.ELIN)GO TO 120              | 00002180 |
|     | SWTCH5=.FALSE.                      | 00002190 |
|     | SWTCH6=.FALSE.                      | 00002200 |
|     | IOUTA=IOUTA+IT                      | 00002210 |
|     | IF(SWTCH1)GO TO 115                 | 00002220 |
|     | IF(SWTCH4)CALL STRAD2               | 00002230 |
| 130 | IF(IPL0T1.OR.IPL0T2)GO TO 135       | 00002240 |
| C   |                                     | 00002250 |
| C   | STORE RADAR DATA FOR OUTPUT         | 00002260 |
| C   |                                     | 00002270 |
| 110 | IF(SWTCH4)GO TO 120                 | 00002280 |
|     | IF(IOUTA.GE.INCOUT)CALL STORD       | 00002290 |
|     | IF(NREC2.GE.NOFF2)CALL OUTRDE       | 00002300 |

|   |   |          |
|---|---|----------|
| C | 120 IF(SWCH6)GO TO 125                            | 00002310 |
|   | IF(.NOT.SWCH1.AND.SWCH5)GO TO 140                 | 00002320 |
|   | GO TO 125   | 00002330 |
| C |   | 00002340 |
| C | STORE OUTPUT DATA FOR LAST VISIBLE POINT          | 00002350 |
| C |   | 00002360 |
| C |   | 00002370 |
|   | 140 SWCH6=.TRUE.                                  | 00002380 |
|   | CALL STRADL                                       | 00002390 |
|   | IF(NREC2.NE.0)CALL OUTDR                          | 00002400 |
|   | CALL OUTOP  | 00002410 |
| C |   | 00002420 |
| C | RE-INITIALIZE SWITCHES                            | 00002430 |
| C |   | 00002440 |
|   | SWCH1=.TRUE.                                      | 00002450 |
|   | SWCH4=.TRUE.                                      | 00002460 |
|   | IF(IPL0T1.OR.IPL0T2)GO TO 145                     | 00002470 |
|   | GO TO 125   | 00002480 |
| C |   | 00002490 |
| C | OUTPUT DATA ON PLOT FILE UP TO LAST VISIBLE POINT | 00002500 |
| C |   | 00002510 |
|   | 145 SWCH2=.TRUE.                                  | 00002520 |
|   | IF(NREC3.NE.0)CALL PLTAP1                         | 00002530 |
|   | CALL PLTAP2                                       | 00002540 |
|   | GO TO 125   | 00002550 |
| C |   | 00002560 |
|   | 135 IF(SWCH2)CALL PLTAP                           | 00002570 |
|   | SWCH2=.FALSE.                                     | 00002580 |
|   | SWCH7=.FALSE.                                     | 00002590 |
| C |   | 00002600 |
| C | STORE RADAR DATA FOR PLOTTING                     | 00002610 |
| C |   | 00002620 |
|   | CALL STORTP                                       | 00002630 |
| C |   | 00002640 |
| C | OUTPUT DATA ON PLOT TAPE/FILE                     | 00002650 |
| C |   | 00002660 |
|   | IF(NREC3.GE.NOFF3)CALL PLTAP1                     | 00002670 |
|   | GO TO 110   | 00002680 |
|   | 115 SWCH1=.FALSE.                                 | 00002690 |
|   | SWCH8=.FALSE.                                     | 00002700 |
|   | CALL STORAD                                       | 00002710 |
|   | GO TO 130   | 00002720 |
|   | 125 CONTINUE                                      | 00002730 |
|   | T=T+TINC  | 00002740 |
|   | 300 CONTINUE                                      | 00002750 |
|   | GO TO 100   | 00002760 |
| C |   | 00002770 |
| C | PRINT OUT RADAR DATA                              | 00002780 |
| C |   | 00002790 |
|   | 200 CONTINUE                                      | 00002800 |
|   | IF(NREC7.EQ.0)T=T-TINC                            | 00002810 |
|   | IF(.NOT.SWCH6)GO TO 23                            | 00002820 |



|      |  |          |
|------|--|----------|
| 24   | IF(NREC2,NE,0)CALL OUTDR                       | 00002830 |
|      | CALL OUTDR                                     | 00002840 |
|      | CALL PRINTR                                    | 00002850 |
|      | IF(SWTC8)CALL NOTVIS                           | 00002860 |
|      | IF(SWTC7)GO TO 500                             | 00002870 |
| C    |  | 00002880 |
| C    | OUTPUT LAST RECORDS ON PLOT TAPE/FILE          | 00002890 |
| C    |  | 00002900 |
|      | IF(SWTC2)GO TO 22                              | 00002910 |
|      | IF(NREC3,NE,0)CALL PLTAP1                      | 00002920 |
|      | CALL PLTAP2                                    | 00002930 |
|      | CALL PLTAP3                                    | 00002940 |
|      | GO TO 500                                      | 00002950 |
| 22   | CONTINUE                                       | 00002960 |
|      | CALL PLTAP3                                    | 00002970 |
|      | GO TO 500                                      | 00002980 |
| 23   | IF(T.LT.TIMES+0.01)GO TO 24                    | 00002990 |
|      | CALL CONVER                                    | 00003000 |
|      | IF(E.GT.ELIM)GO TO 24                          | 00003010 |
|      | CALL STRADL                                    | 00003020 |
|      | GO TO 24                                       | 00003030 |
| 500  | CONTINUE                                       | 00003040 |
| 17   | M=M+1  | 00003045 |
|      | IF(M,EQ,2,AND,KZ)M=4                           | 00003046 |
|      | IF(M.LE,ITM)GO TO 26                           | 00003047 |
|      | IF(IOUT3)GO TO 1010                            | 00003050 |
| 1010 | STOP   | 00003060 |
| C    |  | 00003070 |
| C    | COMPUTE RADAR PARAMETER DIFFERENCES            | 00003080 |
| C    |  | 00003090 |
| C    | WRITE NOMINAL TRAJECTORY ON A SEPARATE FILE    | 00003095 |
| C    |  | 00003096 |
| 1000 | CALL OUTNM                                     | 00003100 |
| C    |  | 00003106 |
| C    | READ AND STORE TIMES OF SIGHTING               | 00003110 |
| C    |  | 00003120 |
|      | CALL TIMEST                                    | 00003130 |
| C    |  | 00003135 |
| C    | MAIN PROCESSING LOOP PARAMETER DIFFERENCES     | 00003140 |
| C    |  | 00003150 |
|      | INOM = 1                                       | 00003160 |
|      | I=4  | 00003170 |
|      | IPASS=1  | 00003180 |
|      | IF(.NOT,KZ)I=1                                 | 00003190 |
|      | IF (.NOT,KZ)INOM=3                             | 00003200 |
| C    |  | 00003204 |
| C    | LOOP ON SITES                                  | 00003205 |
| C    |  | 00003206 |
| 1060 | J=1  | 00003210 |
| 1040 | II=NSIGHT(INOM,J)                              | 00003220 |
|      | IF(TIMES(I,J,1).GT.TIMES(INOM,J,II))GO TO 1020 | 00003230 |
|      | II=NSIGHT(I,J)                                 | 00003240 |

|   |  |          |
|---|--|----------|
| C | IF(TIMES1(INOM,J,1).GT.TIMESF(I,J,II))GO TO 1020         | 00003250 |
| C | DETERMINE THE INTERSECTIONS OF TIME SETS                 | 00003260 |
| C | CALL INTER   | 00003270 |
| C | INPUT RADAR DATA CORRESPONDING TO TIME SET INTERSECTIONS | 00003280 |
| C | CALL INTDAT  | 00003290 |
|   | 1020 IF(J.GE.NSITE)GO TO 1030                            | 00003300 |
|   | J=J+1  | 00003310 |
|   | GO TO 1040   | 00003320 |
|   | 1030 IF(I.GE.ITM)STOP                                    | 00003330 |
|   | IF(INOM.EQ.1)GO TO 1.50                                  | 00004000 |
|   | IF(IPASS.NE.1)GO TO 1050                                 | 00004010 |
|   | IPASS=2  | 00004020 |
|   | I=3  | 00004030 |
|   | 1050 I=I+1   | 00004040 |
|   | GO TO 1060   | 00004050 |
|   | END  | 00004060 |
|   | ***EOF   | 00004070 |
|   |  | 00004080 |
|   |  | 00004090 |
|   |  | 00004100 |
|   |  | 00005010 |

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17.491

## ATMOSPHERIC MODEL

LAB

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1  CATNOSP      ATMOSPHERIC MODEL
2  SUBROUTINE ATMOSP
3  C  THIS ROUTINE COMPUTES THE ATMOSPHERIC DENSITY (IN SLUGS PER FEET
4  C  CUBED) FROM THE 1959 ARDC MODEL ATMOSPHERE. ABOVE 105 KILOMETERS
5  C  THE DENSITY IS SET EQUAL TO ZERO. BELOW THIS VALUE, THE LAYERS
6  C  ASSUME AN ISOTHERMAL OR LINEAR TEMPERATURE LAPSE RATE SECTION.
7
8  DOUBLE PRECISION HP,H2P,SK3,HB,PB,SK1,SK2,CD,ST
9  DOUBLE PRECISION P1,ZK,B1
10 DOUBLE PRECISION TS,T,H,V,RSL,PZ,XYZ
11 COMMON/TS/T,H,XYZ,RSL,PZ
12 COMMON/GE/ZK,B1,P1
13 HP=.348D0*H
14 H2P=HP/(1.0D0+HP/.6356766D7)
15 IF(HP-5.3D4)20,25,25
16 20 IF(HP-4.7D4)21,29,29
17 21 IF(HP-2.5D4)22,30,30
18 22 IF(HP-1.1D4)23,31,31
19 23 IF(HP)28,28,32
20 25 IF(HP-7.9D4)33,33,26
21 26 IF(HP-9.0D4)34,34,27
22 27 IF(HP-1.05D5)35,35,28
23 28 PZ=0.0D0
24 Q1=0.0D0
25 Q2=0.0D0
26 Q3=0.0D0
27 RETURN
28 29 SK3=.120869D-3
29 HB=4.7D4
30 PB=2.8804D-6
31 GO TO 37
32 30 SK1=.138466D-4
33 SK2=1.13883D1
34 PB=7.765D-5
35 HB=2.5D4
36 GO TO 36
37 31 SK3=.157689D-3
38 HB=1.1D4
39 PB=7.62D-4
40 GO TO 37
41 32 SK1=-.225569D-4
42 SK2=-5.25612D0
43 PB=2.37692D-3
44 HB=0.0D0
45 GO TO 36
46 33 SK1=-.159202D-4
47 SK2=-7.59218D0
48 PB=1.39468D-6
49 HB=5.3D4
50 GO TO 36
51 34 SK3=.206234D-3
52 HB=7.9D4

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# ATMOSPHERIC MODEL

LAB

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53      PB=4.1189D-8
54      GO TO 27
55      35  SK1=.241458D-4
56          SK2=8.3442D0
57          PM=4.261D-9
58          MB=9.0D4
59      36  CD=1.0D0+SK1*(H2P-HB)
60          ST=-(1.0D0+SK2)
61          PZ= PB*(CD**ST)
62          RETURN
63      37  PZ=PB*DEXP(-SK3*(H2P-HB))
64          RETURN
65          END

```



```

1  CBALCOF      BALLISTIC COEFFICIENTS
2  SUBROUTINE BALCOF
3      DOUBLE PRECISION  Z1,Z2,Z3,Z4,Z5,B1,ZK
4      DOUBLE PRECISION HB,HB2,HB3,HB4,P1,P2,P3,P4
5      DOUBLE PRECISION XL1,XL2,XL3,XL4,XL5
6      DOUBLE PRECISION GM,TM,X,T,H,XYZ,RSL,PZ
7      DOUBLE PRECISION XD,XDD
8      DOUBLE PRECISION P5,P7,P9,P11,P13,P14,P8
9      COMMON/BS/X(3),XD(3),XDD(3)
10     COMMON/AX/TM,M/TS/T,H,XYZ,RSL,PZ
11     COMMON/GE/ZK,B1,P1
12     DATA GM/1.407639D16/
13     HB = H*1.D-3
14     IF (HB.GE.3.445D2) GO TO 90
15     HB2 = HB*HB
16     HB3 = HB2*HB
17     HB4 = HB2*HB2
18     IF(M.LE.3) GO TO 3
19     IF(M.EQ.4) GO TO 4
20
21 C      ***** M = 3      RV-9-2B      *****
22
23     3      P1 = 0.0D0
24           P2 = 9.0D1
25           P3 = 1.8D2
26           P4 = 2.7D2
27           IF(HB.GE.P4)GO TO 18
28           IF(HB.GE.P3) GO TO 20
29           IF(HB.GE.P2) GO TO 22
30           IF(HB.GE.P1) GO TO 24
31           GO TO 90
32     18      XL1 = .8473D-7
33           XL2 = .3864D-5
34           XL3 = -.4263D-1
35           XL4 = .1417D+2
36           XL5 = -.1124D+4
37           GO TO 2
38     20      XL1 = .2573D-6
39           XL2 = -.4352D-4
40           XL3 = -.4597D-1
41           XL4 = .1253D+2
42           XL5 = -.4204D+3
43           GO TO 2
44     22      XL1 = -.1944D-5
45           XL2 = .7391D-3
46           XL3 = -.1040D0
47           XL4 = .7063D+1
48           XL5 = .1649D3
49           GO TO 2
50     24      XL1 = .1835D-5
51           XL2 = -.2271D-3
52           XL3 = -.5727D-2

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## BALLISTIC COEFFICIENTS

L

```

53      XL4 = .2765D1
54      XL5 = .2008D3
55      GO TO 2
56
57      C      *+*** H = 4      BOOSTER *****
58
59      4      P1 = 5.0D1
60            P2 = 1.40D2
61            P4 = 2.3D2
62            P5 = 3.1D2
63            IF(HB.GT.P5) GO TO 90
64            IF(HB.GE.P4) GO TO 40
65            IF(HB.GE.P2) GO TO 41
66            IF(HB.GE.P1) GO TO 42
67            GO TO 90
68      40      XL1 = .3423D-7
69            XL2 = -.6148D-5
70            XL3 = -.7003D-2
71            XL4 = .2501D2
72            XL5 = -.1995D3
73            GO TO 2
74      41      XL1 = .5097D-6
75            XL2 = -.2590D-3
76            XL3 = .3502D-1
77            XL4 = .6331D-1
78            XL5 = -.1343D3
79            GO TO 2
80      42      XL1 = -.8529D-6
81            XL2 = .4197D-3
82            XL3 = -.7661D-1
83            XL4 = .6386D1
84            XL5 = -.1654D3
85            GO TO 2
86      90      ZK = 0.0D0
87            B1 = 0.0D0
88            GO TO 100
89      2      Z1 = XL1*HB4
90            Z2 = XL2*HB3
91            Z3 = XL3*HB2
92            Z4 = XL4*HB
93            Z5 = XL5
94            B1 = Z1+Z2+Z3+Z4+Z5
95            ZK = GM/(2.0D0*X(1)*X(1)*B1)
96      5      CONTINUE
97      100     RETURN
98      END

```

```

1  CCONVER  CONVERT TO RADAR COORDINATES
2  SUBROUTINE CONVER
3  C  INPUT/OUTPUT MOD 1
4  C  THIS ROUTINE DETERMINES WHETHER THE SENSOR UNDER CONSIDERATION IS
5  C  CAPABLE OF OBSERVING THE VEHICLE AT ANY TIME AND OF COMPUTING THE
6  C  RANGE, RANGE-RATE, RANGE-ACCELERATION, AZIMUTH, AZIMUTH-RATE, AZIMUTH
7  C  ACCELERATION, CO-ELEVATION, CO-ELEVATION RATE, CO-ELEVATION
8  C  ACCELERATION OF THE VEHICLE RELATIVE TO ANY VISIBLE SENSOR. IF THE
9  C  SENSOR OBSERVES THE VEHICLE, ALL DATA IS
10 C  PRINTED IN THE TOPOCENTRIC COORDINATE SYSTEM.
11
12  DOUBLE PRECISION COST, COSL, SINT, SINL, ZEX, Y, Z, EXD, YD, ZD, XDP, YDP, ZDP
13  *JREQ, W2, W3, W4, W5, XS, YS, ZS, SRS, RS, RSD, XNUM1, XNUM2, XNUM3,
14  *THOPI, EFFAK, AHREQ
15  *X1, X3
16  *RS1, RSD1
17  DOUBLE PRECISION XNUM, XNUM, S1K, W9, S2K, S3K, S1K2, S2K2, OPS, E, W6, W7
18  DOUBLE PRECISION XNLH, ED, SIG, W14, W15, SIGD, RSD, SIGDD, EDD
19  DOUBLE PRECISION SC1, SC2, T, H, XYZ, RSL, PZ, H, W, P, Q
20  DOUBLE PRECISION X, XB, XDD
21  DOUBLE PRECISION EL, ELD, ELDD, REGAM, HDBETA
22  DOUBLE PRECISION TN, STN, TM
23  DOUBLE PRECISION P1, HALFPI, THAPI, ARSIN, COSLT, GNUM, GDEM, BETA, GAM
24  DOUBLE PRECISION AH, XPUM, VPRIME, GNUM2, COSB, BNUM
25  DOUBLE PRECISION HX, VO, THE, GLAM, THES, GLAMS
26  COMMON/TS/T, H, XYZ, RSL, PZ
27  COMMON/BS/X(3), XD(3), XDD(3)
28  COMMON/AX/TM, H
29  COMMON/MS/ GAM, BETA, RX, VO, THE, GLAM, SC1, SC2, AH, THES, GLAMS
30  *ELIM/ELIM
31  *CONCOM/RS, RSD, RSD, SIG, SIGD, SIGDD, EL, ELD, ELDD, REGAM, HDBETA
32  *OUTCOM/X1, X3
33  *TIME8/TIME8
34  *OPTION/IOUT1, IOUT2, KZ, IPLOT1, IPLOT2, KAT, SPHERE, OUTINC
35  *IOUT3
36  COMMON/W23459/W2, W3, W4, W5, W9
37  COMMON/E/E
38  LOGICAL IOUT1, IOUT2, KZ, IPLOT1, IPLOT2, KAT, SPHERE
39  *IOUT3
40  DATA EF/57.2957795130823208/, REQ/20925648.000/,
41  *AK/0.174532925199432957/, PI/3.14159265358979323/,
42  *HALFPI/1.57079632679489662/, THAPI/4.71238898038468986/,
43  *THOPI/6.28318530717958648/
44  COST=DCOS(X(2))
45  COSL=DCOS(X(3))
46  SINT=DSIN(X(2))
47  SINL=DSIN(X(3))
48  EX =X(1)*COST*COSL
49  Y  =-X(1)*COST*SINL
50  Z  =X(1)*SINT
51  EXD =XD(1)*COST*COSL-X(1)*XD(2)*SINT*COSL-X(1)*XD(3)*COST*SINL
52  YD  =-XD(1)*COST*SINL+X(1)*XD(2)*SINT*SINL-X(1)*XD(3)*COST*COSL

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## CONVERT TO RADAR COORDINATES

LA

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53      ZD = XDD(1)*SINT(X(1))*XD(2)*COST
54      XDP = (XDD(1)-X(1)*(XD(2)*XD(2))-X(1)*(XD(3)*XD(3)))*COST*DOB1
55      1      = (2.000*XD(1)*XD(2)+X(1)*XDD(2))*SINT*COBL
56      2      = (2.000*XD(1)*XD(3)+X(1)*XDD(3))*COST*SINL
57      3      = 2.000*X(1)*XD(2)*XD(3)*SINT*SINL
58      YDP = (XDD(1)+X(1)*(XD(2)*XD(2))-X(1)*(XD(3)*XD(3)))*COST*DOB1
59      1      = (2.000*XD(1)*XD(2)+X(1)*XDD(2))*SINT*SINL
60      2      = (X(1)*XDD(3)+2.000*XD(1)*XD(3))*COST*COBL
61      3      = 2.000*X(1)*XD(2)*XD(3)*SINT*COBL
62      ZDP = (XDD(1)-X(1)*XD(2)*XD(2))*SINT
63      1      = (2.000*XD(1)*XD(2)+X(1)*XDD(2))*COST
64      AHREQ = AH + REQ
65      XS = AHREQ*W3*W5
66      YS = AHREQ*W3*W4
67      ZS = AHREQ*W2
68      SRS = DSQRT(XS**2+YS**2+ZS**2)
69      S1K = ((EX-XS)*W2*W5+(Y-YS)*W2*W4+(Z-ZS)*W3)
70      S2K = X(1)*COST*DSIN(X(3)*W9)
71      S3K = (EX-XS)*W3*W5+(Y-YS)*W3*W4+(Z-ZS)*W2
72      S1K2 = S1K**2
73      S2K2 = S2K**2
74      S3K2 = S3K**2
75      RS1 = DSQRT(S1K2+S2K2+S3K2)
76      RSD1 = (EXD*(EX-XS)+YD*(Y-YS)+ZD*(Z-ZS))/RS1
77      XNUM1 = ((EX-XS)*XS)/RS1
78      XNUM2 = ((Y-YS)*YS)/RS1
79      XNUM3 = ((Z-ZS)*ZS)/RS1
80      XNUM = (XNUM1+XNUM2+XNUM3)/SRS
81      XNUM = (XNUM1+XNUM2+XNUM3)*RS1
82      OPS = DSQRT(S1K2+S2K2)
83      C ELEVATION ANGLE CONSTRAINT ON M01 TRAJECTORY SIMULATION
84      E = DATAN2(OPS,S3K)
85      IF(E.GT.ELIM) GO TO 200
86      47 EL = HAL*PI - E
87      RS = RS1
88      RSD = RSD1
89      TIME0 = T
90      X1 = X(1)
91      X3 = X(3)
92      45 W6 = DSIN(E)
93      W7 = DCOS(E)
94      XNUM = XS*EXD+YS*YD+ZS*ZD
95      ED = (-RS*XNUM+XNUM*RSD)/((SRS*(RS**2)*W6)
96      ELD = -ED
97      65 SIG = DATAN2(S2K,S1K)
98      IF(SIG.GE.0.000) GO TO 90
99      SIG = SIG+THOP1
100      90 W14 = DSIN(SIG)
101      W15 = DCOS(SIG)
102      IF(DABS(W14).GE.1.00-10.AND.W6.GT.0.000) GO TO 105
103      100 SIGD = 0.000
104      GO TO 110

```



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## CONVERT TO RADAR COORDINATES

LAF

```

105 105 SIGD = (EXD*W2*W5 + YD*W2*W4-ZD*W3 + (RSD*W6+RS*ED*W7)*W15)
106 17(RS*W6*W14)
107 110 XPUM1=(XS/RS)*(XDP/RS)
108 XPUM2=(YS/RS)*(YDP/RS)
109 XPUM3=(ZS/RS)*(ZDP/RS)
110 XPUM = (XPUM1+XPUM2+XPUM3)/W6
111 RSDD=((EX-XS)*XDP+(Y-YS)*YDP+(Z-ZS)*ZDP)
112 1 + (EXD*EXD+YD*YD+ZD*ZD-RSD*RSD)/RS
113 EDD = -XPUM + (XNUM/W6)*(RSDD/RS) = (ED*ED*W7)/W6 - 2.0D0*ED*RSD
114 +/RS
115 ELDD=-EDD
116 IF(DABS(W14).GE.1.0D-16.AND.W6.GT.0.0D0)GO TO 108
117 SIGDD=0.0D0
118 GO TO 109
119 108 SIGDD=(XDP*W2*W5+YDP*W2*W4-ZDP*W3-2.0D0*RSD*W6*W14*SIGD
120 1 -2.0D0*RS*W7*W14*ED*SIGD+2.0D0*RS*W8*W15*SIGD*SIGD
121 2 +2.0D0*RSD*W7*W15*ED*RSD*W6*W15*RS*EDD*W7*W15)/(RS*W6*W14)
122 109 CONTINUE
123 IF(.NOT.IOUT2)RETURN
124
125 C CALCULATION OF HEADING ANGLE(CLOCKWISE 0 TO 2PI)
126
127 COSLT = XD(3)*COST/XD(2)
128 BNUM = XD(3)*COST
129 IF (XD(2)) 1,2,3
130 C ZERO XD(2)
131 2 IF(BNUM) 4,5,6
132 C NEGATIVE BNUM
133 4 BETA = TIHAP1
134 GO TO 60
135 C ZERO BNUM
136 5 BETA = 1.0D1*PI
137 GO TO 60
138 C POSITIVE BNUM
139 6 BETA = HALFPI
140 GO TO 60
141 C NEGATIVE XD(2)
142 1 IF(BNUM) 7,8,9
143 C NEGATIVE OR POSITIVE BNUM
144 7 BETA = PI + DATAN(COSLT)
145 GO TO 60
146 9 BETA = PI + DATAN(COSLT)
147 GO TO 60
148 C ZERO BNUM
149 8 BETA = PI
150 GO TO 60
151 C POSITIVE XD(2)
152 3 IF(BNUM) 10,11,12
153 C NEGATIVE BNUM
154 10 BETA = TWOPI + DATAN(COSLT)
155 GO TO 60
156 C ZERO BNUM

```

2-76 15.050 CONVERT TO RADAR COORDINATES

LA

```

157      11 BETA = 0.0000
158      GO TO 60
159      C POSITIVE GRUM
160      12 BETA = DATAN(COSUT)
161      C CALCULATION OF RE/ENTRY ANGLE(CLOCKWISE 0 TO 2PI)
162      60 COSB = DCOS(BETA)
163      GNUM = X(1)*XD(2) / COSB
164      GDEM = XD(1)
165      IF(GDEM) 13,14,15
166      C ZERO GDEM
167      14 IF (GNUM) 16,17,18
168      C NEGATIVE GNUM
169      16 ARSIN = TIHARI
170      GO TO 62
171      C ZERO GNUM
172      17 ARSIN = 1.001*PI
173      GO TO 62
174      C POSITIVE GNUM
175      18 ARSIN = HALFPI
176      GO TO 62
177      C NEGATIVE GDEM
178      13 IF(GNUM) 19,20,24
179      C NEGATIVE OR POSITIVE GNUM
180      19 ARSIN = THOP1 + DATAN2(GNUM,GDEM)
181      GO TO 62
182      24 ARSIN = DATAN2(GNUM,GDEM)
183      GO TO 62
184      C ZERO GNUM
185      20 ARSIN = PI
186      GO TO 62
187      C POSITIVE GDEM
188      15 IF (GNUM) 21,22,23
189      C NEGATIVE GNUM
190      21 ARSIN = THOP1 + DATAN2 (GNUM,GDEM)
191      GO TO 62
192      C ZERO GNUM
193      22 ARSIN = 0.000
194      GO TO 62
195      C POSITIVE GNUM
196      23 ARSIN = DATAN2 ( GNUM,GDEM)
197      GO TO 62
198      62 GAM = ARSIN
199      REGAM = GAM
200      HDBETA = BETA
201      200 RETURN
202      END

```

MEMORY EXPANDED. USE SLIMITS OR CORE= OPTION FOR NEXT RUN

```

1  CEQTNX      COMPUTE ACCELERATION COMPONENTS
2  SUBROUTINE EQTNX
3  C THIS ROUTINE COMPUTES THE VEHICLE'S ACCELERATION COMPONENTS
4  C REQUIRING VARIABLE BALLISTIC COEFFICIENTS AND DENSITY FROM
5  C ROUTINES BALCOF AND ATMOSPHE, RESPECTIVELY
6
7  DOUBLE PRECISION W,RSL,PZ,T
8  DOUBLE PRECISION V6,EL2,EL3,EL4,EL5,EL6,AA
9  DOUBLE PRECISION DV,XYZ,ZK,S1,S2,S3,S4,S5,VA,VDD,VD,S23,Q1,Q2,Q3
10 DOUBLE PRECISION X,XB,XDD
11 DOUBLE PRECISION A,R,W,TM,B1
12 DOUBLE PRECISION P1
13 LOGICAL IOUT1,IOUT2,IOUT3,KZ,KAT,SPHERE,IPLOT1,IPLOT2
14 DIMENSION DV(5)
15 COMMON/BS/X(3),XD(3),XDD(3)
16 COMMON/TS/T,W,XYZ,RSL,PZ
17 COMMON/A/R,W
18 COMMON/GE/ZK,B1,P1
19 * /OPTION/IOUT1,IOUT2,KZ,IPLOT1,IPLOT2,KAT,SPHERE,OUTINC,IOUT3
20 DATA DV/2.4216704D12,4.0,0D0/
21 * /S6/2.0D0/
22 S1=DCOS(X(2))
23 S2=DSIN(X(2))
24 S3=DSIN(S6*X(2))
25 S4=DCOS(S6*X(2))
26 RSL = R
27 W = X(1)/RSL
28
29 IF(.NOT.KAT)GO TO 31
30 CALL BALCOF
31 CALL ATMOSP
32
33 31 VA = (XD(1)*XD(1))/(X(1)*X(1)+XD(2)*XD(2)+(S1*(XD(3)+W))**.2
34 C VEHICLE'S INERTIAL SPEED (COMPUTED OUTPUT)
35 XYZ=X(1)*DSQRT(VA)
36 VDD= XD(1)*XB(1)+ X(1)*XD(2)*X(1)*XD(2)+(X(1)*(XD(3)-W)*S1)**.2
37 C VEHICLE SPEED WRT THE ATMOSPHERIC WIND
38 VD=DSQRT(VDD)
39 S23=-PZ*ZK*VD
40 C DRAG FORCES CONJUGATE TO GEO.RADIUS,LATITUDE,LONGITUDE(FT/MIN/MIN)
41 Q1= S23*X(1)
42 Q2= S23*X(2)
43 Q3= S23*(XD(3)-W)
44 V6 = R/X(1)
45 EL2=X(1)*XD(2)*XD(2)+0.5D0*(1.0D0+S4)*(W*X(3))*(W*X(3))*X(1)
46 EL3=DV(1)/X(1)*V6+DV(2)/X(1)*V6**3*(3.0D0*S4-1.0D0)
47 EL4=DV(3)/X(1)*V6**5*(35.0D0*S4*S4-10.0D0*S4-13.0D0)
48 C GEOCENTRIC RADIAL ACCELERATION (FT/MIN/MIN)
49 XDD(1)= EL2-EL3-EL4+Q1
50 EL5=(-S6*X(2)*XD(1))/X(1)-0.5D0*S3*(W*X(3))*(W*X(3))
51 EL6=-DV(4)/(X(1)*X(1))*V6**3*S3+DV(5)/(X(1)*X(1))+V6**5*S3*(1.0D0-
52 17.0D0*S4)

```

2-76 15.089 COMPUTE ACCELERATION COMPONENTS

LA

```
53 C GEOCENTRIC LATITUDE ANGULAR ACCELERATION (RAD/MIN/MIN)
54 XDD(2)=EL5.EL6.02
55 AA=-1.000*(W*XD(3))
56 C GEOCENTRIC LONGITUDE ANGULAR ACCELERATION (RAD/MIN/MIN)
57 XDD(3)=AA*(S6*XD(1)/X(1))-AA*(S8*XD(2)+S2)/S1.03
58 RETURN
59 END
```



```

1  CICERBM      GEOCENTRIC SPHERICAL COMPONENTS
2  SUBROUTINE ICERBM
3
4  C      INPUT/OUTPUT MOD 2; MULTIPLE SITE/TRAJECTORY VERSION
5
6  C      THIS ROUTINE ACCEPTS BOUNDARY CONDITIONS OF VEHICLE AND COMPUTES
7  C      GEOCENTRIC SPHERICAL COMPONENTS OF POSITION AND VELOCITY VECTORS.
8  C      IN ADDITION, PERTURBATION TECHNIQUE IS INCORPORATED TO COMPUTE
9  C      THE RESULTANT EFFECT OF SINGULAR OR MULTIPLE PERTURBATIONS OF
10 C      NOMINAL COMPONENTS ON VELOCITY.
11
12 DOUBLE PRECISION VO,RAT,XX,ZK,B1,P1
13 DOUBLE PRECISION RDP,RTDP,RLDP,C13,GMU,CA,GAM,BETA,GLAM,HX,THE,RO
14 DOUBLE PRECISION X,Y,XB,XDD
15 DOUBLE PRECISION SC1,SC2,T,H,XYZ,RSL,PZ,W,H
16 DOUBLE PRECISION XN,XDN,XN1(20),XDN1(20)
17 DOUBLE PRECISION COSGAM,COSBET,SINGAM,SINBET,V2,A,B,C
18 DOUBLE PRECISION SN1,VBODR,VBO
19 DOUBLE PRECISION RATN
20 DOUBLE PRECISION TN,STN,TM
21 DOUBLE PRECISION THES,GLAMS,AH
22 COMMON/BS/X(3),XD(3),XDD(3)
23 COMMON/TS/T,H,XYZ,RSL,PZ
24 COMMON/AXR,W/M2TRAJ/XX(11)
25 COMMON/AX/TM,MT/QE/ZK,B1,P1
26 COMMON/MS/ GAM,BETA,RX,VO,THE,GLAM,SC1,SC2,AH,THES,GLAMS
27 *ABC/A(20),B(20),C(20)
28 *OPTION/IOUT1,IOUT2,KZ,IPLOT1,IPLOT2,KAT,SPHERE,OUTINC,IOUT3
29 *OPT1/INERTL
30 DIMENSION RDP(20),RTDP(20),RLDP(20),XN(3),XDN(3)
31 LOGICAL IOUT1,IOUT2,KZ,IPLOT1,IPLOT2,KAT,SPHERE,IOUT3,INERTL
32 DATA C13/0.01745329251994329577,GMU/5.0675004D19/
33 IF(MT-2)6,10,16
34 6 CONTINUE
35 RO = R + HX
36 XD(1)=VO*DCOS(GAM*C13)
37 IF(GAM.EQ.90.0D0)XD(1)=0.0D0
38 XD(2)=VO/RO*DSIN(GAM*C13)*DCOS(BETA*C13)
39 RAT=RO*DCOS(THE*C13)
40 XD(3)=VO*DSIN(GAM*C13)*DSIN(BETA*C13)/RAT
41 IF(INERTL)XD(3)=XD(3)*W
42 X(1)=RO
43 X(2)= THE*C13
44 X(3)= GLAM*C13
45 IF(.NOT.KZ)GO TO 30
46 DO 19 I=1,3
47   XN1(I) = X(I)
48 15 XDN1(I) = XD(I)
49 30 RETURN
50
51 C INITIAL BOUNDARY CONDITIONS TO SIMULATE TIMEWISE BACKWARD TRAJECTORY
52

```

```

53      10 RO = 1.38333730100
54        X(1) = XM(1)
55        X(2) = TME9*C13
56        X(3) = QUAMS*C13
57        XD(1) = XX(4)
58        XD(2) = XX(5)
59        XD(3) = XX(6)
60        XDD(1) = XX(7)
61        XDD(2) = XX(8)
62        XDD(3) = XX(9)
63        ZK = XX(10)
64        PZ = XX(11)
65      RETURN
66      16 IF(MT.GT.3)GO TO 39
67        DO 10 I = 1,3
68        XN(I) = X(I)
69        XDN(I) = XD(I)
70      18 CONTINUE
71      RETURN
72      35 IF(,NOT,KZ)GO TO 20
73        DO 40 I=1,3
74        X(I) = XN1(I)
75        XD(I) = XDN1(I)
76        XN(I) = XN1(I)
77      40 XDN(I) = XDN1(I)
78        GO TO 45
79      20 DO 25 I = 1,3
80        X(I) = XN(I)
81      25 CONTINUE
82      45 SN1 = DCOS(XN(2)*C13)
83        VBODR = DSQRT((XDN1(1)/XN(1))**2 + XDN(2)*XDN(2)*(SN1*XDN(3))**2)
84        VBO = XN(1) * VBODR
85        BETA = DATAN2(XDN(3)*SN1 ,XDN(2))
86        COSBET = DCOS(BETA)
87        SINBET = DSIN(BETA)
88        COSGAM = XDN(1) / VBO
89        SINGAM = XDN(2) / (VBODR * COSBET)
90        M = MT-3
91        V2 = B(M)*SINGAM*C(M)*COSGAM
92        RDP(M) = (-B(M)*COSGAM*C(M)*SINGAM)*60.000
93        RTDP(M) = (-V2*COSBET+A(M)*SINBET)*60.000
94        RLDP(M) = (-V2*SINBET+A(M)*COSBET)*60.000
95        XD(1) = XDN(1) + RDP(M)
96        XD(2) = XDN(2) + RTDP(M)/XN(1)
97        RATN = XN(1)*DCOS(XN(2)*C13)
98        XD(3) = XDN(3) + RLDP(M)/RATN
99      RETURN
100     END

```

QUALITY OR NON-EQUALITY COMPARISON MAY NOT BE MEANINGFUL IN LOGICAL IF EXPRESSIONS

```

CINIT      INITIALIZATION SUBROUTINE      00000010
SUBROUTINE INITIAL      00000020
C          INPUT/OUTPUT MOD 2,MULTIPLE SITE/TRAJECTORY VERSION      00000030
C          THIS SUBROUTINE PERFORMS SOME OF THE INITIALIZATION NEEDED FOR THE 00000040
C          PROGRAM, ESPECIALLY FOR PRODUCING OUTPUT.      00000050
COMMON/INOUT/INCOUT,IOUT,NOFF1,NOFF2,NOFF3,IOUTA      00000060
*PTO/TO/TS/T,H,XYZ,RSL,PZ      00000070
*POPTION/IOUT1,IOUT2,KZ,IPL0T1,IPL0T2,KAT,SPHERE,OUTINC,IOUT3      00000080
*RTD/RTD6,RTD36,F36,F6080,FERU      00000090
COMMON/W23459/W2,W3,W4,W5,W9      00000100
*MS/GAM,BETA,HX,VO,THE,GLAM,SC1,SC2,AH,THES,GLAMS      00000110
COMMON/GE/ZK,B1,P1/A/R,W/ST/P(3),Q(3)      00000120
*GEOXK/GEO,XK/AX,TM,M      00000130
*SWSW/SWCH1,SWCH2/SW10/SWCH10      00000140
*SW3SW4/SWCH3,SWCH4      00000150
*SW5SW6/SWCH5,SWCH6      00000160
*SW7/SWCH7/SW8/SWCH8/SW9/SWCH9      00000170
*NR/NREC1,NREC2,NREC3,NREC4,NREC5,NREC      00000180
*NR6/NREC6/IT2/IT2,IT      00000190
*TIME5/TIME5/TIME1/TIME1,TIMES      00000200
COMMON/NR7/NREC7,NOFF4      00000210
*NSITES/NSITE,SLAT(20),SLONG(20),SALT(20)      00000220
*ISITE/ISITE      00000230
LOGICAL IOUT1,IOUT2,KZ,IPL0T1,IPL0T2,KAT,SPHERE,IOUT3      00000240
LOGICAL SWCH1,SWCH2,SWCH10      00000250
LOGICAL SWCH3,SWCH4      00000260
LOGICAL SWCH5,SWCH6      00000270
LOGICAL SWCH7,SWCH8,SWCH9      00000280
DOUBLE PRECISION ZK,B1,P1,R,W,GEO,XK,P,Q      00000290
DOUBLE PRECISION W2,W3,W4,W5,W9,GAM,BETA,HX,VO,THE,GLAM,SC1,SC2,      00000300
AH,THES,GLAMS,AK,W10,TO,T,H,XYZ,RSL,PZ,TM      00000310
*,SLAT,SLONG,SALT,TIME1,TIMES      00000320
DATA AK/0.0174532925199432957/      00000330
RTD = 57.295780      00000340
RTD60 = RTD/60      00000350
RTD36 = RTD/360      00000360
F36 = 1.0/36      00000370
F6080 = 1.0/6080      00000380
FERU = 1.0/20925640      00000390
T = 0.0D0      00000400
PZ = 0.0D0      00000410
ZK = 0.0D0      00000420
DO 11 I=1,3      00000430
P(I)=0.0D0      00000440
11 Q(I)=0.0D0      00000450
IF(M.NE.2)GO TO 2      00000460
T = TIME1      00000470
SWCH10 = .FALSE.      00000480
IF(T.LT.TIMES+TO)GO TO 2      00000490

```

|   |          |
|---|----------|
| SWCH10 = .TRUE.   | 00000530 |
| RT2 = (T-TIMES+1.0D-5)/TO   | 00000540 |
| 20 RNCOUT = (OUTINC + 1.0E+09)/TO                                     | 00000550 |
| ROUT = 0  | 00000560 |
| ROUTA = 0   | 00000570 |
| ROFF1 = 676   | 00000580 |
| RF(IOUT1)NOFF1=364  | 00000590 |
| ROFF2 = 624   | 00000600 |
| ROFF3 = NOFF2   | 00000610 |
| RF(IOUT2)NOFF2=364  | 00000620 |
| RF(IPLUT2)NOFF3=364   | 00000630 |
| ROFF4= 554  | 00000640 |
| RF(ISITE,EQ.0)GO TO 10  | 00000650 |
| SC1 = SLAT(ISITE)   | 00000660 |
| SC2 = SLONG(ISITE)  | 00000670 |
| AK = SALT(ISITE)  | 00000680 |
| W9=SC2*AK   | 00000690 |
| W10 = SC1*AK  | 00000700 |
| W2 = DSIN(W10)  | 00000710 |
| W3 = DCOS(W10)  | 00000720 |
| W4 = DSIN(W9)   | 00000730 |
| W5 = DCOS(W9)   | 00000740 |
| 10 TIME5 = 0.0  | 00000750 |
| RREC1 = 0   | 00000760 |
| RREC2 = 0   | 00000770 |
| RREC3 = 0   | 00000780 |
| RREC4 = 0   | 00000790 |
| RREC5 = 0   | 00000800 |
| RREC6 = 0   | 00000810 |
| RREC7=0   | 00000820 |
|   | 00000830 |
| C PHYSICAL CONSTANTS OF THE EARTH MODEL,EQUATORIAL RADIUS AND ANGULAR | 00000840 |
| C SPEED   | 00000850 |
|   | 00000860 |
| R = 20925640.00   | 00000870 |
| W=0.4375269048D-2   | 00000880 |
| AK=5.72961D1  | 00000890 |
|   | 00000900 |
| C UPPER VALUE OF THE TARGET'S GEOCENTRIC RADIAL DISTANCE(FT)          | 00000910 |
|   | 00000920 |
| GEO = 1.383337304D8   | 00000930 |
| P1 = 0.0D0  | 00000940 |
| SWTCH1 = .TRUE.   | 00000950 |
| SWTCH2 = .TRUE.   | 00000960 |
| SWTCH3 = .FALSE.  | 00000970 |
| SWTCH4 = .TRUE.   | 00000980 |
| SWTCH6 = .TRUE.   | 00000990 |
| SWTCH7 = .TRUE.   | 00001000 |
| SWTCH8=.TRUE.   | 00001010 |
| SWTCH9 = .TRUE.   | 00001020 |
| RETURN  | 00001030 |
| END   | 00001040 |



|    |       |  |          |
|----|-------|--|----------|
| C  | INPUT | INPUT SUBROUTINE   | 00001050 |
|    |       | SUBROUTINE INPUT   | 00001060 |
| C  |       | THIS ROUTINE PERFORMS THE INPUT FUNCTION THRU CARDS FOR THE PROGRAM. | 00001070 |
|    |       | COMMON/AX/TM,M/NTRAJ/ITM   | 00001080 |
|    |       | *FMS/GAM,BETA,HX,VO,THE,GLAM,SC1,SC2,AH,THES,GLAMS                   | 00001090 |
|    |       | *ELIM/ELIM/NSWTC/NSWTC   | 00001100 |
|    |       | *POPTION/IOUT1,IOUT2,KZ,IPLLOT1,IPLLOT2,KAT,SPHERE,OUTINC,IOUT3      | 00001110 |
|    |       | *POPT1/INERTL  | 00001120 |
|    |       | *FABC/A(20),B(20),C(20)  | 00001130 |
|    |       | COMMON/SITES/NSITE,SLAT(20),SLONG(20),SALT(20)                       | 00001140 |
|    |       | DOUBLE PRECISION GAM,BETA,HX,VO,THE,GLAM,SC1,SC2,AH,THES,GLAMS,TM,   | 00001150 |
|    |       | *ELIM,A,B,C,SLAT,SLONG,SALT  | 00001160 |
|    |       | LOGICAL IOUT1,IOUT2,KZ,IPLLOT1,IPLLOT2,KAT,SPHERE,IOUT3,IEOFF,INERTL | 00001170 |
|    |       | DATA DTR/0.17453293/   | 00001180 |
|    |       | NAMELIST/INPUT1/NTRAJ,TM,NSWTC                                       | 00001190 |
|    |       | *PINPUT2/IOUT1,IPLLOT1,IPLLOT2,IOUT2,KAT,KZ,SPHERE,OUTINC,IOUT3      | 00001200 |
|    |       | *,INERTL   | 00001210 |
|    |       | *PINPUT3/GAM,BETA,HX,VO,THE,GLAM,THES,GLAMS                          | 00001220 |
|    |       | *PINPUT4/NSITE,SLAT,SLONG,SALT,ELIM                                  | 00001230 |
|    |       | *PINPUT5/A,B,C   | 00001240 |
|    |       | CALL FLGEOF (3,IEOFF)  | 00001250 |
| C  |       | INPUT TRAJECTORY NUMBER, TIME LIMIT, MAIN PROCESSING SWITCH          | 00001260 |
|    |       | READ(5,INPUT1)   | 00001270 |
|    |       | IF(IEOFF)STOP  | 00001280 |
|    |       | ITM = NTRAJ  | 00001290 |
|    |       | WRITE(6,10)NTRAJ,TM,NSWTC  | 00001300 |
| 10 |       | FORMAT(1H1//5X,"MISSILE TRAJECTORY PROGRAM(MULTIPLE SITE/TRAJECTORY  | 00001310 |
|    |       | *I MOD) INPUTS"//714X,"PROGRAM CONTROLS"//10X,"NUMBER OF TRAJECTORY  | 00001320 |
|    |       | *YES SIMULATED(NTRAJ)",I6/710X,"MAXIMUM TIME FOR A TRAJECTORY(TM)",  | 00001330 |
|    |       | *615.5," MIN."//10X,"MAIN PROCESSING SWITCH(NSWTC)",I6)              | 00001340 |
| C  |       | INPUT OTHER PROGRAM CONTROLS   | 00001350 |
|    |       | READ(5,INPUT2)   | 00001360 |
|    |       | WRITE(6,60)IOUT1,IOUT2,OUTINC,IOUT3,KZ,IPLLOT1,IPLLOT2,KAT,SPHERE    | 00001370 |
| 60 |       | FORMAT(//10X,25HPRINT-OUT OPTION 1(IOUT1),L6,10X,25HPRINT-OUT OPTIO  | 00001380 |
|    |       | *ON 2(IOUT2),L6//1 X,51HINCREMENT BETWEEN TIME POINTS FOR PRINT-OUT  | 00001390 |
|    |       | *IOUTINC),F10.3,5H MIN.//1 X,54HPRINTOUT OPTION FOR RADAR PARAMETER  | 00001400 |
|    |       | *DIFFERENCES(IOUT3),L6.1 X,39HMINOMIAL TRAJECTORY SELECTION SWITCH(  | 00001410 |
|    |       | *KZ),L6//10X,25HPLOTTING OPTION 1(IPLLOT1),L6,10X,25HPLOTTING OPTIO  | 00001420 |
|    |       | *N 2(IPLLOT2),L6//1 X,29HATMOSPHERIC MODEL OPTION(KAT),L6//10X,29HSP | 00001430 |
|    |       | *HERICAL EARTH MODEL(SPHERE),L6)                                     | 00001440 |
|    |       | WRITE(6,65)INERTL  | 00001450 |
| 65 |       | FORMAT(//10X,32HINERTIAL VELOCITY OPTION(INERTL),L6)                 | 00001460 |

```

C      INPUT INITIAL STATE VECTOR OF THE INTERCEPTOR          00001570
C      INPUT SUBSATELLITE PARAMETERS                             00001580
                                                                00001590
                                                                00001600
                                                                00001610
                                                                00001620
                                                                00001630
      READ(5,INPUT3)                                             00001640
                                                                00001650
      WRITE(6,24)                                               00001660
24  FORMAT(///10X,60H"*****"//)                               00001670
      * *****//)                                             00001680
      WRITE(6,20)GAM,BETA,HX,VO,THE,GLAM                      00001690
20  FORMAT(///14X,39HINITIAL STATE VECTOR OF THE INTERCEPTOR///10X,36H00001700
      * RE-ENTRY ANGLE WRT THE VERTICAL(GAM),D15.5,5H DEG.//10X,38HHEADING00001710
      * ANGLE WRT RELATIVE NORTH(BETA),D15.5,5H DEG.//10X,32HHEIGHT OF MI00001720
      * SSILE AT BURNOUT(HX),D15.5,4H FT.//10X,52HVELOCITY OF MISSILE RELAC00001730
      * TIME TO BURNOUT AT EPOCH(VO),D17.10,9H FT./SEC.//10X,65HGEOCENTRIC00001740
      * LATITUDE AT BURNOUT, +NORTH AND -SOUTH OF EQUATOR(THE),D15.5,5H D00001750
      * EG.//10X,44HGEOCENTRIC LONGITUDE, EAST OF GREENWICH(GLAM),D15.5,5H 00001760
      * DEG.)                                                    00001770
      VO = VO*60.0                                              00001780
      WRITE(6,40)THES,GLAMS                                     00001790
40  FORMAT(///14X,23HSUBSATELLITE PARAMETERS///10X,55HGEOCENTRIC LATIT00001800
      * UDE, +NORTH AND -SOUTH OF EQUATOR(THES),D15.5,5H DEG.//10X,45HGEO00001810
      * ENTIC LONGITUDE, EAST OF GREENWICH(GLAMS),D15.5,5H DEG.) 00001820
      IF(NSWICH,EQ.160 TO 90)                                00001830
                                                                00001840
                                                                00001850
C      INPUT RADAR PARAMETERS                                   00001860
                                                                00001870
      READ(5,INPUT4)                                             00001880
                                                                00001890
                                                                00001900
                                                                00001910
                                                                00001920
                                                                00001930
      WRITE(6,24)                                               00001940
      WRITE(6,30)(I,SLAT(I),SLONG(I),SALT(I),I=1,NSITE)      00001950
30  FORMAT(///14X,"RADAR PARAMETERS"//10X,"SITE NUMBER",I6//10X,"GEOCE00001960
      * TRIC LATITUDE OF RADAR, +NORTH AND -SOUTH OF EQUATOR(SLAT)",D15.500001970
      * ," DEG."//10X,"GEOCENTRIC LONGITUDE OF RADAR, WEST OF GREENWICH(SLO00001980
      * RG)",D15.5," DEG."//10X,"ALTITUDE OF RADAR ABOVE SEA LEVEL(SALT)",00001990
      * D15.5," FT.")                                           00002000
      WRITE(6,50)ELIM                                           00002010
50  FORMAT(///10X,"MAXIMUM CO-LATITUDE OF ELEVATION ANGLE FOR WHICH CO00002020
      * VERAGE PARAMETERS ARE DETERMINED(ELIM)",D15.5," DEG.") 00002030
      ELIM = ELIM*DTR                                           00002040
90  IF(NTRAJ.LE.3)RETURN                                         00002050
                                                                00002060
C      INPUT VELOCITY PERTURBATIONS                             00002070
                                                                00002080
      READ(5,INPUT5)                                             00002090
                                                                00002100
                                                                00002110
                                                                00002120
                                                                00002130
                                                                00002140
                                                                00002150
      WRITE(6,24)                                               00002160
      NT=NTRAJ-3                                                00002170
      WRITE(6,70)(A(I),I=1,NT)                                  00002180
70  FORMAT(///14X,22HVELOCITY PERTURBATIONS//10X,95HOUT OF TRAJECTORY00002190
      * PLANE PERTURBATION, +EJECTED TO THE LEFT OF NOMINAL TRAJECTORY(A)00002200
      * IN FT./SEC.//(5X,5D17.5))                             00002210

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|  |         |
|--|---------|
| WRITE(6,B)(B(I),I=1,NT)  | 0002090 |
| 80 FORMAT(//1 X,80HIN PLANE PERTURBATION, +EJECTED BACKWARDS FROM NOMI | 0002100 |
| *INAL TRAJECTORY(3) IN FT./SEC.//(5X,5D17.5))                          | 0002110 |
| WRITE(6,B)(B(I),I=1,NT)  | 0002120 |
| 100 FORMAT(//1 X,78HIN PLANE PERTURBATION, +EJECTED UPWARDS FROM NOMI  | 0002130 |
| *AL TRAJECTORY(3) IN FT./SEC.//(5X,5D17.5))                            | 0002140 |
| RETURN   | 0002150 |
| END  | 0002160 |

|         |   |          |
|---------|---|----------|
| CINTRAJ | INPUT TRAJECTORY DATA FROM FILE                               | 00000050 |
| C       |   | 00000055 |
|         | SUBROUTINE INTRAJ   | 00000060 |
| C       |   | 00000065 |
| C       | THIS ROUTINE READS THE TRAJECTORY DATA PLACED ON A FILE       | 00000070 |
| C       | SO THAT RADAR COVERAGE PARAMETERS MAY BE COMPUTED,            | 00000080 |
| C       | IT WILL ALSO READ AND STORE RADAR DATA NEEDED FOR CALCULATING | 00000085 |
| C       | RADAR PARAMETER DIFFERENCES.                                  | 00000086 |
| C       |   | 00000087 |
|         | COMMON/NR7/NREC7,NOFF4/AX/TM,NTRJ/ISITE/ISITE                 | 00000090 |
|         | /OUTT/OUTTJ(500)/NSWTCH/NSWTCH                                | 00000100 |
|         | /JX/JX/TIME1/TIME1/BS/TE(9)                                   | 00000110 |
|         | /SITES/NSITE,SLAT(20),SLONG(20),SALT(20)                      | 00000115 |
|         | /TSIGHT/TIMEI(10,10,5),TIMESF(10,10,5),NSIGHT(10,10)          | 00000116 |
|         | /NTRAJ/NTRAJ/IJJ/INOM,1,JSITE,JSIGHT,TSTART,TEND              | 00000117 |
|         | /OPTION/IOUT1,IOUT2,KZ,IPLT1,IPLT2,KAT,SPHERE,OUTINC,         | 00000118 |
|         | IOUT3   | 00000119 |
|         | DOUBLE PRECISION TA,TM,SLAT,SLONG,SALT                        | 00000120 |
|         | LOGICAL IPLT2,EOF,SWTCH2,EOF10,                               | 00000125 |
|         | IOUT1,IOUT2,KZ,IPLT1,IPLT2,KAT,SPHERE,IOUT3                   | 00000126 |
|         | IF(NTRJ.GT.2)GO TO 20   | 00000130 |
|         | REWIND 9  | 00000140 |
|         | 50 READ(9)IREC,TIME1  | 00000150 |
|         | RETURN  | 00000160 |
|         | 20 IF(NSWTCH.EQ.2)GO TO 25                                    | 00000165 |
|         | IF(ISITE.NE.1)GO TO 3   | 00000170 |
|         | 35 BACKSPACE 9  | 00000171 |
|         | READ(9)IREC,NREC7   | 00000172 |
|         | IBACK=IREC  | 00000173 |
|         | IF(NREC7.EQ.0.AND.IREC.EQ.2)RETURN                            | 00000174 |
|         | 30 DO 40 IB=1,IBACK   | 00000180 |
|         | 40 BACKSPACE 9  | 00000190 |
|         | GO TO 50  | 00000200 |
|         | 25 IF(ISITE.EQ.1)GO TO 50                                     | 00000205 |
|         | IF(ISITE.EQ.2)GO TO 35  | 00000210 |
|         | GO TO 30  | 00000215 |
|         |   | 00000230 |
|         | ENTRY TRAJIN  | 00000240 |
|         | READ(9)IREC,NREC7   | 00000250 |
|         | IF(NREC7.EQ.0)RETURN  | 00000270 |
|         | NDATA = NREC7*9   | 00000280 |
|         | READ(9)IREC,(OUTTJ(I),I=1,NDATA)                              | 00000290 |
|         | RETURN  | 00000310 |
| C       |   | 00000320 |
|         | ENTRY TRAJX   | 00000330 |
| C       |   | 00000340 |
| C       | STORE TRAJECTORY DATA FROM INPUT BUFFER IN TRAJECTORY         | 00000350 |
| C       | APRAYS  | 00000360 |
| C       |   | 00000370 |
|         | II=1  | 00000380 |
|         | DO 10 JJ=JX,JX+9  | 00000390 |
|         | TR(II)=OUTTJ(JJ)  | 00000400 |



|   |          |
|---|----------|
| II=II+1   | 00000410 |
| 10 CONTINUE   | 00000420 |
| JX=JX+9   | 00000430 |
| RETURN  | 00000440 |
| C   | 00000450 |
| ENTRY TIMEST  | 00000460 |
| C   | 00000470 |
| C READ IN AND STORE TIMES OF SIGHTING FOR COMPUTATION OF        | 00000480 |
| C RADAR PARAMETER DIFFERENCES.                                  | 00000490 |
| C   | 00000500 |
| C   | 00000510 |
| C READ IN AND STORE TIMES OF SIGHTING OF NOMINAL TRAJECTORY     | 00000520 |
| C BY ALL RADAR SITES.   | 00000530 |
| C   | 00000540 |
| REWIND 11   | 00000550 |
| INOM=1  | 00000560 |
| IF(.NOT.KZ)INOM=3   | 00000570 |
| JJ=1  | 00000580 |
| II=0  | 00000590 |
| 130 READ(11)TIME3,IPLOT2,IO2,EOF                                | 00000600 |
| IF(EOF)GO TO 140  | 00000610 |
| II=II+1   | 00000620 |
| TIMES1(INOM,JJ,II)=TIME3  | 00000630 |
| 120 READ(11)NREC3,ITR,IS,EOF1,SWTCH2                            | 00000640 |
| IF(EOF1)GO TO 11  | 00000650 |
| READ(11)DUMMY   | 00000660 |
| GO TO 120   | 00000670 |
| 110 READ(11)TIME7   | 00000680 |
| TIMESF(INOM,JJ,II)=TIME7  | 00000690 |
| GO TO 130   | 00000700 |
| 100 NSIGHT(INOM,JJ)=II  | 00000710 |
| IF(JJ.EQ.NSITE)GO TO 140  | 00000720 |
| JJ=JJ+1   | 00000730 |
| II=0  | 00000740 |
| GO TO 130   | 00000750 |
| C   | 00000760 |
| C READ IN AND STORE TIMES OF SIGHTING OF ALL OTHER TRAJECTORIES | 00000770 |
| C BY ALL SITES.   | 00000780 |
| C   | 00000790 |
| 140 REWIND 11   | 00000795 |
| REWIND 1  | 00000800 |
| IF(.NOT.KZ)GO TO 15   | 00000805 |
| 195 JJ=1  | 00000810 |
| 190 READ(10)DUM,DUM,DUM,EOF                                     | 00000820 |
| IF(EOF)GO TO 160  | 00000830 |
| 180 READ(10)DUM,DUM,DUM,EOF10,DUM                               | 00000840 |
| IF(EOF10)GO TO 170  | 00000850 |
| READ(10)DUM   | 00000860 |
| GO TO 180   | 00000870 |
| 170 READ(10)DUM   | 00000880 |
| GO TO 190   | 00000890 |
| 160 IF(JJ.EQ.NSITE)GO TO 200                                    |          |

|     |   |          |
|-----|---|----------|
|     | JJ=JJ+1   | 00000900 |
|     | GO TO 190   | 00000910 |
| 150 | ITRAJ=1   | 00000915 |
|     | GO TO 270   | 00000917 |
| 200 | ITRAJ=4   | 00000920 |
| 270 | JJ=1  | 00000930 |
|     | II=0  | 00000950 |
| 220 | READ(10)TIME3,DUM,DUM,EOF                               | 00000960 |
|     | IF(EOF)GO TO 230  | 00000970 |
|     | II=II+1   | 00000980 |
|     | TIMES1(ITRAJ,JJ,II)=TIME3                               | 00000990 |
| 240 | READ(10)NREC3,ITR,IS,EOF1,ISWTCH2                       | 00001000 |
|     | IF(EOF1)GO TO 250                                       | 00001010 |
|     | READ(10)DUMMY   | 00001020 |
|     | GO TO 240   | 00001030 |
| 250 | READ(10)TIME7   | 00001040 |
|     | TIMESF(ITRAJ,JJ,II)=TIME7                               | 00001050 |
|     | GO TO 220   | 00001060 |
| 230 | NSIGHT(ITRAJ,JJ)=II                                     | 00001070 |
|     | IF(JJ.EQ.NSITE)GO TO 260                                | 00001080 |
|     | JJ=JJ+1   | 00001090 |
|     | II=0  | 00001100 |
|     | GO TO 220   | 00001110 |
| 260 | IF(ITRAJ.EQ.1)GO TO 195                                 | 00001115 |
|     | IF(ITRAJ.EQ.NTRAJ)GO TO 280                             | 00001120 |
|     | ITRAJ=ITRAJ+1   | 00001130 |
|     | GO TO 270   | 00001140 |
| 280 | REWIND 10   | 00001150 |
|     | RETURN  | 00001160 |
| C   |   | 00001170 |
| C   | ENTRY INTER   | 00001180 |
| C   |   | 00001190 |
| C   | DETERMINE THE INTERSECTIONS OF THE TIME SETS            | 00001200 |
|     |   | 00001210 |
|     | JSIGHT=1  | 00001220 |
|     | IF(TIMES1(INOM,JSITE,JSIGHT).GE.TIMES1(I,JSITE,JSIGHT)) | 00001230 |
| 8   | GO TO 290   | 00001240 |
|     | IF(TIMESF(INOM,JSITE,JSIGHT).LE.TIMESF(I,JSITE,JSIGHT)) | 00001250 |
| 8   | GO TO 300   | 00001260 |
|     | TSTART=TIMES1(I,JSITE,JSIGHT)                           | 00001270 |
|     | TEND=TIMESF(I,JSITE,JSIGHT)                             | 00001280 |
| 310 | RETURN  | 00001290 |
| 300 | TSTART=TIMES1(I,JSITE,JSIGHT)                           | 00001300 |
|     | TEND=TIMESF(INOM,JSITE,JSIGHT)                          | 00001310 |
|     | GO TO 310   | 00001320 |
| 290 | IF(TIMESF(INOM,JSITE,JSIGHT).GE.TIMESF(I,JSITE,JSIGHT)) | 00001330 |
| 8   | GO TO 320   | 00001340 |
|     | TSTART=TIMES1(INOM,JSITE,JSIGHT)                        | 00001350 |
|     | TEND=TIMESF(INOM,JSITE,JSIGHT)                          | 00001360 |
|     | GO TO 310   | 00001370 |
| 320 | TSTART=TIMES1(INOM,JSITE,JSIGHT)                        | 00001380 |
|     | TEND=TIMESF(I,JSITE,JSIGHT)                             | 00001390 |

GO TO 310  
END

00001400  
00001410

|   |  |          |
|---|--|----------|
| C | OUTPUT SUBROUTINE  | 00000010 |
|   | SUBROUTINE OUTPUT  | 00000020 |
| C | INPUT/OUTPUT MOD 2, MULTIPLE SITE/TRAJECTORY VERSION                   | 00000030 |
| C |  | 00000040 |
| C | THIS SUBROUTINE PRODUCES THE PRINT-OUT OF THE RESULTS OF A PROGRAM     | 00000050 |
| C | RUN. MISSILE/SATELLITE TRAJECTORY PARAMETERS (POSITION, VELOCITY, ETC) | 00000060 |
| C | ARE PRINTED-OUT. AS ARE THE TRAJECTORIES AS SEEN BY VARIOUS            | 00000070 |
| C | RADAR SITES.   | 00000080 |
| C | THIS ROUTINE ALSO IS USED FOR TEMPORARY STORAGE OF                     | 00000085 |
| C | TRAJECTORY AND RADAR DATA AND CAN WRITE A FILE                         | 00000086 |
| C | FOR LATER USE IN PLOTTING.   | 00000087 |
|   | COMMON/TS/T,H,XYZ,RSL,PZ   | 00000090 |
|   | *7CONCOM/RS,RSD,RSDD,SIG,SIGD,SIGDD,EL,ELD,ELDD,REGAM,HDBETA           | 00000100 |
|   | *7OUTCOM/X1,X3/TIME2/TIME2   | 00000110 |
|   | *7TIME8/TIME8/ISITE/ISITE  | 00000120 |
|   | *7BS/X(3),XD(3),XDD(3)   | 00000130 |
|   | *7MS/GAM,BETA,HX,VO,THE,GLAM,SC1,SC2,AH,THES,GLAMS                     | 00000140 |
|   | *7GE/ZK,B1,P1  | 00000150 |
|   | *7OPTION/IOUT1,IOUT2,KZ,IPL0T1,IPL0T2,KAT,SPHERE,OUTINC,IOUT3          | 00000160 |
|   | *7RTD/RTD,RTD6,RTD36,F36,F6080,FERU                                    | 00000170 |
|   | *7SWSW/SWCH1,SWCH2   | 00000180 |
|   | *7SW3SW4/SWCH3,SWCH4   | 00000190 |
|   | *7SW5SW6/SWCH5,SWCH6   | 00000200 |
|   | *7TIME5/TIME5/TIMEL/TIMEL,TIMES  | 00000210 |
|   | *7AX/TN,NTRJ/M2TRAJ/XX(11)   | 00000220 |
|   | COMMON/NR/NREC1,NREC2,NREC3,NREC4,NREC5,NREC                           | 00000230 |
|   | *7NR6/NREC6/SW10/SWCH10  | 00000240 |
|   | *7IO/IO,IO1,IO2  | 00000250 |
|   | *7INOUT/INCOUT,IOUT,NOFF1,NOFF2,NOFF3,IOUTA                            | 00000260 |
|   | COMMON/NR7/NREC7,NOFF4   | 00000270 |
|   | *7OUTT/OUTT(5000)/OUTRJ/OUTRJ(5000),OUTRAD(5000),OUTPLT(5000)          | 00000280 |
|   | *7SITES/NSITE,SLAT(20),SLONG(20),SALT(20)                              | 00000285 |
|   | DOUBLE PRECISION T,H,XYZ,RSL,PZ,X,XD,XDD,ZK,B1,P1,GAM,BETA,HX,VO,      | 00000290 |
|   | *THE,GLAM,SC1,SC2,AH,THES,GLAMS,RS,RSD,RSDD,SIG,SIGD,SIGDD,EL,ELD,     | 00000300 |
|   | *ELDD,REGAM,HDBETA,TN,X1,X3,TIMEL,TIMES                                | 00000310 |
|   | *XX,SLAT,SLONG,SALT  | 00000320 |
|   |  | 00000330 |
|   | LOGICAL IOUT1,IOUT2,KZ,IPL0T1,IPL0T2,KAT,SPHERE                        | 00000340 |
|   | *IOUT3   | 00000350 |
|   | LOGICAL SWITCH,SWCHR,SWCH1,SWCH2,SWCH3,SWCH4,SWCH5,SWCH6               | 00000360 |
|   | *EOF8,EOF9,EOF,SWCH10  | 00000370 |
|   | TIME1 = T  | 00000460 |
|   | ISTOR1 = 1   | 00000470 |
|   | IO = 7   | 00000480 |
|   | IF(IOUT1)IO=13   | 00000490 |
|   | NREC1 = 0  | 00000500 |
|   | ISTOR4 = 1   | 00000505 |
|   | IF(NTRJ.NE.2)GO TO 120   | 00000510 |
|   | OUTINC=-OUTINC   | 00000512 |
|   | SWITCH=.FALSE.   | 00000515 |
|   | SWCHR=.FALSE.  | 00000517 |



|  |          |
|--|----------|
| 120 IF(NTRJ.EQ.3)OUTINC=-OUTINC                              | 00000518 |
| ENTRY STORTJ   | 00000520 |
| C STORE DATA FROM MISSILE/SATELLITE TRAJECTORY FOR PRINT-OUT | 00000530 |
|  | 00000540 |
| IOUT = 0   | 00000550 |
| TIMES = T  | 00000560 |
| OUTTRJ(ISTOR1) = X(1)  | 00000570 |
| OUTTRJ(ISTOR1+1) = X(2)*RTD                                  | 00000577 |
| OUTTRJ(ISTOR1+2) = X(3)*RTD                                  | 00000580 |
| OUTTRJ(ISTOR1+3) = H   | 00000590 |
| OUTTRJ(ISTOR1+4) = XYZ*0. 16666667                           | 00000600 |
| OUTTRJ(ISTOR1+5) = ZK  | 00000610 |
| OUTTRJ(ISTOR1+6) = PZ  | 00000620 |
| ISTOR1 = ISTOR1 + 7  | 00000630 |
| NREC1 = NREC1 + 1  | 00000640 |
| IF(.NOT.IOUT)RETURN  | 00000650 |
| OUTTRJ(ISTOR1) = XD(1)*0. 16666667                           | 00000660 |
| OUTTRJ(ISTOR1+1) = XD(2)*RTD6                                | 00000670 |
| OUTTRJ(ISTOR1+2) = XD(3)*RTD6                                | 00000680 |
| OUTTRJ(ISTOR1+3) = XDD(1)*P36                                | 00000690 |
| OUTTRJ(ISTOR1+4) = XDD(2)*RTD36                              | 00000700 |
| OUTTRJ(ISTOR1+5) = XDD(3)*RTD36                              | 00000710 |
| ISTOR1 = ISTOR1 + 6  | 00000720 |
| RETURN   | 00000730 |
|  | 00000740 |
| ENTRY STORTR   | 00000750 |
|  | 00000760 |
| C STORE TRAJECTORY DATA FOR RADAR COMPUTATIONS               | 00000770 |
|  | 00000780 |
| NREC7 = NREC7+1  | 00000790 |
| OUTTJ(ISTOR4)=X(1)   | 00000800 |
| OUTTJ(ISTOR4+1)=X(2)   | 00000810 |
| OUTTJ(ISTOR4+2)=X(3)   | 00000820 |
| OUTTJ(ISTOR4+3)=XD(1)  | 00000830 |
| OUTTJ(ISTOR4+4)=XD(2)  | 00000840 |
| OUTTJ(ISTOR4+5)=XD(3)  | 00000850 |
| OUTTJ(ISTOR4+6)=XDD(1)                                       | 00000860 |
| OUTTJ(ISTOR4+7)=XDD(2)                                       | 00000870 |
| OUTTJ(ISTOR4+8)=XDD(3)                                       | 00000880 |
| ISTOR4= ISTOR4+9   | 00000890 |
| RETURN   | 00000900 |
|  | 00000910 |
| ENTRY OUTTRI   | 00000920 |
|  | 00000930 |
| IREC=1   | 00000940 |
| WRITE(9)IREC,TIME1   | 00000950 |
| RETURN   | 00000955 |
|  | 00000960 |
| ENTRY OUTTR  | 00000970 |
|  | 00000980 |
|  | 00000990 |
|  | 00001000 |

|    |   |          |
|----|---|----------|
| C  | OUTPUT TRAJECTORY DATA ON A FILE                  | 00001010 |
|    |   | 00001020 |
|    | IREC=IREC+1                                       | 00001025 |
|    | WRITE(9)IREC,NREC7                                | 00001030 |
|    | IF(NREC7.EQ.0)RETURN                              | 00001040 |
|    | NDATA = NREC7*9                                   | 00001050 |
|    | IREC=IREC+1                                       | 00001055 |
|    | WRITE(9)IREC,(OUTTJ(I),I=1,NDATA)                 | 00001060 |
|    | NREC7 = 0   | 00001070 |
|    | ISTOR4=1  | 00001080 |
|    | RETURN  | 00001090 |
|    |   | 00001100 |
|    | ENTRY STRAD2                                      | 00001110 |
|    |   | 00001120 |
| C  | COMPUTE SECOND RADAR TIME POINT TO BE PRINTED OUT | 00001130 |
|    |   | 00001140 |
|    | TIME4 = T/OUTINC                                  | 00001150 |
|    | ITIME = TIME4                                     | 00001160 |
|    | IF(TIME4-FLOAT(ITIME).LT.1.0E-5)GO TO 80          | 00001170 |
|    | RETURN  | 00001180 |
| 80 | SWTCH4 = .FALSE.                                  | 00001190 |
|    | IOUTA = INCOUT                                    | 00001200 |
|    | TIME4 = T   | 00001210 |
|    | NREC6 = 2   | 00001220 |
|    | RETURN  | 00001230 |
|    | ENTRY STORAD                                      | 00001240 |
|    | TIME2 = T   | 00001250 |
|    | ISTOR2 = 1  | 00001260 |
|    | IO1 = 8   | 00001270 |
|    | IF(IOUT2)IO1=13                                   | 00001280 |
|    | NREC2 = 0   | 00001290 |
|    | NREC6 = 1   | 00001300 |
|    | ENTRY STORD1                                      | 00001310 |
|    |   | 00001320 |
| C  | STORE RADAR DATA FROM MISSILE/SATELLITE           | 00001330 |
| 90 | IOUTA = 0   | 00001340 |
|    | TIME3 = T   | 00001350 |
|    | OUTRAD(ISTOR2) = RS*F6080                         | 00001360 |
|    | OUTRAD(ISTOR2+1) = RSD*0.16666667                 | 00001370 |
|    | OUTRAD(ISTOR2+2) = EL*RTD                         | 00001380 |
|    | OUTRAD(ISTOR2+3) = ELD*RTD60                      | 00001390 |
|    | OUTRAD(ISTOR2+4) = SIG*RTD                        | 00001400 |
|    | OUTRAD(ISTOR2+5) = SIGD*RTD60                     | 00001410 |
|    | OUTRAD(ISTOR2+6) = X1*FERU                        | 00001420 |
|    | OUTRAD(ISTOR2+7) = X3*RTD - GLAMS                 | 00001430 |
|    | ISTOR2 = ISTOR2 + 8                               | 00001440 |
|    | NREC2 = NREC2 + 1                                 | 00001450 |
|    | IF(.NOT.IOUT2)RETURN                              | 00001460 |
|    | OUTRAD(ISTOR2) = RSDD*F36                         | 00001470 |
|    | OUTRAD(ISTOR2+1) = ELDD*RTD36                     | 00001480 |
|    | OUTRAD(ISTOR2+2) = SIGD*RTD36                     | 00001490 |
|    | OUTRAD(ISTOR2+3) = REGAM*RTD                      | 00001500 |

|   |          |
|---|----------|
| OUTRAD(ISTOR2+4) = HDBETA*RTD   | 00001510 |
| ISTOR2 = ISTOR2 + 5   | 00001520 |
| RETURN  | 00001530 |
| ENTRY STRADL  | 00001540 |
| C DETERMINE LAST RADAR TIME POINT FOR STORAGE AND PRINT-OUT           | 00001550 |
| IF(TIMES.LT.TIME5+0.01)RETURN   | 00001560 |
| TIME6 = TIMES   | 00001570 |
| NREC6 = 3   | 00001580 |
| GO TO 90  | 00001590 |
| ENTRY PRINTT  | 00001600 |
| C OUTPUT TRAJECTORY DATA  | 00001610 |
| IF(NREC1.EQ.0)GO TO 5   | 00001620 |
| IO11 = IO - 1   | 00001630 |
| MOD52 = MOD(NREC1,52)*IO  | 00001640 |
| NPAGE = NREC1/52 + 1  | 00001650 |
| IF(MOD52.EQ.0)NPAGE=NPAGE-1   | 00001660 |
| K52 = 52*IO   | 00001670 |
| IF(NTRJ.NE.2)GO TO 85   | 00001680 |
| IF(SWITCH)GO TO 85  | 00001690 |
| SWITCH=.TRUE.   | 00001700 |
| IF(TIME2-TIME1.EQ.OUTINC)GO TO 85                                     | 00001710 |
| SWTCHR=.TRUE.   | 00001720 |
| 85 DO 40 NP=1,NPAGE   | 00001721 |
| IEND = NP*K52   | 00001722 |
| ISTART = (NP-1)*K52 + 1   | 00001723 |
| IF(SWTCHR)GO TO 18  | 00001724 |
| IF(NP.NE.NPAGE)GO TO 30   | 00001725 |
| IF(MOD52.EQ.0)GO TO 30  | 00001730 |
| IF(NPAGE.EQ.1)GO TO 50  | 00001740 |
| IEND = ISTART - 1 + MOD52   | 00001750 |
| 30 IF(IOUT1)GO TO 35  | 00001760 |
| WRITE(6,10)NTRJ,{TIME1+(I/IO)*OUTINC,(OUTTRJ(J),J=I,I+IO11),I=ISTA    | 00001770 |
| *RT,IEND,IO)  | 00001780 |
| 10 FORMAT(1H1,1X,4HTRAJECTORY PARAMETERS , TRAJECTORY NUMBER,I4//5X   | 00001790 |
| *, 9HTIME(MIN),2X,10HRAADIUS(FT),2X,13HLATITUDE( DEG),2X,14HLONGITUDE | 00001800 |
| *[DEG),2X,10HHEIGHT(FT),2X,14HVELOCITY(FT/S),2X,21HBAL.COEFF.(FT**2   | 00001810 |
| */SLG),2X,22HATMOS.DENS.(SLG/FT**3)/(6X,F7,2,1X,E12,5,3X,F7,2,8X,F8   | 00001820 |
| *.2,5X,E12,5,3X,E13,6,4X,E12,5,12X,E12,5))                            | 00001830 |
| GO TO 40  | 00001840 |
| 50 IEND = MOD52   | 00001850 |
| GO TO 30  | 00001860 |
| 35 WRITE(6,15)NTRJ,{TIME1+(I/IO)*OUTINC,(OUTTRJ(J),J=I,I+IO11),I=ISTA | 00001870 |
| *RT,IEND,IO)  | 00001880 |
| 15 FORMAT(1H1,1X,4HTRAJECTORY PARAMETERS , TRAJECTORY NUMBER,I4//3X   | 00001890 |
| *,4HTIME,4X,6HRAADIUS,1X,8HLATITUDE,1X,9HLONGITUDE,4X,6HHEIGHT,3X,8H  | 00001900 |
| *VELOCITY,2X,6HBALCOF,2X,5HATDEN,5X,5HR-DOT,1X,7HLAT-DOT,1X,8HLONG-   | 00001910 |
| *DOT,2X,8HR-DOTDOT,1X,10HLAT-DOTDOT,1X,11HLONG-DOTDOT/2X,5H(MIN),5X   | 00001920 |
|   | 00001930 |
|   | 00001940 |
|   | 00001950 |
|   | 00001960 |

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* 4H(FT), 4X, 5H(DEG), 4X, 5H(DEG), 7X, 4H(FT), 5X, 6H(FT/S), 2X, 7H(F2/5G), 100001970
* X, 7H(SG/F3), 2X, 6H(FT/S), 1X, 7H(DEG/S), 2X, 7H(DEG/S), 1X, 9H(FT/S-2), 100001980
* X, 10H(DEG/S**2), 2X, 1H(DEG/S**2)/(1X, F6.2, 1X, E9.3, 2X, F7.2, 2X, F8.2, 00001990
* 1X, E9.3, 1X, E10.3, 1X, F5.2, E9.2, E10.3, 1X, F7.4, 1X, F8.5, 2X, F8.4, 1X, 00002000
* E10.3, 2X, E10.3) 00002010
GO TO 40 00002020
C 00002030
C PRINT OUT 1ST, 2ND, & FOLLOWING TIME POINTS FOR 2ND TRAJECTORY 00002040
C 00002050
180 SWITCHR=.FALSE. 00002060
IF(NPAGE.NE.1)GO TO 240 00002070
IF(MOD52.EQ.0)GO TO 240 00002080
IEND=MOD52 00002090
240 IF(IOUT1)GO TO 245 00002100
WRITE(6,10)NTRJ,TIME1,(OUTTRJ(J),J=1,IO) 00002110
ISTRT=ISTRT+IO 00002120
WRITE(6,60)(TIME2+((I-IO)/IO)*OUTINC,(OUTTRJ(J),J=1, 00002130
*I+IO-1),I=ISTRT,IEND,IO) 00002140
255 TIME1=TIME2-OUTINC 00002150
GO TO 40 00002160
245 WRITE(6,15)NTRJ,TIME1,(OUTTRJ(J),J=1,IO) 00002170
ISTRT=ISTRT+IO 00002180
WRITE(6,75)(TIME2+((I-IO)/IO)*OUTINC,(OUTTRJ(J),J=1, 00002190
*I+IO-1),I=ISTRT,IEND,IO) 00002200
GO TO 255 00002210
40 CONTINUE 00003000
TIME1 = TIME1 + (IEND/IO)*OUTINC 00003010
5 IF(SWITCH3)GO TO 2 00003020
ISTOR1 = 1 00003030
NREC1 = 0 00003040
65 TIME1=T 00003050
RETURN 00003060
C 00003070
C PRINT OUT LAST TIME POINT 00003080
C 00003090
20 IF(NTRJ.NE.2)GO TO 21 00003100
IF(T.GT.TIMES-0.01D0)GO TO 65 00003110
GO TO 22 00003120
21 IF(T.LT.TIMES+0.01D0)GO TO 65 00003130
22 OUTTRJ(1) = X(1) 00003140
OUTTRJ(2) = X(2)*RTD 00003150
OUTTRJ(3) = X(3)*RTD 00003160
OUTTRJ(4) = H 00003170
OUTTRJ(5) = XYZ*J, 16666667 00003180
OUTTRJ(6) = ZK 00003190
OUTTRJ(7) = PZ 00003200
IF(.NOT.IOUT1)GO TO 25 00003210
OUTTRJ(8) = Xd(1)*J, 16666667 00003220
OUTTRJ(9) = Xd(2)*RTD60 00003230
OUTTRJ(10) = Xd(3)*RTD60 00003240
OUTTRJ(11) = Xdd(1)*F36 00003250
OUTTRJ(12) = Xdd(2)*RTD36 00003260

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|     |   |         |
|-----|---|---------|
|     | OUTTRJ(13) = XDD(3)*RTD36   | 0000327 |
|     | GO TO 45  | 0000328 |
| 25  | IF(MOD52.EQ.)GO TO 55   | 0000329 |
|     | WRITE(6,6)T.(OUTTRJ(J),J=1,IO)                                      | 0000330 |
| 60  | FORMAT(6X,F7.2,1X,E12.5,3X,F7.2,8X,F8.2,5X,E12.5,3X,E13.6,4X,E12.5, | 0000331 |
|     | * ,12X,E12.5)   | 0000332 |
|     | GO TO 65  | 0000333 |
| 55  | WRITE(6,10)NTRJ,T.(OUTTRJ(J),J=1,IO)                                | 0000334 |
|     | GO TO 65  | 0000335 |
| 45  | IF(MOD52.EQ.)GO TO 70   | 0000336 |
|     | WRITE(6,75)T.(OUTTRJ(J),J=1,IO)                                     | 0000337 |
| 75  | FORMAT(1X,F6.2,1X,E9.3,2X,F7.2,2X,F8.2,1X,E9.3,1X,E10.3,1X,F5.2,    | 0000338 |
|     | * ,E9.2,E10.3,1X,F7.4,1X,F8.5,2X,F8.4,1X,E10.3,2X,E10.3)            | 0000339 |
|     | GO TO 65  | 0000340 |
| 70  | WRITE(6,15)NTRJ,T.(OUTTRJ(J),J=1,IO)                                | 0000341 |
|     | GO TO 65  | 0000342 |
|     |   | 0000343 |
|     | ENTRY OUTDR   | 0000344 |
| C   | OUTPUT RADAR DATA ON FILE   | 0000345 |
|     | EOF8 = .FALSE.  | 0000346 |
|     | WRITE(08)NREC2,NREC6,EOF8   | 0000347 |
|     | IF(NREC2.EQ.)RETURN   | 0000348 |
|     | IF(NREC6.EQ.1.OR.NREC6.EQ.2)WRITE(08)TIME2,TIME4                    | 0000349 |
|     | IF(NREC6.EQ.)GO TO 95   | 0000350 |
|     | IF(NREC6.EQ.3)WRITE( 8)TIME2,TIME4,TIME6                            | 0000351 |
| 95  | NREC = NREC2*IO1  | 0000352 |
|     | WRITE(08)(OUTRAD(I),I=1,NREC)                                       | 0000353 |
|     | ISTOR2 = 1  | 0000354 |
|     | NREC2 = 0   | 0000355 |
|     | NREC6 = 0   | 0000356 |
|     | RETURN  | 0000357 |
|     | ENTRY OUTEOF  | 0000358 |
|     | EOF8 = .TRUE.   | 0000359 |
|     | WRITE(08)NREC2,NREC6,EOF8   | 0000360 |
|     | RETURN  | 0000361 |
|     | ENTRY PRINTR  | 0000362 |
| C   | OUTPUT RADAR DATA ON PRINTER  | 0000363 |
|     | REWIND 8  | 0000364 |
|     | IO11 = IO1 - 1  | 0000365 |
| 140 | SWITCH = .TRUE.   | 0000366 |
|     | SWTCHR = .FALSE.  | 0000367 |
|     | 8 READ(08)NREC2,NREC6,EOF8  | 0000368 |
|     | IF(EOF8)GO TO 14  | 0000369 |
|     | IF(NREC2.EQ.)GO TO 300  | 0000370 |
|     | NREC = NREC2*IO1  | 0000371 |
|     | IF(NREC6.EQ.1.OR.NREC6.EQ.2)READ(08)TIME2,TIME4                     | 0000372 |
|     | IF(NREC6.EQ.)GO TO 130  | 0000373 |
|     | IF(NREC6.EQ.3.AND.SWITCH)READ(08)TIME2,TIME4,TIME6                  | 0000374 |
|     | IF(NREC6.EQ.3.AND.(.NOT.SWITCH))READ(08)DUM,DUM,TIME6               | 0000375 |
| 130 | READ(08)(OUTRAD(I),I=1,NREC)  | 0000376 |
|     | MOD52 = MOD(NREC2,52)*IO1   | 0000377 |
|     | NPAGE = NREC2/52 + 1  | 0000378 |

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IF(MOD52,EQ,0)NPAGE=NPAGE-1
K52 = S2*IO1
DO 110 NP=1,NPAGE
IEND = NP*K52
ISTART = (NP-1)*K52 + 1
IF(NP,EQ,1)GO TO 150
160 IF(NP,EQ,NPAGE)GO TO 155
IF(NP,NE,NPAGE)GO TO 105
200 IF(MOD52,EQ,0)GO TO 105
IF(NPAGE,EQ,1)GO TO 115
IEND = ISTART - 1 + MOD52
105 IF(OUT2)GO TO 10
WRITE(6,125)NTRJ,ISITE,SC1,SC2,(TIME2+(I/IO1)*OUTINC,
*OUTRAD(J),J=I,I+IO1),I=ISTART,IEND,IO1)
125 FORMAT(1H1,10X,36HRADAR PARAMETERS , TRAJECTORY NUMBER,I4,3X,10HR,
*BAR SITE,I4,F12.3," DEG.LAT.",F12.3," DEG.LONG." //5X,"TIME",7X,8H
*SL RANGE,4X,13HSL RANGE-RATE,3X,9HELEVATION,7X,7HEL RATE,4X,7HAZIMUT00003950
*UTH,6X,7HAZ RATE,4X,6HRADIUS,4X,12HINERTIAL PHI/4X,5H(MIN),10X,4H(00003960
*NM),8X,5H(FT/S),9X,5H(DEG),9X,7H(DEG/S),5X,5H(DEG),7X,7H(DEG/S),4X(00003970
*,5H(ERU),9X,5H(DEG)/(2X,F7.2,2X,E13.6,4X,E13.6,5X,F7.2,3X,E11.4,4X(00003980
*,F7.2,2X,E11.4,3X,F7.3,9X,F7.2))
GO TO 110
115 IEND = MOD52
GO TO 105
100 WRITE(6,135)NTRJ,ISITE,SC1,SC2,(TIME2+(I/IO1)*OUTINC,
*OUTRAD(J),J=I,I+IO1),I=ISTART,IEND,IO1)
135 FORMAT(1H1,10X,36HRADAR PARAMETERS , TRAJECTORY NUMBER,I4,3X,10HR,
*BAR SITE,I4,F12.3," DEG.LAT.",F12.3," DEG.LONG." //3X,"TIME",2X,8H00004060
*SL RANGE,1X,13HSL RANGE-RATE,1X,9HELEVATION,4X,7HEL-RATE,1X,7HAZIMUT00004070
*H,5X,7HAZ-RATE,2X,6HRADIUS,1X,7HINR-PHI,1X,7HSL-RTRT,4X,7HEL-RTRT,00004080
*4X,7HAZ-RTRT,1X,7HREENTRY,1X,7HHEADING/2X,5H(MIN),5X,4H(NM),5X,6H(00004090
*FT/S),5X,5H(DEG),6X,7H(DEG/S),2X,5H(DEG),6X,7H(DEG/S),3X,5H(ERU),200004100
*X,5H(DEG),1X,8H(FT/S/S),2X,9H(DEG/S/S),2X,9H(DEG/S/S),2X,5H(DEG),300004110
*X,5H(DEG)/(1X,F6.2,1X,E9.3,1X,E11.4,3X,F7.2,1X,E10.3,1X,F7.2,1X,E100004120
*1.4,1X,F7.3,1X,F7.2,1X,F7.3,1X,E10.3,1X,E10.3,1X,F7.2,1X,F7.2))
GO TO 110
C PRINT OUT FIRST,SECOND AND FOLLOWING TIME POINTS
150 IF(SWITCH)GO TO 145
GO TO 160
145 IF(NPAGE,EQ,1)GO TO 165
165 IF(OUT2)GO TO 17
WRITE(6,125)NTRJ,ISITE,SC1,SC2,TIME2,(OUTRAD(J),J=1,IO1)
ISTRT = ISTART + IO1
WRITE(6,175)(TIME4+((I-IO1)/IO1)*OUTINC,(OUTRAD(J),J=I,I+IO1),I=
*ISTRT,IEND,IO1)
175 FORMAT(2X,F7.2,2X,E13.6,4X,E13.6,5X,F7.2,3X,E11.4,4X,F7.2,2X,E11.4
*,3X,F7.3,6X,F7.2)
IF(SWICH)WRITE(6,175)TIME6,(OUTRAD(J),J=IEND+1,IEND+IO1)
190 TIME2 = TIME4 + OUTINC
GO TO 110

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170 WRITE(6,135)NTRJ,ISITE,SC,SC2,TIME2,(OUTRAD(J),J=1,IO1) 00004310
    ISTRT = ISTART + IO1 00004320
    WRITE(6,185)(TIME2+((I-IO1)/IO1)*OUTINC,(OUTRAD(J),J=I,I+IO11),I= 00004330
    *ISTRT,IEND,IO1) 00004340
185 FORMAT(1X,F6.2,1X,E9.3,1X,E11.4,3X,F7.2,1X,E10.3,1X,F7.2,1X,E11.4, 00004350
    *1X,F7.3,1X,F7.2,1X,F7.3,1X,E10.3,1X,E10.3,1X,F7.2,1X,F7.2) 00004360
    IF(SWCHR)WRITE(6,185)TIME6,(OUTRAD(J),J=IEND+1,IEND+IO1) 00004370
    GO TO 190 00004380
165 IF(NREC6.NE.3)GO TO 196 00004390
    SWCHR = .TRUE. 00004400
    IEND = IEND - IO1 00004410
    IF(MOD52.NE.0)IEND=MOD52-IO1 00004420
    GO TO 195 00004430
196 IF(MOD52.NE.0)IEND=MOD52 00004432
    GO TO 195 00004434
C PRINT OUT LAST TIME POINT 00004440
155 IF(NREC6.NE.3)GO TO 200 00004450
    IF(MOD52.EQ.0)GO TO 205 00004460
    IF(NPAGE.EQ.1)GO TO 210 00004470
    IEND = ISTART - 1 + MOD52 - IO1 00004480
230 IF(OUT2)GO TO 22 00004490
    IF(IEND.LE.ISTART)GO TO 215 00004500
    WRITE(6,125)NTRJ,ISITE,SC,SC2,(TIME2+(I/IO1)*OUTINC, 00004510
    *(OUTRAD(J),J=I,I+IO11),I=ISTART,IEND,IO1) 00004520
    WRITE(6,175)TIME6,(OUTRAD(J),J=IEND+1,IEND+IO1) 00004530
    GO TO 110 00004540
215 WRITE(6,125)NTRJ,ISITE,SC,SC2,TIME6,(OUTRAD(J),J= 00004550
    *ISTART,ISTART+IO11) 00004560
    GO TO 110 00004570
220 IF(IEND.LE.ISTART)GO TO 225 00004580
    WRITE(6,135)NTRJ,ISITE,SC,SC2,(TIME2+(I/IO1)*OUTINC, 00004590
    *(OUTRAD(J),J=I,I+IO11),I=ISTART,IEND,IO1) 00004600
    WRITE(6,185)TIME6,(OUTRAD(J),J=IEND+1,IEND+IO1) 00004610
    GO TO 110 00004620
225 WRITE(6,135)NTRJ,ISITE,SC,SC2,TIME6,(OUTRAD(J),J= 00004630
    *ISTART,ISTART+IO11) 00004640
    GO TO 110 00004650
205 IEND = IEND - IO1 00004660
    GO TO 230 00004670
210 IEND = MOD52 - IO1 00004680
    GO TO 230 00004690
110 CONTINUE 00004700
    SWITCH = .FALSE. 00004710
    SWCHR = .FALSE. 00004720
    TIME2 = TIME2 + (IEND/IO1)*OUTINC 00004730
    GO TO 8 00004740
300 REWIND 8 00004750
    RETURN 00004760
    ENTRY NOTVIS 00004770
    WRITE(6,250)NTRJ,ISITE,SC,SC2 00004780
250 FORMAT(1H1///10X,"OBJECT NOT VISIBLE TO RADAR"//10X, 00004790

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|   |   |          |
|---|---|----------|
|   | *"TRAJECTORY NUMBER",I4,SX,"RADAR SITE",I4,F12.3,   | 00004810 |
|   | *" DEG.LAT.",F12.3," DEG.LONG.")                    | 00004820 |
|   | RETURN  | 00004830 |
|   | ENTRY PLTAPE  | 00004840 |
| C |   | 00004850 |
| C | GENERATE DATA TAPE/FILE FOR INPUT TO PLOT PROGRAMS  | 00004860 |
| C |   | 00004870 |
| C | INITIALIZATION FOR PLOT TAPE/FILE                   | 00004880 |
| C |   | 00004890 |
|   | TIME3=T   | 00004900 |
|   | ISTOR3=1  | 00004910 |
|   | IO2=8   | 00004920 |
|   | IF(IPL0T2)IO2=13                                    | 00004930 |
|   | NREC3=0   | 00004940 |
|   | NREC4=0   | 00004950 |
|   | NREC5=0   | 00004960 |
|   | EOF=.FALSE.   | 00004970 |
|   | WRITE(10)TIME3,IPL0T2,IO2,EOF                       | 00004980 |
|   | RETURN  | 00004990 |
| C |   | 00005000 |
|   | ENTRY STORP   | 00005010 |
| C |   | 00005020 |
| C | TEMPORARILY STORE RADAR DATA FROM MISSILE/SATELLITE | 00005030 |
| C |   | 00005040 |
|   | TIME7=T   | 00005050 |
|   | OUTPLT(ISTOR3)=RS*F6.80                             | 00005060 |
|   | OUTPLT(ISTOR3+1)=RSD*0.016666667                    | 00005070 |
|   | OUTPLT(ISTOR3+2)=EL*RTD                             | 00005080 |
|   | OUTPLT(ISTOR3+3)=ELD*RTD6                           | 00005090 |
|   | OUTPLT(ISTOR3+4)=SIG*RTD                            | 00005100 |
|   | OUTPLT(ISTOR3+5)=SIGD*RTD60                         | 00005110 |
|   | OUTPLT(ISTOR3+6)=X(1)*FERU                          | 00005120 |
|   | OUTPLT(ISTOR3+7)=X(3)*RTD-GLAMS                     | 00005130 |
|   | ISTOR3=ISTOR3+8                                     | 00005140 |
|   | NREC3=NREC3+1                                       | 00005150 |
|   | NREC4=NREC4+1                                       | 00005160 |
|   | IF(.NOT.IPL0T2)RETURN                               | 00005170 |
|   | OUTPLT(ISTOR3)=RSD2*F36                             | 00005180 |
|   | OUTPLT(ISTOR3+1)=ELDD*RTD36                         | 00005190 |
|   | OUTPLT(ISTOR3+2)=SIGDD*RTD36                        | 00005200 |
|   | OUTPLT(ISTOR3+3)=REGAM*RTD                          | 00005210 |
|   | OUTPLT(ISTOR3+4)=HDBETA*RTD                         | 00005220 |
|   | ISTOR3=ISTOR3+5                                     | 00005230 |
|   | RETURN  | 00005240 |
| C |   | 00005250 |
|   | ENTRY PLTAP1  | 00005260 |
| C |   | 00005270 |
| C | OUTPUT DATA ON PLOT TAPE/FILE                       | 00005280 |
| C |   | 00005290 |
|   | EOF10=.FALSE.                                       | 00005300 |
|   | WRITE(10)NREC3,NREC4,NREC5,EOF10,SWTCH2             | 00005310 |
|   | IF(NREC3.EQ.0)RETURN                                | 00005320 |

|     |  |          |
|-----|--|----------|
|     | IF(NREC3.EQ.(-1))GO TO 235                             | 00005330 |
|     | NDATA = NREC3+IO2                                      | 00005340 |
|     | WRITE(10)(OUTPLT(I),I=1,NDATA)                         | 00005350 |
| 235 | NREC3=0  | 00005360 |
|     | ISTOR3=1   | 00005370 |
|     | NREC5=NREC5+1  | 00005380 |
|     | RETURN   | 00005390 |
| C   |  | 00005400 |
|     | ENTRY PLTEND   | 00005410 |
| C   | OUTPUT LAST TIME OF MISSILE SIGHTING BY RADAR SITE     | 00005420 |
|     | WRITE(10)TIME7   | 00005430 |
|     | RETURN   | 00005440 |
| C   |  | 00005450 |
|     | ENTRY PLTAP2   | 00005460 |
| C   |  | 00005470 |
| C   | OUTPUT LAST RECORD ON PLOT TAPE/FILE FOR ONE SIGHTING  | 00005480 |
| C   |  | 00005490 |
|     | EOF10=.TRUE.   | 00005500 |
|     | WRITE(10)NREC3,NREC4,NREC5,EOF10,SWTCH2                | 00005510 |
|     | RETURN   | 00005520 |
| C   |  | 00005530 |
|     | ENTRY PLTAP3   | 00005540 |
| C   |  | 00005550 |
| C   | OUTPUT FINAL RECORD ON PLOT FILE                       | 00005560 |
| C   |  | 00005570 |
|     | EOF=.TRUE.   | 00005580 |
|     | WRITE(10)TIME7,IPL0T2,IO2,EOF                          | 00005590 |
|     | RETURN   | 00005600 |
| C   |  | 00005610 |
|     | ENTRY STORT2   | 00005620 |
| C   |  | 00005630 |
| C   | STORE DATA FOR 2ND TRAJECTORY                          | 00005640 |
| C   |  | 00005650 |
|     | XX(1)=X(1)   | 00005660 |
|     | XX(2)=X(2)   | 00005670 |
|     | XX(3)=X(3)   | 00005680 |
|     | XX(4)=XD(1)  | 00005690 |
|     | XX(5)=XD(2)  | 00005700 |
|     | XX(6)=XD(3)  | 00005710 |
|     | XX(7)=XDD(1)   | 00005720 |
|     | XX(8)=XDD(2)   | 00005730 |
|     | XX(9)=XDD(3)   | 00005740 |
|     | XX(10)=ZK  | 00005742 |
|     | XX(11)=PZ  | 00005744 |
|     | RETURN   | 00005750 |
| C   |  | 00005760 |
|     | ENTRY OUTNOM   | 00005770 |
| C   |  | 00005780 |
| C   | PLACE NOMINAL TRAJECTORY RADAR DATA ON A SEPARATE FILE | 00005790 |
| C   |  | 00005800 |
|     | ISITE =1   | 00005810 |
|     | IF(.NOT.KZ)GO TO 4 0                                   | 00005820 |

|                                      |          |
|--------------------------------------|----------|
| REWIND 10                            | 00005830 |
| REWIND 11                            | 00005840 |
| 440 READ(10)TIME3,XPLOT3,IO2,EOF     | 00005850 |
| WRITE(11)TIME3,XPLOT2,IO2,EOF        | 00005860 |
| IF(EOF)GO TO 41                      | 00005870 |
| 430 READ(10)NREC3,XT8,IS,EOF1,SWTCH2 | 00005880 |
| WRITE(11)NREC3,XT8,IS,EOF10,SWTCH2   | 00005890 |
| IF(EOF10)GO TO 42                    | 00005900 |
| NDATA =NREC3*IO2                     | 00005910 |
| READ(10)(OUTPLT(I),I=1,NDATA)        | 00005920 |
| WRITE(11)(OUTPLT(I),I=1,NDATA)       | 00005930 |
| GO TO 430                            | 00005940 |
| 420 READ(10)TIME7                    | 00005950 |
| WRITE(11)TIME7                       | 00005960 |
| GO TO 440                            | 00005970 |
| 410 IF(ISITE.EQ.NSITE)RETURN         | 00005980 |
| ISITE=ISITE+1                        | 00005990 |
| GO TO 440                            | 00006000 |
| 400 CONTINUE                         | 00006010 |
| RETURN                               | 00006015 |
| END                                  | 00006020 |

|      |  |          |
|------|--|----------|
| CRKG | 4TH ORDER RUNGE-KUTTA-GILL                                     | 00002170 |
|      | SUBROUTINE RKG   | 00002180 |
| C    | INPUT/OUTPUT MOD 1   | 00002190 |
| C    | THIS ROUTINE IS A 4TH ORDER RUNGE-KUTTA-GILL WHICH NUMERICALLY | 00002200 |
| C    | INTEGRATES THE 2ND ORDER NON-LINEAR DIFFERENTIAL EQUATIONS OF  | 00002210 |
| C    | MOTION.  | 00002220 |
|      | DOUBLE PRECISION C,F,D,A,B,DEG,DXN,DXDX,DL,SAD,ABLE,BAKER      | 00002230 |
|      | DOUBLE PRECISION X,XD,XDD                                      | 00002240 |
|      | DOUBLE PRECISION P,Q   | 00002250 |
|      | DOUBLE PRECISION P1,ZK,B1,TWOPI                                | 00002260 |
|      | DIMENSION C(4), P(4), D(4), A(3), B(3)                         | 00002270 |
|      | DOUBLE PRECISION TO  | 00002280 |
|      | COMMON /BS/ X(3),XD(3),XDD(3)                                  | 00002290 |
|      | COMMON/GE/ZK,B1,P1   | 00002300 |
|      | COMMON /ST/ P(3), Q(3)   | 00002310 |
|      | *7TO/TO  | 00002320 |
|      | DATA C/0.5D0,.2928932188,.1707106781,.1666666667/              | 00002330 |
|      | DATA D/0.5D0,.2928932188,.1707106781,0.5D0/                    | 00002340 |
|      | DATA P/2.0D0,1.0D0,1.0D0,2.0D0/                                | 00002350 |
|      | *TWOPI/6.2831852 717958648/                                    | 00002360 |
|      | DO 10 J=1,4  | 00002370 |
|      | CALL EQTNX   | 00002380 |
|      | DO 10 I=1,3  | 00002390 |
|      | A(I)=XD(I)   | 00002400 |
|      | B(I)=XDD(I)  | 00002410 |
|      | DXN=(A(I)-F(J)*Q(I))*C(J)                                      | 00002420 |
|      | DXDX=(B(I)-P(J)*P(I))*C(J)                                     | 00002430 |
|      | DL=TO*DXN  | 00002440 |
|      | X(I)=X(I)+DL   | 00002450 |
|      | XD(I)=XD(I)+TO*DXDX  | 00002460 |
|      | Q(I)=Q(I)+3.0D0*DXN-D(J)*A(I)                                  | 00002470 |
| 10   | P(I)=P(I)+3.0D0*DXDX-D(J)*B(I)                                 | 00002480 |
|      | IF(X(3)) 13,14,14  | 00002490 |
| 13   | X(3)=X(3)+TWOPI  | 00002500 |
| 14   | SAD=X(3)-TWOPI   | 00002510 |
|      | IF(SAD) 12,11,11   | 00002520 |
| 11   | X(3)=SAD   | 00002530 |
| 12   | RETURN   | 00002540 |
|      | END  | 00002550 |



**Listing of the Sample Input for the Program**

# MISSILE TRAJECTORY PROGRAM(MULTIPLE SITE/TRAJECTORY MOD) INPUTS

## PROGRAM CONTROLS

NUMBER OF TRAJECTORIES SIMULATED(NTRAJ) 10  
 MAXIMUM TIME FOR A TRAJECTORY(TM) 0.20000 02 MIN.  
 MAIN PROCESSING SWITCH(NSWICH) 1  
 PRINT-OUT OPTION 1(IOUT1) F PRINT-OUT OPTION 2(IOUT2) F  
 INCREMENT BETWEEN TIME POINTS FOR PRINT-OUT(OUTINC) 0.100 MIN.  
 PRINTOUT OPTION FOR RADAR PARAMETER DIFFERENCES(IOUT3) F NOMINAL TRAJECTORY SELECTION SWITCH(KZ) T  
 PLOTTING OPTION 1(IPL0T1) T PLOTTING OPTION 2(IPL0T2) F  
 ATMOSPHERIC MODEL OPTION(KAT) F  
 SPHERICAL EARTH MODEL(SPHERE) T  
 INERTIAL VELOCITY OPTION(INERTL) T

\*\*\*\*\*

## INITIAL STATE VECTOR OF THE INTERCEPTOR

RE-ENTRY ANGLE WRT THE VERTICAL(GAM) 0.90000 02 DEG.  
 HEADING ANGLE WRT RELATIVE NORTH(BETA) 0.81826 02 DEG.  
 HEIGHT OF MISSILE AT BURNOUT(HX) 0.60833 06 FT.  
 VELOCITY OF MISSILE RELATIVE TO BURNOUT AT EPOCH(V0) 0.2556742000 05 FT./SEC.  
 GEOCENTRIC LATITUDE AT BURNOUT, +NORTH AND -SOUTH OF EQUATOR(THET) 0.62700 02 DEG.  
 GEOCENTRIC LONGITUDE, EAST OF GREENWICH(GLAM) 0.40350 02 DEG.

## SUBSATELLITE PARAMETERS

GEOCENTRIC LATITUDE, +NORTH AND -SOUTH OF EQUATOR(THES) -0.40000 2 DEG.  
 GEOCENTRIC LONGITUDE, EAST OF GREENWICH(GLINS) 0.60000 02 DEG.

.....

RADAR PARAMETERS

SITE NUMBER 1

GEOCENTRIC LATITUDE OF RADAR, +NORTH AND -SOUTH OF EQUATOR(SLAT) 0.35900D 02 DEG;

GEOCENTRIC LONGITUDE OF RADAR, WEST OF GREENWICH(SLONG) 0.23333D 03 DEG,

ALTITUDE OF RADAR ABOVE SEA LEVEL(SALT) 0, FT,

MAXIMUM CO-LATITUDE OF ELEVATION ANGLE FOR WHICH COVERAGE PARAMETERS ARE DETERMINED(ELIM) 0.89000D 02 DEG.

.....

VELOCITY PERTURBATIONS

OUT OF TRAJECTORY PLANE PERTURBATION, +EJECTED TO THE LEFT OF NOMINAL TRAJECTORY(A) IN FT./SEC.

0. 0.35333D 01 0. 0. 0.50000D 01

IN PLANE PERTURBATION, +EJECTED BACKWARDS FROM NOMINAL TRAJECTORY(B) IN FT./SEC.

0. 0.50000D 01 0.35330D 01 -0.35330D 01 0.

IN PLANE PERTURBATION, +EJECTED UPWARDS FROM NOMINAL TRAJECTORY(C) IN FT./SEC.

0.50000D 01 0. 0.35330D 01 0.35330D 01 0.

**Sample Output for the RADC Trajectory Program**



# TRAJECTORY PARAMETERS, TRAJECTORY NUMBER 1

| TIME(MIN) | RADIUS(FT)  | LATITUDE(DEG) | LONGITUDE(DEG) | HEIGHT(FT) | VELOCITY(FT/ST) | BAL.COEFF.(FT**2/SLG) | ATMOS.DENS.(SLG/FT**3) |
|-----------|-------------|---------------|----------------|------------|-----------------|-----------------------|------------------------|
| 0.00      | 0.21534E 08 | 62.70         | 40.35          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 0.10      | 0.21534E 08 | 62.76         | 41.24          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 0.20      | 0.21534E 08 | 62.82         | 42.07          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 0.30      | 0.21534E 08 | 62.85         | 42.93          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 0.40      | 0.21534E 08 | 62.89         | 43.80          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 0.50      | 0.21534E 08 | 62.92         | 44.67          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 0.60      | 0.21534E 08 | 62.95         | 45.54          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 0.70      | 0.21534E 08 | 62.97         | 46.41          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 0.80      | 0.21534E 08 | 62.99         | 47.28          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 0.90      | 0.21534E 08 | 63.00         | 48.15          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 1.00      | 0.21534E 08 | 63.00         | 49.02          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 1.10      | 0.21534E 08 | 63.00         | 49.90          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 1.20      | 0.21534E 08 | 62.99         | 50.77          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 1.30      | 0.21534E 08 | 62.98         | 51.65          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 1.40      | 0.21534E 08 | 62.96         | 52.52          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 1.50      | 0.21534E 08 | 62.94         | 53.39          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 1.60      | 0.21534E 08 | 62.91         | 54.26          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 1.70      | 0.21534E 08 | 62.87         | 55.13          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 1.80      | 0.21534E 08 | 62.83         | 55.99          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 1.90      | 0.21534E 08 | 62.78         | 56.85          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 2.00      | 0.21534E 08 | 62.73         | 57.71          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 2.10      | 0.21534E 08 | 62.67         | 58.57          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 2.20      | 0.21534E 08 | 62.61         | 59.42          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 2.30      | 0.21534E 08 | 62.54         | 60.27          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 2.40      | 0.21534E 08 | 62.47         | 61.12          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 2.50      | 0.21534E 08 | 62.39         | 61.96          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 2.60      | 0.21534E 08 | 62.3          | 62.79          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 2.70      | 0.21534E 08 | 62.21         | 63.62          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 2.80      | 0.21534E 08 | 62.12         | 64.45          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 2.90      | 0.21534E 08 | 62.02         | 65.27          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 3.00      | 0.21534E 08 | 61.91         | 66.08          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 3.10      | 0.21534E 08 | 61.80         | 66.89          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 3.20      | 0.21534E 08 | 61.69         | 67.69          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 3.30      | 0.21534E 08 | 61.57         | 68.48          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 3.40      | 0.21534E 08 | 61.44         | 69.27          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 3.50      | 0.21534E 08 | 61.31         | 70.06          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 3.60      | 0.21534E 08 | 61.17         | 70.83          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 3.70      | 0.21534E 08 | 61.03         | 71.60          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 3.80      | 0.21534E 08 | 60.89         | 72.36          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 3.90      | 0.21534E 08 | 60.74         | 73.12          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 4.00      | 0.21534E 08 | 60.59         | 73.86          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 4.10      | 0.21534E 08 | 60.43         | 74.60          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 4.20      | 0.21534E 08 | 60.27         | 75.33          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 4.30      | 0.21534E 08 | 60.10         | 76.06          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 4.40      | 0.21534E 08 | 59.93         | 76.78          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 4.50      | 0.21534E 08 | 59.76         | 77.49          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 4.60      | 0.21534E 08 | 59.58         | 78.19          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 4.70      | 0.21534E 08 | 59.40         | 78.88          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 4.80      | 0.21534E 08 | 59.21         | 79.57          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 4.90      | 0.21534E 08 | 59.02         | 80.24          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 5.00      | 0.21534E 08 | 58.82         | 80.91          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |
| 5.10      | 0.21534E 08 | 58.63         | 81.58          | 0.6803E 06 | 0.255674E 09    | 0.                    | 0.                     |

# TRAJECTORY PARAMETERS, TRAJECTORY NUMBER 1

| TIME(MIN) | RADIUS(FT) | LATITUDE(DEG) | LONGITUDE(DEG) | HEIGHT(FT)  | VELOCITY(FT/S) | BAL.COEFF.(FT**2/SLG) | ATMOS.DENS.(SLG/FT**3) |
|-----------|------------|---------------|----------------|-------------|----------------|-----------------------|------------------------|
| 5.20      | 21534E 08  | 58.42         | 82.23          | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 5.30      | 21534E 08  | 58.22         | 82.88          | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 5.40      | 21534E 08  | 58.01         | 83.52          | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 5.50      | 21534E 08  | 57.80         | 84.15          | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 5.60      | 21534E 08  | 57.52         | 84.77          | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 5.70      | 21534E 08  | 57.36         | 85.39          | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 5.80      | 21534E 08  | 57.14         | 86.00          | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 5.90      | 21534E 08  | 56.92         | 86.60          | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 6.00      | 21534E 08  | 56.69         | 87.19          | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 6.10      | 21534E 08  | 56.46         | 87.78          | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 6.20      | 21534E 08  | 56.22         | 88.35          | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 6.30      | 21534E 08  | 55.99         | 88.93          | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 6.40      | 21534E 08  | 55.75         | 89.49          | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 6.50      | 21534E 08  | 55.50         | 90.04          | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 6.60      | 21534E 08  | 55.26         | 90.59          | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 6.70      | 21534E 08  | 55.01         | 91.14          | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 6.80      | 21534E 08  | 54.76         | 91.67          | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 6.90      | 21534E 08  | 54.51         | 92.20          | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 7.00      | 21534E 08  | 54.25         | 92.72          | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 7.10      | 21534E 08  | 53.99         | 93.23          | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 7.20      | 21534E 08  | 53.73         | 93.74          | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 7.30      | 21534E 08  | 53.47         | 94.24          | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 7.40      | 21534E 08  | 53.2          | 94.74          | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 7.50      | 21534E 08  | 52.94         | 95.23          | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 7.60      | 21534E 08  | 52.67         | 95.71          | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 7.70      | 21534E 08  | 52.40         | 96.18          | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 7.80      | 21534E 08  | 52.12         | 96.65          | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 7.90      | 21534E 08  | 51.85         | 97.12          | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 8.00      | 21534E 08  | 51.57         | 97.57          | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 8.10      | 21534E 08  | 51.29         | 98.03          | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 8.20      | 21534E 08  | 51.01         | 98.47          | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 8.30      | 21534E 08  | 50.72         | 98.91          | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 8.40      | 21534E 08  | 50.44         | 99.35          | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 8.50      | 21534E 08  | 50.15         | 99.78          | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 8.60      | 21534E 08  | 49.86         | 100.20         | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 8.70      | 21534E 08  | 49.57         | 100.62         | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 8.80      | 21534E 08  | 49.28         | 101.03         | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 8.90      | 21534E 08  | 48.99         | 101.44         | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 9.00      | 21534E 08  | 48.69         | 101.84         | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 9.10      | 21534E 08  | 48.39         | 102.24         | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 9.20      | 21534E 08  | 48.09         | 102.63         | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 9.30      | 21534E 08  | 47.79         | 103.02         | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 9.40      | 21534E 08  | 47.49         | 103.40         | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 9.50      | 21534E 08  | 47.19         | 103.78         | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 9.60      | 21534E 08  | 46.88         | 104.15         | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 9.70      | 21534E 08  | 46.58         | 104.52         | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 9.80      | 21534E 08  | 46.27         | 104.89         | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 9.90      | 21534E 08  | 45.96         | 105.25         | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 10.00     | 21534E 08  | 45.65         | 105.61         | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 10.10     | 21534E 08  | 45.34         | 105.96         | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 10.20     | 21534E 08  | 45.03         | 106.31         | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |
| 10.30     | 21534E 08  | 44.72         | 106.65         | 0.60803E 06 | 0.255674E 05   | 0.                    | 0.                     |

# TRAJECTORY PARAMETERS, TRAJECTORY NUMBER 1

| TIME(MIN) | RADIUS(FT) | LATITUDE(DEG) | LONGITUDE(DEG) | HEIGHT(FT) | VELOCITY(FT/S) | BAL.COEFF.(PT**2/SLG) | ATMOS.DENS.(SLG/FT**3) |
|-----------|------------|---------------|----------------|------------|----------------|-----------------------|------------------------|
| 10.40     | 21534E 08  | 44.4          | 106.99         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 10.50     | 21534E 08  | 44.09         | 107.33         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 10.60     | 21534E 08  | 43.77         | 107.66         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 10.70     | 21534E 08  | 43.45         | 107.99         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 10.80     | 21534E 08  | 43.13         | 108.31         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 10.90     | 21534E 08  | 42.81         | 108.63         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 11.00     | 21534E 08  | 42.49         | 108.95         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 11.10     | 21534E 08  | 42.17         | 109.26         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 11.20     | 21534E 08  | 41.85         | 109.57         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 11.30     | 21534E 08  | 41.52         | 109.88         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 11.40     | 21534E 08  | 41.20         | 110.19         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 11.50     | 21534E 08  | 40.87         | 110.49         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 11.60     | 21534E 08  | 40.54         | 110.78         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 11.70     | 21534E 08  | 40.22         | 111.08         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 11.80     | 21534E 08  | 39.89         | 111.37         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 11.90     | 21534E 08  | 39.56         | 111.66         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 12.00     | 21534E 08  | 39.23         | 111.94         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 12.10     | 21534E 08  | 38.90         | 112.22         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 12.20     | 21534E 08  | 38.57         | 112.50         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 12.30     | 21534E 08  | 38.23         | 112.78         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 12.40     | 21534E 08  | 37.90         | 113.05         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 12.50     | 21534E 08  | 37.56         | 113.33         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 12.60     | 21534E 08  | 37.23         | 113.59         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 12.70     | 21534E 08  | 36.89         | 113.86         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 12.80     | 21534E 08  | 36.56         | 114.12         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 12.90     | 21534E 08  | 36.22         | 114.38         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 13.00     | 21534E 08  | 35.88         | 114.64         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 13.10     | 21534E 08  | 35.54         | 114.90         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 13.20     | 21534E 08  | 35.21         | 115.15         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 13.30     | 21534E 08  | 34.87         | 115.40         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 13.40     | 21534E 08  | 34.53         | 115.65         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 13.50     | 21534E 08  | 34.18         | 115.90         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 13.60     | 21534E 08  | 33.84         | 116.14         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 13.70     | 21534E 08  | 33.50         | 116.39         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 13.80     | 21534E 08  | 33.16         | 116.63         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 13.90     | 21534E 08  | 32.82         | 116.87         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 14.00     | 21534E 08  | 32.47         | 117.10         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 14.10     | 21534E 08  | 32.13         | 117.34         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 14.20     | 21534E 08  | 31.78         | 117.57         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 14.30     | 21534E 08  | 31.44         | 117.80         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 14.40     | 21534E 08  | 31.09         | 118.03         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 14.50     | 21534E 08  | 30.74         | 118.25         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 14.60     | 21534E 08  | 30.40         | 118.48         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 14.70     | 21534E 08  | 30.05         | 118.70         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 14.80     | 21534E 08  | 29.7          | 118.92         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 14.90     | 21534E 08  | 29.35         | 119.14         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 15.00     | 21534E 08  | 29.01         | 119.36         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 15.10     | 21534E 08  | 28.66         | 119.58         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 15.20     | 21534E 08  | 28.31         | 119.79         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 15.30     | 21534E 08  | 27.96         | 120.01         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 15.40     | 21534E 08  | 27.61         | 120.22         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |
| 15.50     | 21534E 08  | 27.26         | 120.43         | 0.6804E 06 | 0.25574E 03    | 0.                    | 0.                     |



| TRAJECTORY PARAMETERS, TRAJECTORY NUMBER 1 |            |               |                |             |                |                       |                        |
|--|------------|---------------|----------------|-------------|----------------|-----------------------|------------------------|
| TIME(MIN)                                  | RADIUS(FT) | LATITUDE(DEG) | LONGITUDE(DEG) | HEIGHT(FT)  | VELOCITY(FT/S) | RAI.COEFF.(FT**2/SLG) | ATMOS.DENS.(SLG/FT**3) |
| 15.60                                      | 21534E 08  | 26.91         | 120.64         | 0.60804E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 15.70                                      | 21534E 08  | 26.55         | 120.84         | 0.60804E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 15.80                                      | 21534E 08  | 26.22         | 121.05         | 0.60804E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 15.90                                      | 21534E 08  | 25.85         | 121.25         | 0.60804E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 16.00                                      | 21534E 08  | 25.51         | 121.46         | 0.60804E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 16.10                                      | 21534E 08  | 25.14         | 121.66         | 0.60804E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 16.20                                      | 21534E 08  | 24.79         | 121.86         | 0.60804E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 16.30                                      | 21534E 08  | 24.44         | 122.06         | 0.60804E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 16.40                                      | 21534E 08  | 24.08         | 122.26         | 0.60804E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 16.50                                      | 21534E 08  | 23.73         | 122.45         | 0.60804E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 16.60                                      | 21534E 08  | 23.37         | 122.65         | 0.60804E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 16.70                                      | 21534E 08  | 23.02         | 122.84         | 0.60804E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 16.80                                      | 21534E 08  | 22.66         | 123.04         | 0.60805E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 16.90                                      | 21534E 08  | 22.31         | 123.23         | 0.60805E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 17.00                                      | 21534E 08  | 21.95         | 123.42         | 0.60805E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 17.10                                      | 21534E 08  | 21.60         | 123.61         | 0.60805E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 17.20                                      | 21534E 08  | 21.24         | 123.80         | 0.60805E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 17.30                                      | 21534E 08  | 20.88         | 123.98         | 0.60805E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 17.40                                      | 21534E 08  | 20.53         | 124.17         | 0.60805E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 17.50                                      | 21534E 08  | 20.17         | 124.36         | 0.60805E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 17.60                                      | 21534E 08  | 19.81         | 124.54         | 0.60805E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 17.70                                      | 21534E 08  | 19.45         | 124.73         | 0.60805E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 17.80                                      | 21534E 08  | 19.11         | 124.91         | 0.60805E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 17.90                                      | 21534E 08  | 18.74         | 125.09         | 0.60805E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 18.00                                      | 21534E 08  | 18.38         | 125.27         | 0.60805E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 18.10                                      | 21534E 08  | 18.02         | 125.45         | 0.60805E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 18.20                                      | 21534E 08  | 17.66         | 125.63         | 0.60805E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 18.30                                      | 21534E 08  | 17.30         | 125.81         | 0.60805E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 18.40                                      | 21534E 08  | 16.95         | 125.99         | 0.60805E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 18.50                                      | 21534E 08  | 16.59         | 126.17         | 0.60805E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 18.60                                      | 21534E 08  | 16.23         | 126.34         | 0.60805E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 18.70                                      | 21534E 08  | 15.87         | 126.52         | 0.60805E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 18.80                                      | 21534E 08  | 15.51         | 126.69         | 0.60805E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 18.90                                      | 21534E 08  | 15.15         | 126.87         | 0.60805E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 19.00                                      | 21534E 08  | 14.79         | 127.04         | 0.60805E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 19.10                                      | 21534E 08  | 14.43         | 127.21         | 0.60805E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 19.20                                      | 21534E 08  | 14.07         | 127.38         | 0.60805E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 19.30                                      | 21534E 08  | 13.70         | 127.56         | 0.60805E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 19.40                                      | 21534E 08  | 13.34         | 127.73         | 0.60805E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 19.50                                      | 21534E 08  | 12.98         | 127.90         | 0.60805E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 19.60                                      | 21534E 08  | 12.62         | 128.07         | 0.60805E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 19.70                                      | 21534E 08  | 12.26         | 128.24         | 0.60805E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 19.80                                      | 21534E 08  | 11.91         | 128.41         | 0.60805E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 19.90                                      | 21534E 08  | 11.54         | 128.57         | 0.60805E 06 | 0.25567E 05    | 0.                    | 0.                     |
| 20.00                                      | 21534E 08  | 11.17         | 128.74         | 0.60805E 06 | 0.25567E 05    | 0.                    | 0.                     |

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| RADAR PARAMETERS • TRAJECTORY NUMBER 1 |               |                        |                 |                   |              |                   |             |                   |  | 35.900 DEG. LAT. |  | 233.333 DEG. LONG. |  |
|--|---------------|------------------------|-----------------|-------------------|--------------|-------------------|-------------|-------------------|--|------------------|--|--------------------|--|
| TIME (MINS)                            | SL RANGE (NM) | SL RANGE-RATE (FT/SEC) | ELEVATION (DEG) | EL RATE (DEG/SEC) | AZMUTH (DEG) | AZ RATE (DEG/SEC) | RADIUS (FT) | INERTIAL PZ (DEG) |  |                  |  |                    |  |
| 11:00                                  | 0.761120      | 0.175410               | 05              | 0.527200          | 291.64       | 0.233200          | 1.029       | 51.66             |  |                  |  |                    |  |
| 11:10                                  | 0.749782      | 0.170505               | 05              | 0.526600          | 290.34       | 0.233200          | 1.029       | 51.64             |  |                  |  |                    |  |
| 11:20                                  | 0.727473      | 0.163772               | 05              | 0.526600          | 288.97       | 0.233200          | 1.029       | 51.62             |  |                  |  |                    |  |
| 11:30                                  | 0.711302      | 0.150042               | 05              | 0.528500          | 287.53       | 0.244200          | 1.029       | 51.60             |  |                  |  |                    |  |
| 11:40                                  | 0.695172      | 0.151212               | 05              | 0.526600          | 286.03       | 0.246100          | 1.029       | 51.58             |  |                  |  |                    |  |
| 11:50                                  | 0.680133      | 0.150805               | 05              | 0.523200          | 284.46       | 0.248000          | 1.029       | 51.55             |  |                  |  |                    |  |
| 12:00                                  | 0.665192      | 0.145912               | 05              | 0.521100          | 282.81       | 0.240800          | 1.029       | 51.53             |  |                  |  |                    |  |
| 12:10                                  | 0.651132      | 0.140725               | 05              | 0.510900          | 281.09       | 0.230200          | 1.029       | 51.50             |  |                  |  |                    |  |
| 12:20                                  | 0.637112      | 0.134475               | 05              | 0.501400          | 279.30       | 0.305500          | 1.029       | 51.48             |  |                  |  |                    |  |
| 12:30                                  | 0.624072      | 0.127952               | 05              | 0.499300          | 277.42       | 0.339300          | 1.029       | 51.42             |  |                  |  |                    |  |
| 12:40                                  | 0.612022      | 0.122745               | 05              | 0.474400          | 275.47       | 0.332500          | 1.029       | 51.40             |  |                  |  |                    |  |
| 12:50                                  | 0.600982      | 0.119181               | 05              | 0.562200          | 273.43       | 0.355500          | 1.029       | 51.44             |  |                  |  |                    |  |
| 13:00                                  | 0.590942      | 0.102422               | 05              | 0.434600          | 271.32       | 0.338200          | 1.029       | 51.40             |  |                  |  |                    |  |
| 13:10                                  | 0.580902      | 0.096279               | 05              | 0.409400          | 269.13       | 0.313200          | 1.029       | 51.35             |  |                  |  |                    |  |
| 13:20                                  | 0.570862      | 0.093402               | 05              | 0.380300          | 266.86       | 0.339200          | 1.029       | 51.40             |  |                  |  |                    |  |
| 13:30                                  | 0.562749      | 0.086062               | 05              | 0.471300          | 264.52       | 0.355200          | 1.029       | 51.35             |  |                  |  |                    |  |
| 13:40                                  | 0.555462      | 0.093302               | 05              | 0.370500          | 262.12       | 0.406800          | 1.029       | 51.40             |  |                  |  |                    |  |
| 13:50                                  | 0.548162      | 0.093802               | 05              | 0.270000          | 259.65       | 0.416100          | 1.029       | 51.39             |  |                  |  |                    |  |
| 14:00                                  | 0.540782      | 0.098662               | 05              | 0.260000          | 257.13       | 0.446200          | 1.029       | 51.39             |  |                  |  |                    |  |
| 14:10                                  | 0.533492      | 0.091562               | 05              | 0.381900          | 254.56       | 0.417200          | 1.029       | 51.37             |  |                  |  |                    |  |
| 14:20                                  | 0.526202      | 0.082799               | 05              | 0.429400          | 251.95       | 0.447100          | 1.029       | 51.37             |  |                  |  |                    |  |
| 14:30                                  | 0.518902      | 0.077912               | 05              | 0.379100          | 249.32       | 0.440200          | 1.029       | 51.34             |  |                  |  |                    |  |
| 14:40                                  | 0.510602      | 0.073202               | 05              | 0.352800          | 246.66       | 0.428200          | 1.029       | 51.34             |  |                  |  |                    |  |
| 14:50                                  | 0.503302      | 0.068702               | 05              | 0.327200          | 244.01       | 0.442200          | 1.029       | 51.37             |  |                  |  |                    |  |
| 15:00                                  | 0.530442      | 0.058870               | 05              | 0.403000          | 241.36       | 0.406200          | 1.029       | 51.30             |  |                  |  |                    |  |
| 15:10                                  | 0.531662      | 0.069612               | 05              | 0.331700          | 238.72       | 0.468200          | 1.029       | 51.30             |  |                  |  |                    |  |
| 15:20                                  | 0.532782      | 0.078862               | 05              | 0.317000          | 236.12       | 0.431200          | 1.029       | 51.25             |  |                  |  |                    |  |
| 15:30                                  | 0.536652      | 0.083162               | 05              | 0.381100          | 233.55       | 0.445200          | 1.029       | 51.25             |  |                  |  |                    |  |
| 15:40                                  | 0.540382      | 0.095852               | 05              | 0.428000          | 231.03       | 0.445200          | 1.029       | 51.20             |  |                  |  |                    |  |
| 15:50                                  | 0.543832      | 0.095802               | 05              | 0.412200          | 228.56       | 0.460200          | 1.029       | 51.22             |  |                  |  |                    |  |
| 16:00                                  | 0.555582      | 0.093632               | 05              | 0.348800          | 226.16       | 0.351200          | 1.029       | 51.14             |  |                  |  |                    |  |
| 16:10                                  | 0.563392      | 0.093432               | 05              | 0.381500          | 223.82       | 0.363200          | 1.029       | 51.36             |  |                  |  |                    |  |
| 16:20                                  | 0.582282      | 0.097672               | 05              | 0.410400          | 221.56       | 0.371200          | 1.029       | 51.28             |  |                  |  |                    |  |
| 16:30                                  | 0.593332      | 0.105312               | 05              | 0.354200          | 219.37       | 0.383200          | 1.029       | 51.23             |  |                  |  |                    |  |
| 16:40                                  | 0.613422      | 0.113452               | 05              | 0.456800          | 217.26       | 0.355200          | 1.029       | 51.04             |  |                  |  |                    |  |
| 16:50                                  | 0.619122      | 0.120492               | 05              | 0.474800          | 215.23       | 0.351200          | 1.029       | 51.02             |  |                  |  |                    |  |
| 17:00                                  | 0.625192      | 0.128192               | 05              | 0.501600          | 213.28       | 0.356200          | 1.029       | 51.03             |  |                  |  |                    |  |
| 17:10                                  | 0.638462      | 0.146472               | 05              | 0.421600          | 211.41       | 0.356200          | 1.029       | 51.03             |  |                  |  |                    |  |
| 17:20                                  | 0.651762      | 0.148762               | 05              | 0.410900          | 209.61       | 0.284200          | 1.029       | 51.04             |  |                  |  |                    |  |
| 17:30                                  | 0.660952      | 0.146122               | 05              | 0.377900          | 207.89       | 0.268200          | 1.029       | 51.05             |  |                  |  |                    |  |
| 17:40                                  | 0.667352      | 0.152172               | 05              | 0.230000          | 206.25       | 0.258200          | 1.029       | 51.05             |  |                  |  |                    |  |
| 17:50                                  | 0.669542      | 0.162752               | 05              | 0.152630          | 204.68       | 0.260200          | 1.029       | 51.05             |  |                  |  |                    |  |
| 18:00                                  | 0.695772      | 0.162402               | 05              | 0.028100          | 203.18       | 0.240200          | 1.029       | 51.06             |  |                  |  |                    |  |
| 18:10                                  | 0.711732      | 0.166862               | 05              | 0.028600          | 201.74       | 0.237200          | 1.029       | 51.06             |  |                  |  |                    |  |
| 18:20                                  | 0.720482      | 0.174332               | 05              | 0.028100          | 200.37       | 0.232200          | 1.029       | 51.06             |  |                  |  |                    |  |
| 18:30                                  | 0.746162      | 0.174492               | 05              | 0.026700          | 199.06       | 0.213200          | 1.029       | 51.06             |  |                  |  |                    |  |

# TRAJECTORY PARAMETERS • TRAJECTORY NUMBER 4

| TIME (MIN) | RADIUS (FT) | LATITUDE (DEG) | LONGITUDE (DEG) | HEIGHT (FT) | VELOCITY (FT/S) | BAL. COEFF. (PT. * 2 / SLG) | ATMOS. DENS. (SLG / FT. * 3) |
|------------|-------------|----------------|-----------------|-------------|-----------------|-----------------------------|------------------------------|
| 0.00       | 21534E 08   | 62.77          | 40.35           | 0.60803E 06 | 0.255674E 05    | 0.                          | 0.                           |
| 0.10       | 21534E 08   | 62.76          | 41.21           | 0.60806E 06 | 0.255674E 05    | 0.                          | 0.                           |
| 0.20       | 21534E 08   | 62.8           | 42.07           | 0.60809E 06 | 0.255674E 05    | 0.                          | 0.                           |
| 0.30       | 21534E 08   | 62.85          | 42.93           | 0.60812E 06 | 0.255673E 05    | 0.                          | 0.                           |
| 0.40       | 21534E 08   | 62.89          | 43.80           | 0.60815E 06 | 0.255673E 05    | 0.                          | 0.                           |
| 0.50       | 21534E 08   | 62.92          | 44.67           | 0.60818E 06 | 0.255672E 05    | 0.                          | 0.                           |
| 0.60       | 21534E 08   | 62.95          | 45.54           | 0.60821E 06 | 0.255672E 05    | 0.                          | 0.                           |
| 0.70       | 21534E 08   | 62.97          | 46.41           | 0.60824E 06 | 0.255672E 05    | 0.                          | 0.                           |
| 0.80       | 21534E 08   | 62.99          | 47.28           | 0.60827E 06 | 0.255671E 05    | 0.                          | 0.                           |
| 0.90       | 21534E 08   | 63.00          | 48.15           | 0.60830E 06 | 0.255671E 05    | 0.                          | 0.                           |
| 1.00       | 21534E 08   | 63.01          | 49.03           | 0.60833E 06 | 0.255671E 05    | 0.                          | 0.                           |
| 1.10       | 21534E 08   | 63.00          | 49.90           | 0.60836E 06 | 0.255670E 05    | 0.                          | 0.                           |
| 1.20       | 21534E 08   | 62.99          | 50.77           | 0.60839E 06 | 0.255670E 05    | 0.                          | 0.                           |
| 1.30       | 21534E 08   | 62.98          | 51.65           | 0.60842E 06 | 0.255670E 05    | 0.                          | 0.                           |
| 1.40       | 21534E 08   | 62.96          | 52.52           | 0.60845E 06 | 0.255669E 05    | 0.                          | 0.                           |
| 1.50       | 21534E 08   | 62.94          | 53.39           | 0.60848E 06 | 0.255669E 05    | 0.                          | 0.                           |
| 1.60       | 21534E 08   | 62.91          | 54.26           | 0.60851E 06 | 0.255669E 05    | 0.                          | 0.                           |
| 1.70       | 21534E 08   | 62.87          | 55.13           | 0.60854E 06 | 0.255668E 05    | 0.                          | 0.                           |
| 1.80       | 21534E 08   | 62.83          | 55.99           | 0.60857E 06 | 0.255668E 05    | 0.                          | 0.                           |
| 1.90       | 21534E 08   | 62.78          | 56.85           | 0.60860E 06 | 0.255667E 05    | 0.                          | 0.                           |
| 2.00       | 21534E 08   | 62.73          | 57.71           | 0.60863E 06 | 0.255667E 05    | 0.                          | 0.                           |
| 2.10       | 21534E 08   | 62.67          | 58.57           | 0.60866E 06 | 0.255667E 05    | 0.                          | 0.                           |
| 2.20       | 21534E 08   | 62.61          | 59.42           | 0.60869E 06 | 0.255666E 05    | 0.                          | 0.                           |
| 2.30       | 21534E 08   | 62.54          | 60.27           | 0.60872E 06 | 0.255666E 05    | 0.                          | 0.                           |
| 2.40       | 21534E 08   | 62.47          | 61.11           | 0.60875E 06 | 0.255666E 05    | 0.                          | 0.                           |
| 2.50       | 21534E 08   | 62.39          | 61.95           | 0.60878E 06 | 0.255665E 05    | 0.                          | 0.                           |
| 2.60       | 21534E 08   | 62.3           | 62.79           | 0.60881E 06 | 0.255665E 05    | 0.                          | 0.                           |
| 2.70       | 21534E 08   | 62.21          | 63.62           | 0.60883E 06 | 0.255665E 05    | 0.                          | 0.                           |
| 2.80       | 21534E 08   | 62.12          | 64.45           | 0.60886E 06 | 0.255664E 05    | 0.                          | 0.                           |
| 2.90       | 21535E 08   | 62.02          | 65.26           | 0.60889E 06 | 0.255664E 05    | 0.                          | 0.                           |
| 3.00       | 21535E 08   | 61.9           | 66.08           | 0.60892E 06 | 0.255664E 05    | 0.                          | 0.                           |
| 3.10       | 21535E 08   | 61.80          | 66.89           | 0.60895E 06 | 0.255663E 05    | 0.                          | 0.                           |
| 3.20       | 21535E 08   | 61.69          | 67.69           | 0.60898E 06 | 0.255663E 05    | 0.                          | 0.                           |
| 3.30       | 21535E 08   | 61.57          | 68.48           | 0.60901E 06 | 0.255663E 05    | 0.                          | 0.                           |
| 3.40       | 21535E 08   | 61.44          | 69.27           | 0.60904E 06 | 0.255662E 05    | 0.                          | 0.                           |
| 3.50       | 21535E 08   | 61.31          | 70.05           | 0.60907E 06 | 0.255662E 05    | 0.                          | 0.                           |
| 3.60       | 21535E 08   | 61.17          | 70.83           | 0.60910E 06 | 0.255662E 05    | 0.                          | 0.                           |
| 3.70       | 21535E 08   | 61.04          | 71.60           | 0.60913E 06 | 0.255661E 05    | 0.                          | 0.                           |
| 3.80       | 21535E 08   | 60.89          | 72.36           | 0.60916E 06 | 0.255661E 05    | 0.                          | 0.                           |
| 3.90       | 21535E 08   | 60.74          | 73.11           | 0.60918E 06 | 0.255660E 05    | 0.                          | 0.                           |
| 4.00       | 21535E 08   | 60.59          | 73.86           | 0.60921E 06 | 0.255660E 05    | 0.                          | 0.                           |
| 4.10       | 21535E 08   | 60.43          | 74.60           | 0.60924E 06 | 0.255660E 05    | 0.                          | 0.                           |
| 4.20       | 21535E 08   | 60.27          | 75.33           | 0.60927E 06 | 0.255659E 05    | 0.                          | 0.                           |
| 4.30       | 21535E 08   | 60.10          | 76.06           | 0.60930E 06 | 0.255659E 05    | 0.                          | 0.                           |
| 4.40       | 21535E 08   | 59.93          | 76.77           | 0.60933E 06 | 0.255659E 05    | 0.                          | 0.                           |
| 4.50       | 21535E 08   | 59.76          | 77.48           | 0.60936E 06 | 0.255658E 05    | 0.                          | 0.                           |
| 4.60       | 21535E 08   | 59.58          | 78.18           | 0.60938E 06 | 0.255658E 05    | 0.                          | 0.                           |
| 4.70       | 21535E 08   | 59.40          | 78.88           | 0.60941E 06 | 0.255658E 05    | 0.                          | 0.                           |
| 4.80       | 21535E 08   | 59.21          | 79.56           | 0.60944E 06 | 0.255657E 05    | 0.                          | 0.                           |
| 4.90       | 21535E 08   | 59.02          | 80.24           | 0.60947E 06 | 0.255657E 05    | 0.                          | 0.                           |
| 5.00       | 21535E 08   | 58.82          | 80.91           | 0.60950E 06 | 0.255657E 05    | 0.                          | 0.                           |
| 5.10       | 21535E 08   | 58.63          | 81.57           | 0.60953E 06 | 0.255656E 05    | 0.                          | 0.                           |

# TRAJECTORY PARAMETERS , TRAJECTORY NUMBER 4

| TIME(MIN) | RADIUS(FT) | LATITUDE(DEC) | LONGITUDE(DEC) | HEIGHT(FT) | VELOCITY(FT/SEC) | BAL.COEFF.(P+2/SLG) | ATMOS.DENS.(SLG/P8+03) |
|-----------|------------|---------------|----------------|------------|------------------|---------------------|------------------------|
| 5.20      | 215352     | 58.42         | 82.23          | 0.609552   | 0.255652         | 0.                  | 0.                     |
| 5.22      | 215352     | 58.22         | 82.88          | 0.609582   | 0.255682         | 0.                  | 0.                     |
| 5.30      | 215352     | 58.01         | 83.52          | 0.609612   | 0.255652         | 0.                  | 0.                     |
| 5.40      | 215352     | 57.80         | 84.15          | 0.609642   | 0.255652         | 0.                  | 0.                     |
| 5.50      | 215352     | 57.58         | 84.77          | 0.609672   | 0.255652         | 0.                  | 0.                     |
| 5.60      | 215352     | 57.37         | 85.39          | 0.609692   | 0.255652         | 0.                  | 0.                     |
| 5.70      | 215352     | 57.14         | 85.99          | 0.609722   | 0.255652         | 0.                  | 0.                     |
| 5.80      | 215352     | 56.92         | 86.59          | 0.609752   | 0.255652         | 0.                  | 0.                     |
| 5.90      | 215352     | 56.69         | 87.19          | 0.609782   | 0.255652         | 0.                  | 0.                     |
| 6.00      | 215352     | 56.46         | 87.77          | 0.609802   | 0.255652         | 0.                  | 0.                     |
| 6.10      | 215352     | 56.22         | 88.35          | 0.609832   | 0.255652         | 0.                  | 0.                     |
| 6.20      | 215352     | 55.99         | 88.92          | 0.609862   | 0.255652         | 0.                  | 0.                     |
| 6.30      | 215352     | 55.75         | 89.49          | 0.609882   | 0.255652         | 0.                  | 0.                     |
| 6.40      | 215352     | 55.51         | 90.04          | 0.609912   | 0.255652         | 0.                  | 0.                     |
| 6.50      | 215352     | 55.26         | 90.59          | 0.609942   | 0.255652         | 0.                  | 0.                     |
| 6.60      | 215352     | 55.01         | 91.13          | 0.609972   | 0.255652         | 0.                  | 0.                     |
| 6.70      | 215352     | 54.76         | 91.67          | 0.609992   | 0.255652         | 0.                  | 0.                     |
| 6.80      | 215352     | 54.51         | 92.20          | 0.610022   | 0.255652         | 0.                  | 0.                     |
| 6.90      | 215352     | 54.25         | 92.72          | 0.610052   | 0.255652         | 0.                  | 0.                     |
| 7.00      | 215352     | 53.99         | 93.23          | 0.610072   | 0.255652         | 0.                  | 0.                     |
| 7.10      | 215352     | 53.73         | 93.74          | 0.610102   | 0.255652         | 0.                  | 0.                     |
| 7.20      | 215352     | 53.47         | 94.24          | 0.610122   | 0.255652         | 0.                  | 0.                     |
| 7.30      | 215352     | 53.21         | 94.73          | 0.610152   | 0.255652         | 0.                  | 0.                     |
| 7.40      | 215352     | 52.94         | 95.22          | 0.610182   | 0.255652         | 0.                  | 0.                     |
| 7.50      | 215352     | 52.67         | 95.70          | 0.610202   | 0.255652         | 0.                  | 0.                     |
| 7.60      | 215352     | 52.40         | 96.18          | 0.610232   | 0.255652         | 0.                  | 0.                     |
| 7.70      | 215352     | 52.12         | 96.65          | 0.610252   | 0.255652         | 0.                  | 0.                     |
| 7.80      | 215352     | 51.85         | 97.11          | 0.610282   | 0.255652         | 0.                  | 0.                     |
| 7.90      | 215352     | 51.57         | 97.57          | 0.610302   | 0.255652         | 0.                  | 0.                     |
| 8.00      | 215352     | 51.29         | 98.02          | 0.610332   | 0.255652         | 0.                  | 0.                     |
| 8.10      | 215352     | 51.01         | 98.47          | 0.610352   | 0.255652         | 0.                  | 0.                     |
| 8.20      | 215352     | 50.73         | 98.91          | 0.610382   | 0.255652         | 0.                  | 0.                     |
| 8.30      | 215352     | 50.44         | 99.34          | 0.610402   | 0.255652         | 0.                  | 0.                     |
| 8.40      | 215352     | 50.15         | 99.77          | 0.610432   | 0.255652         | 0.                  | 0.                     |
| 8.50      | 215352     | 49.86         | 100.20         | 0.610452   | 0.255652         | 0.                  | 0.                     |
| 8.60      | 215352     | 49.57         | 100.61         | 0.610482   | 0.255652         | 0.                  | 0.                     |
| 8.70      | 215352     | 49.28         | 101.03         | 0.610502   | 0.255652         | 0.                  | 0.                     |
| 8.80      | 215352     | 48.99         | 101.43         | 0.610532   | 0.255652         | 0.                  | 0.                     |
| 8.90      | 215352     | 48.69         | 101.84         | 0.610552   | 0.255652         | 0.                  | 0.                     |
| 9.00      | 215352     | 48.40         | 102.23         | 0.610582   | 0.255652         | 0.                  | 0.                     |
| 9.10      | 215352     | 48.11         | 102.63         | 0.610602   | 0.255652         | 0.                  | 0.                     |
| 9.20      | 215352     | 47.80         | 103.01         | 0.610622   | 0.255652         | 0.                  | 0.                     |
| 9.30      | 215352     | 47.51         | 103.40         | 0.610652   | 0.255652         | 0.                  | 0.                     |
| 9.40      | 215352     | 47.19         | 103.78         | 0.610672   | 0.255652         | 0.                  | 0.                     |
| 9.50      | 215352     | 46.89         | 104.15         | 0.610692   | 0.255652         | 0.                  | 0.                     |
| 9.60      | 215352     | 46.58         | 104.52         | 0.610722   | 0.255652         | 0.                  | 0.                     |
| 9.70      | 215352     | 46.28         | 104.88         | 0.610742   | 0.255652         | 0.                  | 0.                     |
| 9.80      | 215352     | 45.97         | 105.24         | 0.610762   | 0.255652         | 0.                  | 0.                     |
| 9.90      | 215352     | 45.66         | 105.60         | 0.610792   | 0.255652         | 0.                  | 0.                     |
| 10.00     | 215352     | 45.35         | 105.95         | 0.610812   | 0.255652         | 0.                  | 0.                     |
| 10.10     | 215352     | 45.03         | 106.30         | 0.610832   | 0.255652         | 0.                  | 0.                     |
| 10.20     | 215352     | 44.72         | 106.65         | 0.610862   | 0.255652         | 0.                  | 0.                     |
| 10.30     | 215352     |               |                |            |                  |                     |                        |



| TRAJECTORY PARAMETERS, TRAJECTORY NUMBER 4 |            |               |                |            |                |                       |                        |
|--|------------|---------------|----------------|------------|----------------|-----------------------|------------------------|
| TIME(MIN)                                  | RADIUS(FT) | LATITUDE(DEG) | LONGITUDE(DEG) | HEIGHT(FT) | VELOCITY(FT/S) | BAL.COEFF.(FT**2/SLG) | ATMOS.DENS.(SLG/FT**3) |
| 10.40                                      | 21537.8    | 44.41         | 106.98         | 0.6108E 06 | 0.255640E 05   | 0.                    | 0.                     |
| 10.50                                      | 21537.8    | 44.09         | 107.32         | 0.6109E 06 | 0.255640E 05   | 0.                    | 0.                     |
| 10.60                                      | 21537.8    | 43.77         | 107.65         | 0.6109E 06 | 0.255640E 05   | 0.                    | 0.                     |
| 10.70                                      | 21537.8    | 43.46         | 107.98         | 0.6109E 06 | 0.255640E 05   | 0.                    | 0.                     |
| 10.80                                      | 21537.8    | 43.14         | 108.31         | 0.6109E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 10.90                                      | 21537.8    | 42.82         | 108.63         | 0.6109E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 11.00                                      | 21537.8    | 42.5          | 108.94         | 0.6110E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 11.10                                      | 21537.8    | 42.17         | 109.26         | 0.6110E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 11.20                                      | 21537.8    | 41.85         | 109.57         | 0.6110E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 11.30                                      | 21537.8    | 41.53         | 109.88         | 0.6110E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 11.40                                      | 21537.8    | 41.2          | 110.18         | 0.6110E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 11.50                                      | 21537.8    | 40.86         | 110.48         | 0.6111E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 11.60                                      | 21537.8    | 40.55         | 110.78         | 0.6111E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 11.70                                      | 21537.8    | 40.22         | 111.07         | 0.6111E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 11.80                                      | 21537.8    | 39.89         | 111.36         | 0.6111E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 11.90                                      | 21537.8    | 39.56         | 111.65         | 0.6111E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 12.00                                      | 21537.8    | 39.23         | 111.94         | 0.6112E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 12.10                                      | 21537.8    | 38.90         | 112.22         | 0.6112E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 12.20                                      | 21537.8    | 38.57         | 112.50         | 0.6112E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 12.30                                      | 21537.8    | 38.24         | 112.78         | 0.6112E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 12.40                                      | 21537.8    | 37.91         | 113.05         | 0.6112E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 12.50                                      | 21537.8    | 37.57         | 113.32         | 0.6113E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 12.60                                      | 21537.8    | 37.24         | 113.59         | 0.6113E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 12.70                                      | 21537.8    | 36.90         | 113.85         | 0.6113E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 12.80                                      | 21537.8    | 36.56         | 114.12         | 0.6113E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 12.90                                      | 21537.8    | 36.23         | 114.38         | 0.6113E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 13.00                                      | 21537.8    | 35.89         | 114.64         | 0.6114E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 13.10                                      | 21537.8    | 35.55         | 114.9          | 0.6114E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 13.20                                      | 21537.8    | 35.21         | 115.15         | 0.6114E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 13.30                                      | 21537.8    | 34.87         | 115.40         | 0.6114E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 13.40                                      | 21537.8    | 34.53         | 115.65         | 0.6114E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 13.50                                      | 21537.8    | 34.19         | 115.99         | 0.6114E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 13.60                                      | 21537.8    | 33.85         | 116.14         | 0.6115E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 13.70                                      | 21537.8    | 33.51         | 116.38         | 0.6115E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 13.80                                      | 21537.8    | 33.17         | 116.62         | 0.6115E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 13.90                                      | 21537.8    | 32.82         | 116.86         | 0.6115E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 14.00                                      | 21537.8    | 32.48         | 117.10         | 0.6115E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 14.10                                      | 21537.8    | 32.14         | 117.33         | 0.6115E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 14.20                                      | 21537.8    | 31.79         | 117.56         | 0.6116E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 14.30                                      | 21537.8    | 31.45         | 117.79         | 0.6116E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 14.40                                      | 21537.8    | 31.1          | 118.02         | 0.6116E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 14.50                                      | 21537.8    | 30.75         | 118.25         | 0.6116E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 14.60                                      | 21537.8    | 30.41         | 118.47         | 0.6116E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 14.70                                      | 21537.8    | 30.06         | 118.70         | 0.6116E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 14.80                                      | 21537.8    | 29.71         | 118.92         | 0.6117E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 14.90                                      | 21537.8    | 29.36         | 119.14         | 0.6117E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 15.00                                      | 21537.8    | 29.02         | 119.35         | 0.6117E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 15.10                                      | 21537.8    | 28.67         | 119.57         | 0.6117E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 15.20                                      | 21537.8    | 28.32         | 119.79         | 0.6117E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 15.30                                      | 21537.8    | 27.97         | 120.00         | 0.6117E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 15.40                                      | 21537.8    | 27.62         | 120.21         | 0.6117E 06 | 0.255632E 05   | 0.                    | 0.                     |
| 15.50                                      | 21537.8    | 27.27         | 120.42         | 0.6118E 06 | 0.255632E 05   | 0.                    | 0.                     |



# TRAJECTORY PARAMETERS, TRAJECTORY NUMBER 4

| TIME(MIN) | RADIUS(FT) | LATITUDE(DEG) | LONGITUDE(DEG) | HEIGHT(FT) | VELOCITY(MT/S) | BAL.COEFF.(FT**2/SLG) | ATMOS.DENS.(SLG/FT**3) |
|-----------|------------|---------------|----------------|------------|----------------|-----------------------|------------------------|
| 15.00     | 2157.08    | 26.92         | 120.63         | 0.6182E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 15.10     | 2157.08    | 26.92         | 120.64         | 0.6183E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 15.20     | 2157.08    | 26.92         | 120.64         | 0.6183E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 15.30     | 2157.08    | 26.92         | 121.04         | 0.6184E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 15.40     | 2157.08    | 26.92         | 121.25         | 0.6186E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 15.50     | 2157.08    | 26.92         | 121.45         | 0.6187E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 16.00     | 2158.08    | 25.51         | 121.45         | 0.6188E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 16.10     | 2158.08    | 25.51         | 121.45         | 0.6188E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 16.20     | 2158.08    | 25.51         | 121.85         | 0.6190E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 16.30     | 2158.08    | 25.51         | 122.05         | 0.6191E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 16.40     | 2158.08    | 25.51         | 122.25         | 0.6192E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 16.50     | 2158.08    | 23.74         | 122.45         | 0.6193E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 16.60     | 2158.08    | 23.39         | 122.64         | 0.6194E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 16.70     | 2158.08    | 23.03         | 122.84         | 0.6195E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 16.80     | 2158.08    | 22.68         | 123.03         | 0.6197E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 16.90     | 2158.08    | 22.32         | 123.22         | 0.6198E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 17.00     | 2158.08    | 21.97         | 123.41         | 0.6199E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 17.10     | 2158.08    | 21.61         | 123.60         | 0.6100E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 17.20     | 2158.08    | 21.25         | 123.79         | 0.6101E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 17.30     | 2158.08    | 20.90         | 123.98         | 0.6102E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 17.40     | 2158.08    | 20.54         | 124.16         | 0.6103E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 17.50     | 2158.08    | 20.18         | 124.35         | 0.6104E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 17.60     | 2158.08    | 19.83         | 124.53         | 0.6105E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 17.70     | 2158.08    | 19.47         | 124.72         | 0.6106E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 17.80     | 2158.08    | 19.11         | 124.90         | 0.6107E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 17.90     | 2158.08    | 18.75         | 125.08         | 0.6108E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 18.00     | 2158.08    | 18.39         | 125.26         | 0.6109E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 18.10     | 2158.08    | 18.04         | 125.44         | 0.6109E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 18.20     | 2158.08    | 17.68         | 125.62         | 0.6110E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 18.30     | 2158.08    | 17.32         | 125.80         | 0.6111E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 18.40     | 2158.08    | 16.96         | 125.98         | 0.6112E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 18.50     | 2158.08    | 16.60         | 126.16         | 0.6113E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 18.60     | 2158.08    | 16.24         | 126.33         | 0.6113E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 18.70     | 2158.08    | 15.88         | 126.51         | 0.6114E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 18.80     | 2158.08    | 15.52         | 126.68         | 0.6115E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 18.90     | 2158.08    | 15.16         | 126.86         | 0.6115E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 19.00     | 2158.08    | 14.80         | 127.03         | 0.6116E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 19.10     | 2158.08    | 14.44         | 127.20         | 0.6117E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 19.20     | 2158.08    | 14.08         | 127.38         | 0.6117E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 19.30     | 2158.08    | 13.72         | 127.55         | 0.6118E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 19.40     | 2158.08    | 13.36         | 127.72         | 0.6119E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 19.50     | 2158.08    | 13.00         | 127.89         | 0.6119E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 19.60     | 2158.08    | 12.64         | 128.06         | 0.6120E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 19.70     | 2158.08    | 12.28         | 128.23         | 0.6120E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 19.80     | 2158.08    | 11.91         | 128.40         | 0.6121E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 19.90     | 2158.08    | 11.55         | 128.56         | 0.6121E 06 | 0.25569E 05    | 0.                    | 0.                     |
| 20.00     | 2158.08    | 11.19         | 128.73         | 0.6122E 06 | 0.25569E 05    | 0.                    | 0.                     |

| RADAR PARAMETERS |               |                      |                 |                 |               |                 |              |                     |  | 35.900 DEG. LAT. 233.333 DEG. LONG. |               |                      |                 |                 |               |                 |              |                     |  |
|------------------|---------------|----------------------|-----------------|-----------------|---------------|-----------------|--------------|---------------------|--|-------------------------------------|---------------|----------------------|-----------------|-----------------|---------------|-----------------|--------------|---------------------|--|
| TIME (MIN)       | SL RANGE (NM) | SL RANGE-RATE (FT/S) | ELEVATION (DEG) | EL RATE (DEG/S) | AZIMUTH (DEG) | AZ RATE (DEG/S) | RADIUS (ERV) | INFEEDIAL PHI (DEG) |  | TIME (MIN)                          | SL RANGE (NM) | SL RANGE-RATE (FT/S) | ELEVATION (DEG) | EL RATE (DEG/S) | AZIMUTH (DEG) | AZ RATE (DEG/S) | RADIUS (ERV) | INFEEDIAL PHI (DEG) |  |
| 11.80            | 0.77882E 03   | -0.178166E 05        | 1.02            | 0.5267E-01      | 292.92        | -0.2033E 00     | 1.029        | 51.36               |  | 11.80                               | 0.77882E 03   | -0.178166E 05        | 1.02            | 0.5267E-01      | 292.92        | -0.2033E 00     | 1.029        | 51.36               |  |
| 11.90            | 0.76476E 03   | -0.17544E 05         | 1.34            | 0.5288E-01      | 291.87        | -0.2128E 00     | 1.029        | 51.55               |  | 11.90                               | 0.76476E 03   | -0.17544E 05         | 1.34            | 0.5288E-01      | 291.87        | -0.2128E 00     | 1.029        | 51.55               |  |
| 12.00            | 0.74444E 03   | -0.17059E 05         | 1.65            | 0.5303E-01      | 290.36        | -0.2228E 00     | 1.029        | 51.74               |  | 12.00                               | 0.74444E 03   | -0.17059E 05         | 1.65            | 0.5303E-01      | 290.36        | -0.2228E 00     | 1.029        | 51.74               |  |
| 12.10            | 0.72803E 03   | -0.16649E 05         | 1.97            | 0.5308E-01      | 288.99        | -0.2338E 00     | 1.029        | 52.22               |  | 12.10                               | 0.72803E 03   | -0.16649E 05         | 1.97            | 0.5308E-01      | 288.99        | -0.2338E 00     | 1.029        | 52.22               |  |
| 12.20            | 0.71591E 03   | -0.16228E 05         | 2.29            | 0.5303E-01      | 287.56        | -0.2448E 00     | 1.029        | 52.50               |  | 12.20                               | 0.71591E 03   | -0.16228E 05         | 2.29            | 0.5303E-01      | 287.56        | -0.2448E 00     | 1.029        | 52.50               |  |
| 12.30            | 0.69834E 03   | -0.15724E 05         | 2.61            | 0.5285E-01      | 286.06        | -0.2558E 00     | 1.029        | 52.78               |  | 12.30                               | 0.69834E 03   | -0.15724E 05         | 2.61            | 0.5285E-01      | 286.06        | -0.2558E 00     | 1.029        | 52.78               |  |
| 12.40            | 0.68567E 03   | -0.15212E 05         | 2.92            | 0.5251E-01      | 284.49        | -0.2677E 00     | 1.029        | 53.05               |  | 12.40                               | 0.68567E 03   | -0.15212E 05         | 2.92            | 0.5251E-01      | 284.49        | -0.2677E 00     | 1.029        | 53.05               |  |
| 12.50            | 0.66822E 03   | -0.14664E 05         | 3.24            | 0.5200E-01      | 282.85        | -0.2800E 00     | 1.029        | 53.32               |  | 12.50                               | 0.66822E 03   | -0.14664E 05         | 3.24            | 0.5200E-01      | 282.85        | -0.2800E 00     | 1.029        | 53.32               |  |
| 12.60            | 0.65163E 03   | -0.14076E 05         | 3.55            | 0.5129E-01      | 281.13        | -0.2928E 00     | 1.029        | 53.59               |  | 12.60                               | 0.65163E 03   | -0.14076E 05         | 3.55            | 0.5129E-01      | 281.13        | -0.2928E 00     | 1.029        | 53.59               |  |
| 12.70            | 0.63048E 03   | -0.13453E 05         | 3.85            | 0.5035E-01      | 279.43        | -0.3052E 00     | 1.029        | 53.85               |  | 12.70                               | 0.63048E 03   | -0.13453E 05         | 3.85            | 0.5035E-01      | 279.43        | -0.3052E 00     | 1.029        | 53.85               |  |
| 12.80            | 0.62579E 03   | -0.12881E 05         | 4.15            | 0.4915E-01      | 277.46        | -0.3187E 00     | 1.029        | 54.12               |  | 12.80                               | 0.62579E 03   | -0.12881E 05         | 4.15            | 0.4915E-01      | 277.46        | -0.3187E 00     | 1.029        | 54.12               |  |
| 12.90            | 0.61822E 03   | -0.12083E 05         | 4.44            | 0.4768E-01      | 275.51        | -0.3318E 00     | 1.029        | 54.38               |  | 12.90                               | 0.61822E 03   | -0.12083E 05         | 4.44            | 0.4768E-01      | 275.51        | -0.3318E 00     | 1.029        | 54.38               |  |
| 13.00            | 0.61268E 03   | -0.11395E 05         | 4.72            | 0.4585E-01      | 273.48        | -0.3452E 00     | 1.029        | 54.64               |  | 13.00                               | 0.61268E 03   | -0.11395E 05         | 4.72            | 0.4585E-01      | 273.48        | -0.3452E 00     | 1.029        | 54.64               |  |
| 13.10            | 0.59047E 03   | -0.10531E 05         | 5.09            | 0.4369E-01      | 271.37        | -0.3582E 00     | 1.029        | 54.99               |  | 13.10                               | 0.59047E 03   | -0.10531E 05         | 5.09            | 0.4369E-01      | 271.37        | -0.3582E 00     | 1.029        | 54.99               |  |
| 13.20            | 0.58489E 03   | -0.96919E 04         | 5.45            | 0.4117E-01      | 269.18        | -0.3712E 00     | 1.029        | 55.15               |  | 13.20                               | 0.58489E 03   | -0.96919E 04         | 5.45            | 0.4117E-01      | 269.18        | -0.3712E 00     | 1.029        | 55.15               |  |
| 13.30            | 0.57135E 03   | -0.88143E 04         | 5.79            | 0.3827E-01      | 266.92        | -0.3838E 00     | 1.029        | 55.40               |  | 13.30                               | 0.57135E 03   | -0.88143E 04         | 5.79            | 0.3827E-01      | 266.92        | -0.3838E 00     | 1.029        | 55.40               |  |
| 13.40            | 0.56312E 03   | -0.78948E 04         | 5.71            | 0.3497E-01      | 264.58        | -0.3952E 00     | 1.029        | 55.55               |  | 13.40                               | 0.56312E 03   | -0.78948E 04         | 5.71            | 0.3497E-01      | 264.58        | -0.3952E 00     | 1.029        | 55.55               |  |
| 13.50            | 0.55578E 03   | -0.69325E 04         | 5.90            | 0.3129E-01      | 262.18        | -0.4060E 00     | 1.029        | 55.99               |  | 13.50                               | 0.55578E 03   | -0.69325E 04         | 5.90            | 0.3129E-01      | 262.18        | -0.4060E 00     | 1.029        | 55.99               |  |
| 13.60            | 0.54943E 03   | -0.59335E 04         | 6.08            | 0.2723E-01      | 259.71        | -0.4159E 00     | 1.029        | 56.14               |  | 13.60                               | 0.54943E 03   | -0.59335E 04         | 6.08            | 0.2723E-01      | 259.71        | -0.4159E 00     | 1.029        | 56.14               |  |
| 13.70            | 0.54081E 03   | -0.49036E 04         | 6.23            | 0.2283E-01      | 257.19        | -0.4292E 00     | 1.029        | 56.38               |  | 13.70                               | 0.54081E 03   | -0.49036E 04         | 6.23            | 0.2283E-01      | 257.19        | -0.4292E 00     | 1.029        | 56.38               |  |
| 13.80            | 0.53976E 03   | -0.38454E 04         | 6.35            | 0.1812E-01      | 254.62        | -0.4433E 00     | 1.029        | 56.62               |  | 13.80                               | 0.53976E 03   | -0.38454E 04         | 6.35            | 0.1812E-01      | 254.62        | -0.4433E 00     | 1.029        | 56.62               |  |
| 13.90            | 0.53499E 03   | -0.27649E 04         | 6.45            | 0.1315E-01      | 252.02        | -0.4568E 00     | 1.029        | 56.86               |  | 13.90                               | 0.53499E 03   | -0.27649E 04         | 6.45            | 0.1315E-01      | 252.02        | -0.4568E 00     | 1.029        | 56.86               |  |
| 14.00            | 0.53312E 03   | -0.16667E 04         | 6.51            | 0.0955E-02      | 249.38        | -0.4652E 00     | 1.029        | 57.10               |  | 14.00                               | 0.53312E 03   | -0.16667E 04         | 6.51            | 0.0955E-02      | 249.38        | -0.4652E 00     | 1.029        | 57.10               |  |
| 14.10            | 0.53343E 03   | -0.05808E 03         | 6.54            | 0.0719E-02      | 246.73        | -0.4682E 00     | 1.029        | 57.33               |  | 14.10                               | 0.53343E 03   | -0.05808E 03         | 6.54            | 0.0719E-02      | 246.73        | -0.4682E 00     | 1.029        | 57.33               |  |
| 14.20            | 0.53322E 03   | 0.55336E 03          | 6.54            | -0.0259E-02     | 244.28        | -0.4642E 00     | 1.029        | 57.56               |  | 14.20                               | 0.53322E 03   | 0.55336E 03          | 6.54            | -0.0259E-02     | 244.28        | -0.4642E 00     | 1.029        | 57.56               |  |
| 14.30            | 0.53404E 03   | 0.16613E 04          | 6.51            | -0.0785E-02     | 241.43        | -0.4652E 00     | 1.029        | 57.99               |  | 14.30                               | 0.53404E 03   | 0.16613E 04          | 6.51            | -0.0785E-02     | 241.43        | -0.4652E 00     | 1.029        | 57.99               |  |
| 14.40            | 0.53687E 03   | 0.27582E 04          | 6.45            | -0.0130E-01     | 238.80        | -0.4682E 00     | 1.029        | 58.22               |  | 14.40                               | 0.53687E 03   | 0.27582E 04          | 6.45            | -0.0130E-01     | 238.80        | -0.4682E 00     | 1.029        | 58.22               |  |
| 14.50            | 0.53974E 03   | 0.38393E 04          | 6.36            | -0.0480E-01     | 236.19        | -0.4682E 00     | 1.029        | 58.55               |  | 14.50                               | 0.53974E 03   | 0.38393E 04          | 6.36            | -0.0480E-01     | 236.19        | -0.4682E 00     | 1.029        | 58.55               |  |
| 14.60            | 0.54458E 03   | 0.48987E 04          | 6.23            | -0.0271E-01     | 233.62        | -0.4642E 00     | 1.029        | 58.77               |  | 14.60                               | 0.54458E 03   | 0.48987E 04          | 6.23            | -0.0271E-01     | 233.62        | -0.4642E 00     | 1.029        | 58.77               |  |
| 14.70            | 0.54902E 03   | 0.59212E 04          | 6.08            | -0.0212E-01     | 231.10        | -0.4419E 00     | 1.029        | 58.99               |  | 14.70                               | 0.54902E 03   | 0.59212E 04          | 6.08            | -0.0212E-01     | 231.10        | -0.4419E 00     | 1.029        | 58.99               |  |
| 14.80            | 0.55547E 03   | 0.69234E 04          | 5.91            | -0.0317E-01     | 228.63        | -0.4061E 00     | 1.029        | 58.22               |  | 14.80                               | 0.55547E 03   | 0.69234E 04          | 5.91            | -0.0317E-01     | 228.63        | -0.4061E 00     | 1.029        | 58.22               |  |
| 14.90            | 0.56335E 03   | 0.78833E 04          | 5.71            | -0.0486E-01     | 226.23        | -0.3952E 00     | 1.029        | 59.49               |  | 14.90                               | 0.56335E 03   | 0.78833E 04          | 5.71            | -0.0486E-01     | 226.23        | -0.3952E 00     | 1.029        | 59.49               |  |
| 15.00            | 0.57115E 03   | 0.88076E 04          | 5.49            | -0.0615E-01     | 223.89        | -0.3862E 00     | 1.029        | 59.55               |  | 15.00                               | 0.57115E 03   | 0.88076E 04          | 5.49            | -0.0615E-01     | 223.89        | -0.3862E 00     | 1.029        | 59.55               |  |
| 15.10            | 0.58029E 03   | 0.96863E 04          | 5.25            | -0.0406E-01     | 221.63        | -0.3712E 00     | 1.029        | 59.77               |  | 15.10                               | 0.58029E 03   | 0.96863E 04          | 5.25            | -0.0406E-01     | 221.63        | -0.3712E 00     | 1.029        | 59.77               |  |
| 15.20            | 0.59006E 03   | 0.10546E 05          | 5.00            | -0.0358E-01     | 219.44        | -0.3582E 00     | 1.029        | 59.99               |  | 15.20                               | 0.59006E 03   | 0.10546E 05          | 5.00            | -0.0358E-01     | 219.44        | -0.3582E 00     | 1.029        | 59.99               |  |
| 15.30            | 0.61187E 03   | 0.11380E 05          | 4.73            | -0.0457E-01     | 217.33        | -0.3482E 00     | 1.029        | 60.00               |  | 15.30                               | 0.61187E 03   | 0.11380E 05          | 4.73            | -0.0457E-01     | 217.33        | -0.3482E 00     | 1.029        | 60.00               |  |
| 15.40            | 0.61233E 03   | 0.12007E 05          | 4.45            | -0.0755E-01     | 215.29        | -0.3322E 00     | 1.029        | 60.14               |  | 15.40                               | 0.61233E 03   | 0.12007E 05          | 4.45            | -0.0755E-01     | 215.29        | -0.3322E 00     | 1.029        | 60.14               |  |
| 15.50            | 0.62499E 03   | 0.12746E 05          | 4.16            | -0.0905E-01     | 213.34        | -0.3102E 00     | 1.029        | 60.22               |  | 15.50                               | 0.62499E 03   | 0.12746E 05          | 4.16            | -0.0905E-01     | 213.34        | -0.3102E 00     | 1.029        | 60.22               |  |
| 15.60            | 0.63792E 03   | 0.13432E 05          | 3.86            | -0.0625E-01     | 211.46        | -0.3052E 00     | 1.029        | 60.33               |  | 15.60                               | 0.63792E 03   | 0.13432E 05          | 3.86            | -0.0625E-01     | 211.46        | -0.3052E 00     | 1.029        | 60.33               |  |
| 15.70            | 0.65150E 03   | 0.14062E 05          | 3.46            | -0.0512E-01     | 209.67        | -0.2938E 00     | 1.029        | 60.44               |  | 15.70                               | 0.65150E 03   | 0.14062E 05          | 3.46            | -0.0512E-01     | 209.67        | -0.2938E 00     | 1.029        | 60.44               |  |
| 15.80            | 0.66572E 03   | 0.14674E 05          | 3.05            | -0.0519E-01     | 207.95        | -0.2802E 00     | 1.029        | 61.04               |  | 15.80                               | 0.66572E 03   | 0.14674E 05          | 3.05            | -0.0519E-01     | 207.95        | -0.2802E 00     | 1.029        | 61.04               |  |
| 15.90            | 0.68099E 03   | 0.15194E 05          | 2.64            | -0.0542E-01     | 206.30        | -0.2682E 00     | 1.029        | 61.55               |  | 15.90                               | 0.68099E 03   | 0.15194E 05          | 2.64            | -0.0542E-01     | 206.30        | -0.2682E 00     | 1.029        | 61.55               |  |
| 16.00            | 0.69548E 03   | 0.15753E 05          | 2.20            | -0.0525E-01     | 204.73        | -0.2562E 00     | 1.029        | 61.55               |  | 16.00                               | 0.69548E 03   | 0.15753E 05          | 2.20            | -0.0525E-01     | 204.73        | -0.2562E 00     | 1.029        | 61.55               |  |
| 16.10            | 0.71385E 03   | 0.16182E 05          | 2.00            | -0.0594E-01     | 203.23        | -0.2492E 00     | 1.029        | 61.55               |  | 16.10                               | 0.71385E 03   | 0.16182E 05          | 2.00            | -0.0594E-01     | 203.23        | -0.2492E 00     | 1.029        | 61.55               |  |
| 16.20            | 0.72777E 03   | 0.16679E 05          | 1.99            | -0.0599E-01     | 201.79        | -0.2338E 00     | 1.029        | 61.55               |  | 16.20                               | 0.72777E 03   | 0.16679E 05          | 1.99            | -0.0599E-01     | 201.79        | -0.2338E 00     | 1.029        | 61.55               |  |
| 16.30            | 0.74419E 03   | 0.17043E 05          | 1.67            | -0.0594E-01     | 200.42        | -0.2238E 00     | 1.029        | 62.55               |  | 16.30                               | 0.74419E 03   | 0.17043E 05          | 1.67            | -0.0594E-01     | 200.42        | -0.2238E 00     | 1.029        | 62.55               |  |
| 16.40            | 0.76126E 03   | 0.17436E 05          | 1.35            | -0.0526E-01     | 199.11        | -0.2138E 00     | 1.029        | 62.55               |  | 16.40                               | 0.76126E 03   | 0.17436E 05          | 1.35            | -0.0526E-01     | 199.11        | -0.2138E 00     | 1.029        | 62.55               |  |
| 16.50            | 0.77887E 03   | 0.17796E 05          | 1.03            | -0.0559E-01     | 197.86        | -0.2039E 00     | 1.029        | 62.55               |  | 16.50                               | 0.77887E 03   | 0.17796E 05          | 1.03            | -0.0559E-01     | 197.86        | -0.2039E 00     | 1.029        | 62.55               |  |

# TRAJECTORY PARAMETERS, TRAJECTORY NUMBER 5

| TIME (MIN) | RADIUS (FT) | LATITUDE (DEG) | LONGITUDE (DEG) | HEIGHT (FT) | VELOCITY (FT/SEC) | BAL. COEFF. (FT**2/SLG) | ATMOS. DENS. (SLG/FT**3) |
|------------|-------------|----------------|-----------------|-------------|-------------------|-------------------------|--------------------------|
| 0.0        | 215342      | 62.70          | 40.35           | 0.68032     | 0.255512          | 0.0                     | 0.0                      |
| 0.10       | 215342      | 62.76          | 41.21           | 0.68032     | 0.255512          | 0.0                     | 0.0                      |
| 0.20       | 215342      | 62.81          | 42.07           | 0.68032     | 0.255512          | 0.0                     | 0.0                      |
| 0.30       | 215342      | 62.85          | 42.93           | 0.68032     | 0.255512          | 0.0                     | 0.0                      |
| 0.40       | 215342      | 62.89          | 43.80           | 0.68032     | 0.255512          | 0.0                     | 0.0                      |
| 0.50       | 215342      | 62.92          | 44.67           | 0.68032     | 0.255512          | 0.0                     | 0.0                      |
| 0.60       | 215342      | 62.95          | 45.54           | 0.68022     | 0.255512          | 0.0                     | 0.0                      |
| 0.70       | 215342      | 62.97          | 46.41           | 0.68022     | 0.255512          | 0.0                     | 0.0                      |
| 0.80       | 215342      | 62.99          | 47.28           | 0.68022     | 0.255512          | 0.0                     | 0.0                      |
| 0.90       | 215342      | 63.00          | 48.15           | 0.68022     | 0.255512          | 0.0                     | 0.0                      |
| 1.00       | 215342      | 63.00          | 49.03           | 0.68022     | 0.255512          | 0.0                     | 0.0                      |
| 1.10       | 215342      | 63.00          | 49.90           | 0.68022     | 0.255512          | 0.0                     | 0.0                      |
| 1.20       | 215342      | 63.00          | 50.77           | 0.68012     | 0.255512          | 0.0                     | 0.0                      |
| 1.30       | 215342      | 62.98          | 51.65           | 0.68012     | 0.255512          | 0.0                     | 0.0                      |
| 1.40       | 215342      | 62.96          | 52.52           | 0.68012     | 0.255512          | 0.0                     | 0.0                      |
| 1.50       | 215342      | 62.94          | 53.39           | 0.68012     | 0.255512          | 0.0                     | 0.0                      |
| 1.60       | 215342      | 62.91          | 54.26           | 0.68002     | 0.255512          | 0.0                     | 0.0                      |
| 1.70       | 215342      | 62.87          | 55.13           | 0.68002     | 0.255512          | 0.0                     | 0.0                      |
| 1.80       | 215342      | 62.83          | 55.99           | 0.68002     | 0.255512          | 0.0                     | 0.0                      |
| 1.90       | 215342      | 62.78          | 56.85           | 0.67992     | 0.255512          | 0.0                     | 0.0                      |
| 2.00       | 215342      | 62.73          | 57.71           | 0.67992     | 0.255512          | 0.0                     | 0.0                      |
| 2.10       | 215342      | 62.67          | 58.57           | 0.67982     | 0.255512          | 0.0                     | 0.0                      |
| 2.20       | 215342      | 62.61          | 59.42           | 0.67982     | 0.255512          | 0.0                     | 0.0                      |
| 2.30       | 215342      | 62.54          | 60.27           | 0.67982     | 0.255512          | 0.0                     | 0.0                      |
| 2.40       | 215342      | 62.47          | 61.11           | 0.67972     | 0.255512          | 0.0                     | 0.0                      |
| 2.50       | 215342      | 62.39          | 61.95           | 0.67972     | 0.255512          | 0.0                     | 0.0                      |
| 2.60       | 215342      | 62.31          | 62.79           | 0.67962     | 0.255512          | 0.0                     | 0.0                      |
| 2.70       | 215342      | 62.21          | 63.62           | 0.67962     | 0.255512          | 0.0                     | 0.0                      |
| 2.80       | 215342      | 62.12          | 64.44           | 0.67952     | 0.255512          | 0.0                     | 0.0                      |
| 2.90       | 215342      | 62.02          | 65.26           | 0.67952     | 0.255512          | 0.0                     | 0.0                      |
| 3.00       | 215342      | 61.91          | 66.08           | 0.67942     | 0.255512          | 0.0                     | 0.0                      |
| 3.10       | 215342      | 61.80          | 66.88           | 0.67932     | 0.255512          | 0.0                     | 0.0                      |
| 3.20       | 215342      | 61.69          | 67.69           | 0.67932     | 0.255512          | 0.0                     | 0.0                      |
| 3.30       | 215342      | 61.57          | 68.48           | 0.67922     | 0.255512          | 0.0                     | 0.0                      |
| 3.40       | 215342      | 61.44          | 69.27           | 0.67922     | 0.255512          | 0.0                     | 0.0                      |
| 3.50       | 215342      | 61.31          | 70.05           | 0.67912     | 0.255512          | 0.0                     | 0.0                      |
| 3.60       | 215342      | 61.18          | 70.83           | 0.67902     | 0.255512          | 0.0                     | 0.0                      |
| 3.70       | 215342      | 61.04          | 71.60           | 0.67892     | 0.255512          | 0.0                     | 0.0                      |
| 3.80       | 215342      | 60.89          | 72.36           | 0.67892     | 0.255512          | 0.0                     | 0.0                      |
| 3.90       | 215342      | 60.74          | 73.11           | 0.67882     | 0.255512          | 0.0                     | 0.0                      |
| 4.00       | 215342      | 60.59          | 73.86           | 0.67872     | 0.255512          | 0.0                     | 0.0                      |
| 4.10       | 215342      | 60.43          | 74.60           | 0.67862     | 0.255512          | 0.0                     | 0.0                      |
| 4.20       | 215342      | 60.27          | 75.33           | 0.67862     | 0.255512          | 0.0                     | 0.0                      |
| 4.30       | 215342      | 60.10          | 76.06           | 0.67852     | 0.255512          | 0.0                     | 0.0                      |
| 4.40       | 215342      | 59.93          | 76.77           | 0.67842     | 0.255512          | 0.0                     | 0.0                      |
| 4.50       | 215342      | 59.76          | 77.48           | 0.67832     | 0.255512          | 0.0                     | 0.0                      |
| 4.60       | 215342      | 59.58          | 78.18           | 0.67822     | 0.255512          | 0.0                     | 0.0                      |
| 4.70       | 215342      | 59.40          | 78.88           | 0.67812     | 0.255512          | 0.0                     | 0.0                      |
| 4.80       | 215342      | 59.21          | 79.56           | 0.67802     | 0.255512          | 0.0                     | 0.0                      |
| 4.90       | 215342      | 59.02          | 80.24           | 0.67792     | 0.255512          | 0.0                     | 0.0                      |
| 5.00       | 215342      | 58.82          | 80.91           | 0.67792     | 0.255512          | 0.0                     | 0.0                      |
| 5.10       | 215342      | 58.63          | 81.57           | 0.67782     | 0.255512          | 0.0                     | 0.0                      |



| TRAJECTORY PARAMETERS |            |               |                |             | TRAJECTORY NUMBER 5 |                       |                        |  |  |
|-----------------------|------------|---------------|----------------|-------------|---------------------|-----------------------|------------------------|--|--|
| TIME(MIN)             | RADIUS(FT) | LATITUDE(LEG) | LONGITUDE(DEC) | HEIGHT(FT)  | VELOCITY(FT/S)      | BAL.COEFF.(FT**2/SLG) | ATMOS.DENS.(SLG/FT**3) |  |  |
| 5.20                  | 21533      | 8             | 58.42          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 5.30                  | 21533      | 8             | 58.22          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 5.40                  | 21533      | 8             | 58.02          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 5.50                  | 21533      | 8             | 57.82          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 5.60                  | 21533      | 8             | 57.62          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 5.70                  | 21533      | 8             | 57.42          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 5.80                  | 21533      | 8             | 57.22          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 5.90                  | 21533      | 8             | 57.02          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 6.00                  | 21533      | 8             | 56.82          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 6.10                  | 21533      | 8             | 56.62          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 6.20                  | 21533      | 8             | 56.42          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 6.30                  | 21533      | 8             | 56.22          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 6.40                  | 21533      | 8             | 56.02          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 6.50                  | 21533      | 8             | 55.82          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 6.60                  | 21533      | 8             | 55.62          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 6.70                  | 21533      | 8             | 55.42          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 6.80                  | 21533      | 8             | 55.22          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 6.90                  | 21533      | 8             | 55.02          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 7.00                  | 21533      | 8             | 54.82          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 7.10                  | 21533      | 8             | 54.62          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 7.20                  | 21533      | 8             | 54.42          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 7.30                  | 21533      | 8             | 54.22          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 7.40                  | 21533      | 8             | 54.02          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 7.50                  | 21533      | 8             | 53.82          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 7.60                  | 21533      | 8             | 53.62          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 7.70                  | 21533      | 8             | 53.42          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 7.80                  | 21533      | 8             | 53.22          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 7.90                  | 21533      | 8             | 53.02          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 8.00                  | 21533      | 8             | 52.82          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 8.10                  | 21533      | 8             | 52.62          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 8.20                  | 21533      | 8             | 52.42          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 8.30                  | 21533      | 8             | 52.22          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 8.40                  | 21533      | 8             | 52.02          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 8.50                  | 21533      | 8             | 51.82          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 8.60                  | 21533      | 8             | 51.62          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 8.70                  | 21533      | 8             | 51.42          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 8.80                  | 21533      | 8             | 51.22          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 8.90                  | 21533      | 8             | 51.02          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 9.00                  | 21533      | 8             | 50.82          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 9.10                  | 21533      | 8             | 50.62          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 9.20                  | 21533      | 8             | 50.42          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 9.30                  | 21533      | 8             | 50.22          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 9.40                  | 21533      | 8             | 50.02          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 9.50                  | 21533      | 8             | 49.82          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 9.60                  | 21533      | 8             | 49.62          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 9.70                  | 21533      | 8             | 49.42          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 9.80                  | 21533      | 8             | 49.22          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 9.90                  | 21533      | 8             | 49.02          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 10.00                 | 21533      | 8             | 48.82          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 10.10                 | 21533      | 8             | 48.62          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 10.20                 | 21533      | 8             | 48.42          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |
| 10.30                 | 21533      | 8             | 48.22          | 0.60777E 06 | 0.25565E 05         | 0.                    | 0.                     |  |  |



# TRAJECTORY PARAMETERS • TRAJECTORY NUMBER 5

| TIME(MIN) | RADIUS(FT) | LATITUDE(DEG) | LONGITUDE(DEG) | HEIGHT(FT) | VELOCITY(FT/SEC) | BAL. CORP. (FT**2/SLG) | ATMOS. DENS. (SLG/FT**3) |
|-----------|------------|---------------|----------------|------------|------------------|------------------------|--------------------------|
| 10.40     | 0.21532    | 44.4          | 106.99         | 0.60702    | 0.255662         | 0.                     | 0.                       |
| 10.50     | 0.21532    | 44.09         | 107.32         | 0.60692    | 0.255662         | 0.                     | 0.                       |
| 10.60     | 0.21532    | 43.77         | 107.66         | 0.60682    | 0.255662         | 0.                     | 0.                       |
| 10.70     | 0.21532    | 43.45         | 107.98         | 0.60672    | 0.255662         | 0.                     | 0.                       |
| 10.80     | 0.21532    | 43.13         | 108.31         | 0.60662    | 0.255662         | 0.                     | 0.                       |
| 10.90     | 0.21532    | 42.81         | 108.63         | 0.60652    | 0.255662         | 0.                     | 0.                       |
| 11.00     | 0.21532    | 42.49         | 108.95         | 0.60642    | 0.255662         | 0.                     | 0.                       |
| 11.10     | 0.21532    | 42.17         | 109.26         | 0.60632    | 0.255662         | 0.                     | 0.                       |
| 11.20     | 0.21532    | 41.85         | 109.57         | 0.60622    | 0.255662         | 0.                     | 0.                       |
| 11.30     | 0.21532    | 41.52         | 109.88         | 0.60612    | 0.255662         | 0.                     | 0.                       |
| 11.40     | 0.21532    | 41.2          | 110.18         | 0.60602    | 0.255662         | 0.                     | 0.                       |
| 11.50     | 0.21532    | 40.87         | 110.48         | 0.60592    | 0.255662         | 0.                     | 0.                       |
| 11.60     | 0.21532    | 40.55         | 110.78         | 0.60582    | 0.255662         | 0.                     | 0.                       |
| 11.70     | 0.21532    | 40.22         | 111.08         | 0.60572    | 0.255662         | 0.                     | 0.                       |
| 11.80     | 0.21532    | 39.89         | 111.37         | 0.60562    | 0.255662         | 0.                     | 0.                       |
| 11.90     | 0.21532    | 39.56         | 111.66         | 0.60552    | 0.255662         | 0.                     | 0.                       |
| 12.00     | 0.21532    | 39.23         | 111.94         | 0.60542    | 0.255662         | 0.                     | 0.                       |
| 12.10     | 0.21532    | 38.90         | 112.22         | 0.60532    | 0.255662         | 0.                     | 0.                       |
| 12.20     | 0.21532    | 38.57         | 112.50         | 0.60522    | 0.255662         | 0.                     | 0.                       |
| 12.30     | 0.21532    | 38.23         | 112.78         | 0.60512    | 0.255662         | 0.                     | 0.                       |
| 12.40     | 0.21532    | 37.9          | 113.05         | 0.60502    | 0.255662         | 0.                     | 0.                       |
| 12.50     | 0.21532    | 37.57         | 113.32         | 0.60492    | 0.255662         | 0.                     | 0.                       |
| 12.60     | 0.21532    | 37.23         | 113.59         | 0.60482    | 0.255662         | 0.                     | 0.                       |
| 12.70     | 0.21532    | 36.90         | 113.86         | 0.60472    | 0.255662         | 0.                     | 0.                       |
| 12.80     | 0.21532    | 36.56         | 114.12         | 0.60462    | 0.255662         | 0.                     | 0.                       |
| 12.90     | 0.21532    | 36.22         | 114.38         | 0.60452    | 0.255662         | 0.                     | 0.                       |
| 13.00     | 0.21532    | 35.88         | 114.64         | 0.60442    | 0.255662         | 0.                     | 0.                       |
| 13.10     | 0.21532    | 35.55         | 114.90         | 0.60432    | 0.255662         | 0.                     | 0.                       |
| 13.20     | 0.21532    | 35.21         | 115.15         | 0.60422    | 0.255662         | 0.                     | 0.                       |
| 13.30     | 0.21532    | 34.87         | 115.40         | 0.60412    | 0.255662         | 0.                     | 0.                       |
| 13.40     | 0.21532    | 34.53         | 115.65         | 0.60402    | 0.255662         | 0.                     | 0.                       |
| 13.50     | 0.21532    | 34.19         | 115.90         | 0.60392    | 0.255662         | 0.                     | 0.                       |
| 13.60     | 0.21532    | 33.84         | 116.14         | 0.60382    | 0.255662         | 0.                     | 0.                       |
| 13.70     | 0.21532    | 33.50         | 116.39         | 0.60372    | 0.255662         | 0.                     | 0.                       |
| 13.80     | 0.21532    | 33.16         | 116.63         | 0.60362    | 0.255662         | 0.                     | 0.                       |
| 13.90     | 0.21532    | 32.82         | 116.86         | 0.60352    | 0.255662         | 0.                     | 0.                       |
| 14.00     | 0.21532    | 32.47         | 117.10         | 0.60342    | 0.255662         | 0.                     | 0.                       |
| 14.10     | 0.21532    | 32.13         | 117.34         | 0.60332    | 0.255662         | 0.                     | 0.                       |
| 14.20     | 0.21532    | 31.78         | 117.57         | 0.60322    | 0.255662         | 0.                     | 0.                       |
| 14.30     | 0.21532    | 31.44         | 117.80         | 0.60312    | 0.255662         | 0.                     | 0.                       |
| 14.40     | 0.21532    | 31.09         | 118.03         | 0.60302    | 0.255662         | 0.                     | 0.                       |
| 14.50     | 0.21532    | 30.75         | 118.25         | 0.60292    | 0.255662         | 0.                     | 0.                       |
| 14.60     | 0.21532    | 30.4          | 118.48         | 0.60282    | 0.255662         | 0.                     | 0.                       |
| 14.70     | 0.21532    | 30.05         | 118.70         | 0.60272    | 0.255662         | 0.                     | 0.                       |
| 14.80     | 0.21532    | 29.7          | 118.92         | 0.60262    | 0.255662         | 0.                     | 0.                       |
| 14.90     | 0.21532    | 29.36         | 119.14         | 0.60252    | 0.255662         | 0.                     | 0.                       |
| 15.00     | 0.21532    | 29.01         | 119.36         | 0.60242    | 0.255662         | 0.                     | 0.                       |
| 15.10     | 0.21532    | 28.66         | 119.58         | 0.60232    | 0.255662         | 0.                     | 0.                       |
| 15.20     | 0.21532    | 28.31         | 119.79         | 0.60222    | 0.255662         | 0.                     | 0.                       |
| 15.30     | 0.21532    | 27.96         | 120.01         | 0.60212    | 0.255662         | 0.                     | 0.                       |
| 15.40     | 0.21532    | 27.61         | 120.22         | 0.60202    | 0.255662         | 0.                     | 0.                       |
| 15.50     | 0.21532    | 27.26         | 120.43         | 0.60192    | 0.255662         | 0.                     | 0.                       |

| TRAJECTORY PARAMETERS |             |                |                 |             | TRAJECTORY NUMBER |    | BAL. COEFF. (FT**2/SLG) |    | ATMOS. DENS. (SLG/FT**3) |    |
|-----------------------|-------------|----------------|-----------------|-------------|-------------------|----|-------------------------|----|--------------------------|----|
| TIME (IN)             | RADIUS (FT) | LATITUDE (DEG) | LONGITUDE (DEG) | HEIGHT (FT) | VELOCITY (FT/S)   |    |                         |    |                          |    |
| 15.60                 | 2132E 8     | 26.9           | 120.64          | 0.60587E 06 | 0.255677E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 15.70                 | 21331E 08   | 26.95          | 120.84          | 0.60585E 06 | 0.255677E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 15.80                 | 21331E 8    | 26.2           | 121.05          | 0.60582E 06 | 0.255677E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 15.90                 | 21331E 08   | 25.85          | 121.25          | 0.60580E 06 | 0.255678E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 16.00                 | 21331E 8    | 25.5           | 121.46          | 0.60577E 06 | 0.255678E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 16.10                 | 21331E 08   | 25.14          | 121.66          | 0.60575E 06 | 0.255678E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 16.20                 | 21331E 8    | 24.79          | 121.86          | 0.60572E 06 | 0.255678E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 16.30                 | 21331E 08   | 24.44          | 122.06          | 0.60570E 06 | 0.255679E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 16.40                 | 21331E 8    | 24.08          | 122.26          | 0.60567E 06 | 0.255679E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 16.50                 | 21331E 08   | 23.73          | 122.45          | 0.60565E 06 | 0.255679E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 16.60                 | 21331E 8    | 23.37          | 122.65          | 0.60562E 06 | 0.255680E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 16.70                 | 21331E 08   | 23.02          | 122.84          | 0.60560E 06 | 0.255680E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 16.80                 | 21331E 8    | 22.66          | 123.04          | 0.60557E 06 | 0.255680E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 16.90                 | 21331E 08   | 22.31          | 123.23          | 0.60555E 06 | 0.255681E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 17.00                 | 21331E 8    | 21.95          | 123.42          | 0.60552E 06 | 0.255681E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 17.10                 | 21331E 08   | 21.60          | 123.61          | 0.60549E 06 | 0.255681E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 17.20                 | 21331E 8    | 21.24          | 123.80          | 0.60547E 06 | 0.255681E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 17.30                 | 21331E 08   | 20.88          | 123.98          | 0.60544E 06 | 0.255682E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 17.40                 | 21331E 8    | 20.52          | 124.17          | 0.60542E 06 | 0.255682E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 17.50                 | 21331E 08   | 20.17          | 124.36          | 0.60539E 06 | 0.255682E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 17.60                 | 21331E 8    | 19.81          | 124.54          | 0.60536E 06 | 0.255683E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 17.70                 | 21331E 08   | 19.45          | 124.73          | 0.60534E 06 | 0.255683E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 17.80                 | 21331E 8    | 19.1           | 124.91          | 0.60531E 06 | 0.255683E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 17.90                 | 21331E 08   | 18.74          | 125.09          | 0.60529E 06 | 0.255684E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 18.00                 | 21331E 8    | 18.38          | 125.27          | 0.60526E 06 | 0.255684E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 18.10                 | 21331E 08   | 18.02          | 125.45          | 0.60523E 06 | 0.255684E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 18.20                 | 21331E 8    | 17.66          | 125.63          | 0.60521E 06 | 0.255685E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 18.30                 | 21331E 08   | 17.30          | 125.81          | 0.60518E 06 | 0.255685E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 18.40                 | 21331E 8    | 16.94          | 125.99          | 0.60515E 06 | 0.255685E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 18.50                 | 21331E 08   | 16.59          | 126.17          | 0.60513E 06 | 0.255686E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 18.60                 | 21331E 8    | 16.23          | 126.34          | 0.60510E 06 | 0.255686E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 18.70                 | 21331E 08   | 15.87          | 126.52          | 0.60507E 06 | 0.255686E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 18.80                 | 21331E 8    | 15.51          | 126.69          | 0.60505E 06 | 0.255686E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 18.90                 | 21331E 08   | 15.15          | 126.87          | 0.60502E 06 | 0.255687E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 19.00                 | 21331E 8    | 14.79          | 127.04          | 0.60499E 06 | 0.255687E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 19.10                 | 21331E 08   | 14.42          | 127.21          | 0.60497E 06 | 0.255687E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 19.20                 | 21331E 8    | 14.06          | 127.38          | 0.60494E 06 | 0.255688E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 19.30                 | 21331E 08   | 13.70          | 127.56          | 0.60491E 06 | 0.255688E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 19.40                 | 21331E 8    | 13.34          | 127.73          | 0.60488E 06 | 0.255688E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 19.50                 | 21330E 08   | 12.98          | 127.90          | 0.60486E 06 | 0.255689E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 19.60                 | 2133E 8     | 12.62          | 128.07          | 0.60483E 06 | 0.255689E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 19.70                 | 21330E 08   | 12.26          | 128.24          | 0.60480E 06 | 0.255689E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 19.80                 | 2133E 8     | 11.9           | 128.41          | 0.60478E 06 | 0.255690E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 19.90                 | 21330E 08   | 11.54          | 128.57          | 0.60475E 06 | 0.255690E 05      | 0. | 0.                      | 0. | 0.                       | 0. |
| 20.00                 | 2133E 8     | 11.17          | 128.74          | 0.60472E 06 | 0.255690E 05      | 0. | 0.                      | 0. | 0.                       | 0. |

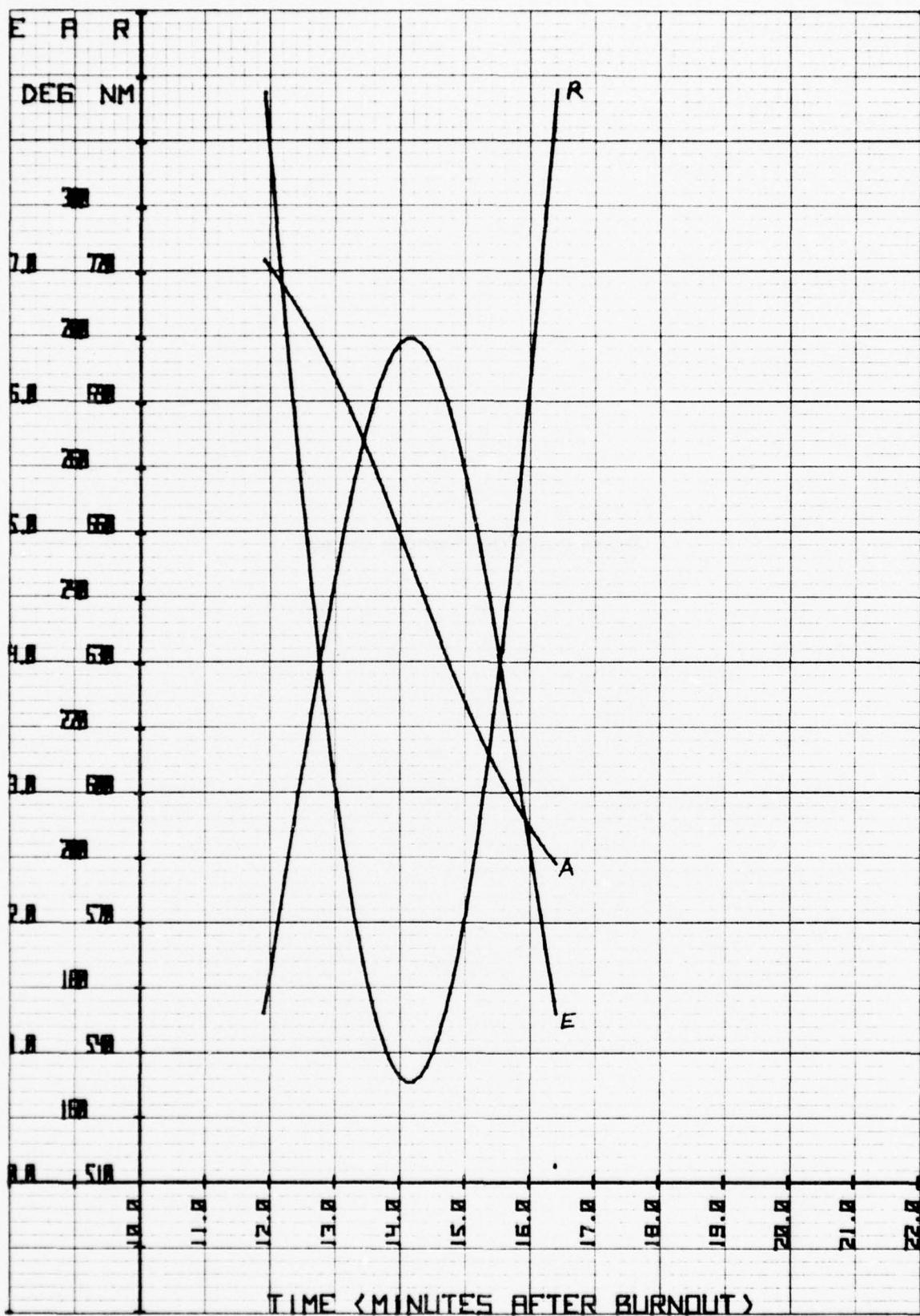
# RADAR PARAMETERS • TRAJECTORY NUMBER 5 RADAR SITE 1 35.900 DEG. LAT. 233.333 DEG. LONG.

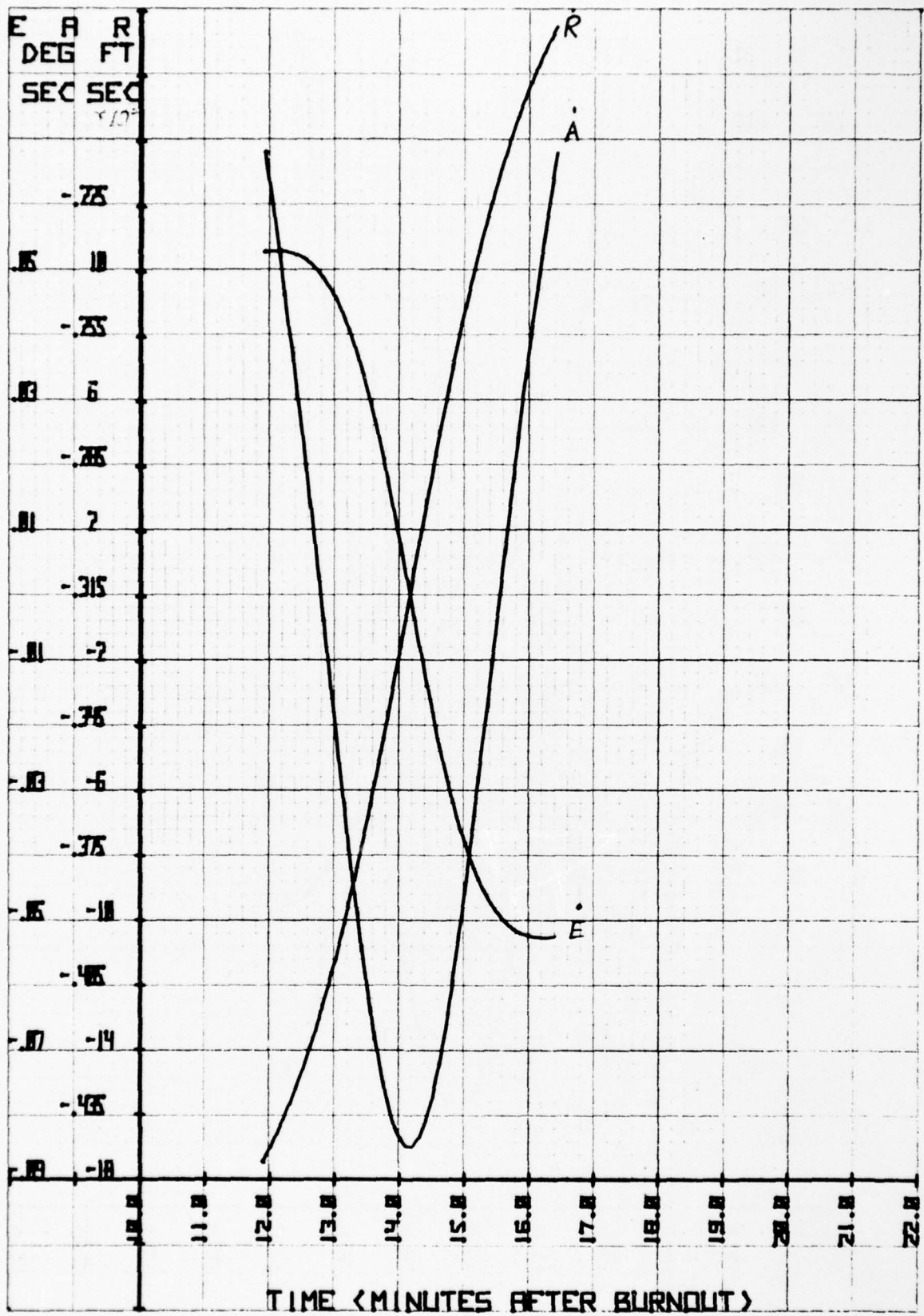
| TIME<br>(MIN) | SL RANGE<br>(NM) | SL RANGE-RATE<br>(FT/SA) | ELEVATION<br>(DEG) | EL RATE<br>(DEG/S) | AZIMUTH<br>(DEG) | AZ RATE<br>(DEG/S) | RADIUS<br>(ERY) | INERTIAL PHI<br>(DEG) |
|---------------|------------------|--------------------------|--------------------|--------------------|------------------|--------------------|-----------------|-----------------------|
| 11.90         | 0.761682         | 0.174577E 05             | 1.29               | 0.5262E-04         | 290.65           | -0.2130E 00        | 1.029           | 51.66                 |
| 12.00         | 0.744098         | -0.170688E 05            | 1.60               | 0.5262E-04         | 290.34           | -0.2231E 00        | 1.029           | 51.94                 |
| 12.10         | 0.727363         | -0.166588E 05            | 1.92               | 0.5262E-04         | 289.97           | -0.2332E 00        | 1.029           | 52.22                 |
| 12.20         | 0.711174E 02     | -0.162047E 05            | 2.24               | 0.5262E-04         | 289.54           | -0.2433E 00        | 1.029           | 52.50                 |
| 12.30         | 0.695416E 03     | -0.157257E 05            | 2.55               | 0.5255E-04         | 289.09           | -0.2534E 00        | 1.029           | 52.78                 |
| 12.40         | 0.680188E 03     | -0.152128E 05            | 2.87               | 0.5241E-04         | 288.47           | -0.2635E 00        | 1.029           | 53.05                 |
| 12.50         | 0.665433E 03     | -0.146600E 05            | 3.18               | 0.5191E-04         | 287.82           | -0.2736E 00        | 1.029           | 53.32                 |
| 12.60         | 0.651242E 03     | -0.140762E 05            | 3.49               | 0.5072E-04         | 287.10           | -0.2837E 00        | 1.029           | 53.59                 |
| 12.70         | 0.637631E 03     | -0.134588E 05            | 3.79               | 0.5032E-04         | 279.31           | -0.3038E 00        | 1.029           | 53.86                 |
| 12.80         | 0.624623E 03     | -0.127951E 05            | 4.09               | 0.4821E-04         | 277.43           | -0.3139E 00        | 1.029           | 54.12                 |
| 12.90         | 0.612341E 03     | -0.120762E 05            | 4.37               | 0.4732E-04         | 275.48           | -0.3232E 00        | 1.029           | 54.38                 |
| 13.00         | 0.600861E 03     | -0.113242E 05            | 4.65               | 0.4551E-04         | 273.44           | -0.3333E 00        | 1.029           | 54.64                 |
| 13.10         | 0.590055E 03     | -0.105225E 05            | 4.92               | 0.4352E-04         | 271.33           | -0.3434E 00        | 1.029           | 54.90                 |
| 13.20         | 0.580063E 03     | -0.096892E 05            | 5.17               | 0.4031E-04         | 269.14           | -0.3535E 00        | 1.029           | 55.15                 |
| 13.30         | 0.570966E 03     | -0.088074E 05            | 5.41               | 0.3792E-04         | 266.87           | -0.3636E 00        | 1.029           | 55.40                 |
| 13.40         | 0.562722E 03     | -0.078333E 05            | 5.63               | 0.3432E-04         | 264.54           | -0.3737E 00        | 1.029           | 55.65                 |
| 13.50         | 0.554223E 03     | -0.068028E 05            | 5.82               | 0.3062E-04         | 262.13           | -0.3838E 00        | 1.029           | 55.90                 |
| 13.60         | 0.546083E 03     | -0.057203E 05            | 6.00               | 0.2631E-04         | 259.66           | -0.3939E 00        | 1.029           | 56.14                 |
| 13.70         | 0.537452E 03     | -0.045888E 05            | 6.15               | 0.2232E-04         | 257.14           | -0.4040E 00        | 1.029           | 56.39                 |
| 13.80         | 0.529422E 03     | -0.034285E 05            | 6.27               | 0.1782E-04         | 254.57           | -0.4141E 00        | 1.029           | 56.63                 |
| 13.90         | 0.521616E 03     | -0.022452E 05            | 6.36               | 0.1282E-04         | 251.96           | -0.4242E 00        | 1.029           | 56.88                 |
| 14.00         | 0.514028E 03     | -0.010463E 05            | 6.42               | 0.0732E-04         | 249.32           | -0.4343E 00        | 1.029           | 57.10                 |
| 14.10         | 0.506933E 03     | 0.003693E 03             | 6.45               | 0.0232E-04         | 246.68           | -0.4444E 00        | 1.029           | 57.33                 |
| 14.20         | 0.500000E 03     | 0.007574E 03             | 6.45               | 0.2802E-04         | 244.02           | -0.4545E 00        | 1.029           | 57.57                 |
| 14.30         | 0.493253E 03     | 0.008422E 04             | 6.42               | -0.0802E-04        | 241.37           | -0.4646E 00        | 1.029           | 57.80                 |
| 14.40         | 0.486291E 03     | 0.007832E 04             | 6.35               | -0.1392E-04        | 238.74           | -0.4747E 00        | 1.029           | 58.03                 |
| 14.50         | 0.479573E 03     | 0.006493E 04             | 6.26               | -0.1832E-04        | 236.13           | -0.4848E 00        | 1.029           | 58.25                 |
| 14.60         | 0.473012E 03     | 0.005232E 04             | 6.14               | -0.2202E-04        | 233.56           | -0.4949E 00        | 1.029           | 58.48                 |
| 14.70         | 0.466622E 03     | 0.003954E 04             | 5.99               | -0.2782E-04        | 231.04           | -0.5050E 00        | 1.029           | 58.70                 |
| 14.80         | 0.460413E 03     | 0.002516E 04             | 5.81               | -0.3102E-04        | 228.57           | -0.5151E 00        | 1.029           | 58.92                 |
| 14.90         | 0.454299E 03     | 0.001266E 04             | 5.61               | -0.3462E-04        | 226.17           | -0.5252E 00        | 1.029           | 59.14                 |
| 15.00         | 0.448255E 03     | 0.000340E 04             | 5.39               | -0.3812E-04        | 223.83           | -0.5353E 00        | 1.029           | 59.36                 |
| 15.10         | 0.442272E 03     | 0.000137E 04             | 5.16               | -0.4102E-04        | 221.57           | -0.5454E 00        | 1.029           | 59.58                 |
| 15.20         | 0.436413E 03     | 0.000555E 05             | 4.90               | -0.4352E-04        | 219.39           | -0.5555E 00        | 1.029           | 59.79                 |
| 15.30         | 0.430672E 03     | 0.001343E 05             | 4.64               | -0.4552E-04        | 217.27           | -0.5656E 00        | 1.029           | 60.01                 |
| 15.40         | 0.425053E 03     | 0.002093E 05             | 4.36               | -0.4702E-04        | 215.24           | -0.5757E 00        | 1.029           | 60.22                 |
| 15.50         | 0.419552E 03     | 0.002793E 05             | 4.07               | -0.4822E-04        | 213.28           | -0.5858E 00        | 1.029           | 60.43                 |
| 15.60         | 0.414163E 03     | 0.003463E 05             | 3.77               | -0.5012E-04        | 211.41           | -0.5959E 00        | 1.029           | 60.64                 |
| 15.70         | 0.408883E 03     | 0.004086E 05             | 3.47               | -0.5102E-04        | 209.62           | -0.6060E 00        | 1.029           | 60.84                 |
| 15.80         | 0.403713E 03     | 0.004670E 05             | 3.16               | -0.5132E-04        | 207.90           | -0.6161E 00        | 1.029           | 61.05                 |
| 15.90         | 0.408573E 03     | 0.005216E 05             | 2.85               | -0.5232E-04        | 206.25           | -0.6262E 00        | 1.029           | 61.25                 |
| 16.00         | 0.403584E 03     | 0.005723E 05             | 2.53               | -0.5282E-04        | 204.68           | -0.6363E 00        | 1.029           | 61.46                 |
| 16.10         | 0.408713E 03     | 0.006204E 05             | 2.22               | -0.5262E-04        | 203.18           | -0.6464E 00        | 1.029           | 61.66                 |
| 16.20         | 0.414013E 03     | 0.006648E 05             | 1.90               | -0.5242E-04        | 201.74           | -0.6565E 00        | 1.029           | 61.86                 |
| 16.30         | 0.419453E 03     | 0.007063E 05             | 1.58               | -0.5262E-04        | 200.37           | -0.6666E 00        | 1.029           | 62.06                 |
| 16.40         | 0.425013E 03     | 0.007450E 05             | 1.27               | -0.5262E-04        | 199.07           | -0.6767E 00        | 1.029           | 62.26                 |

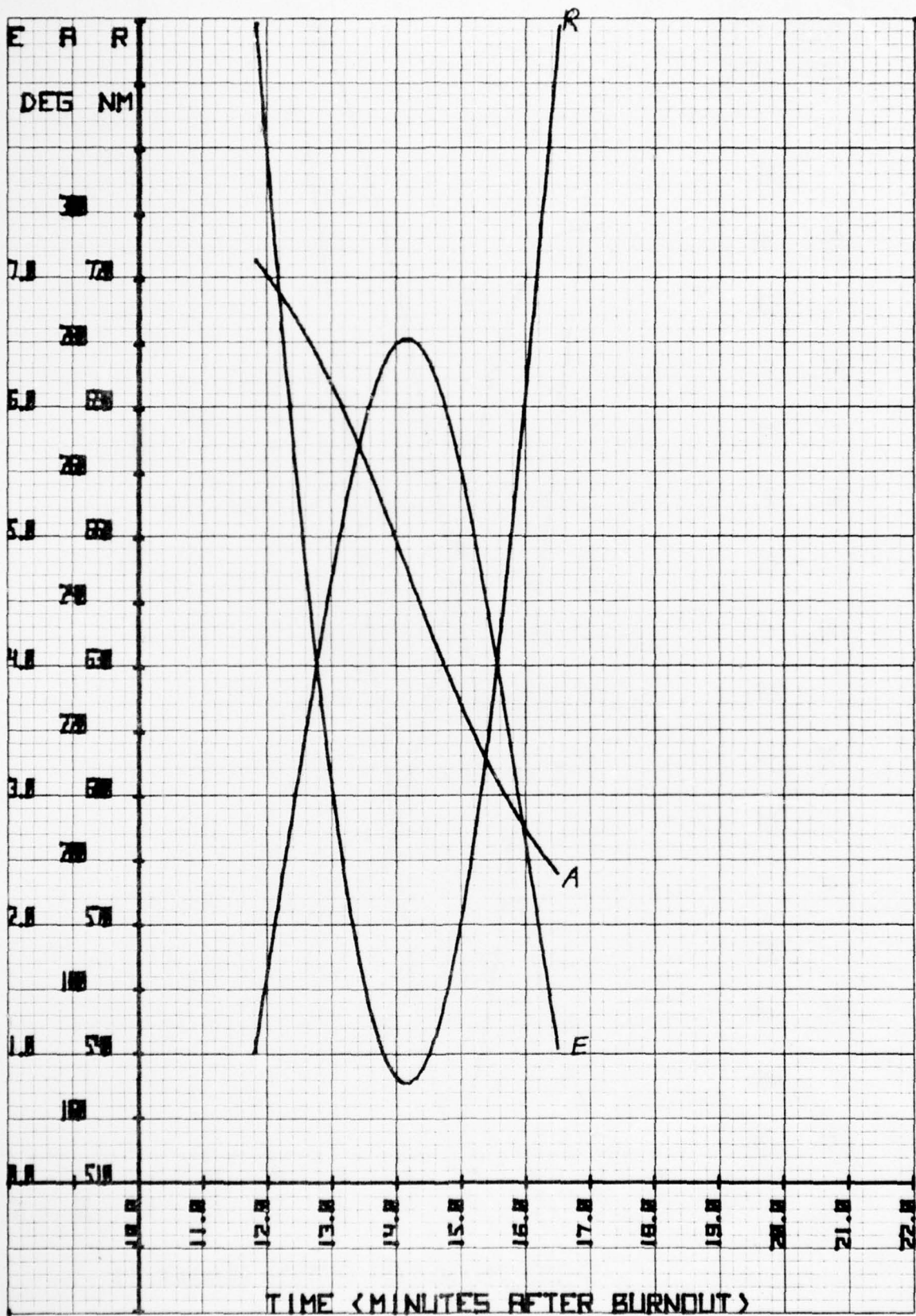
Plots from the Sample Output

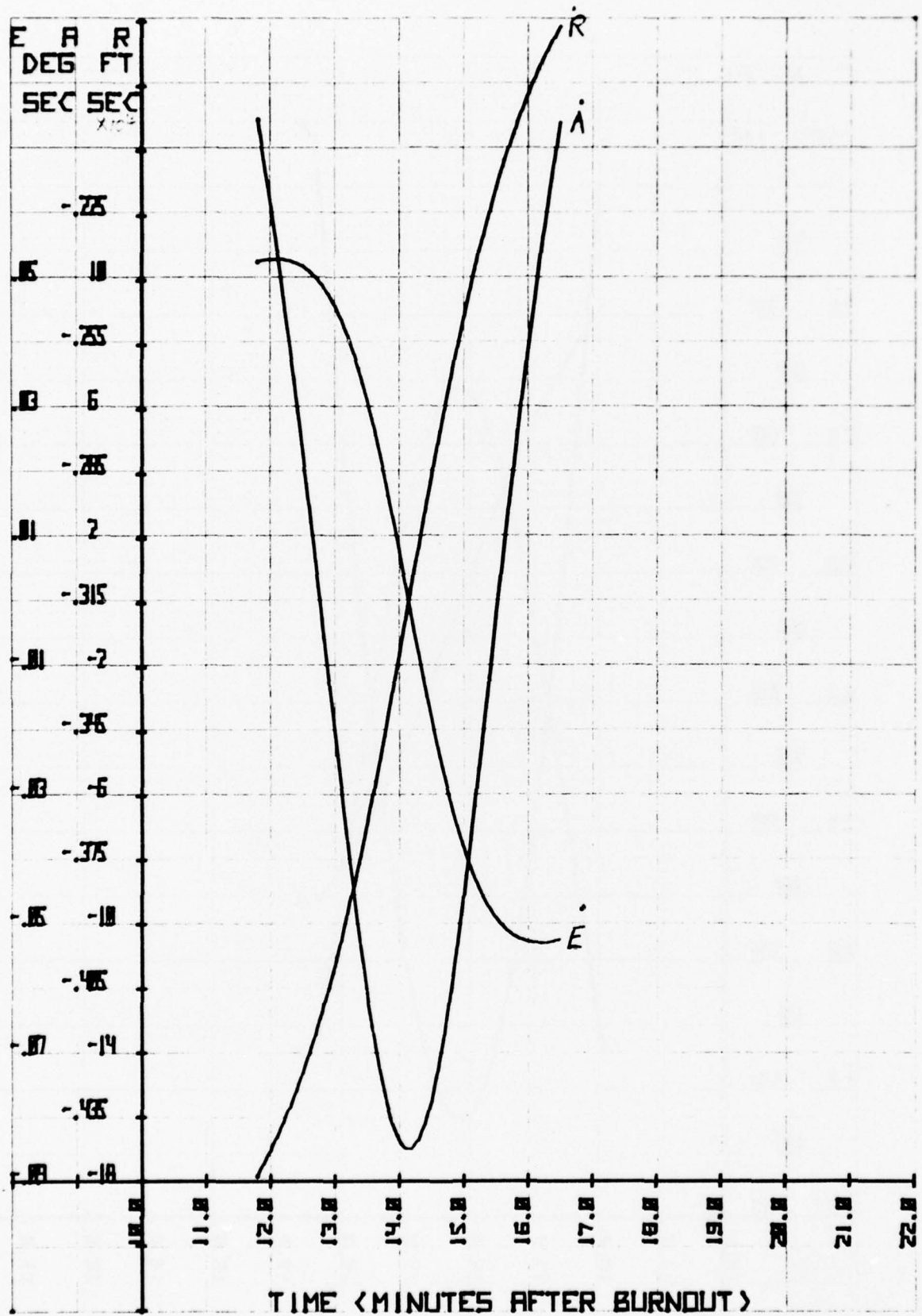


Trajectory 1

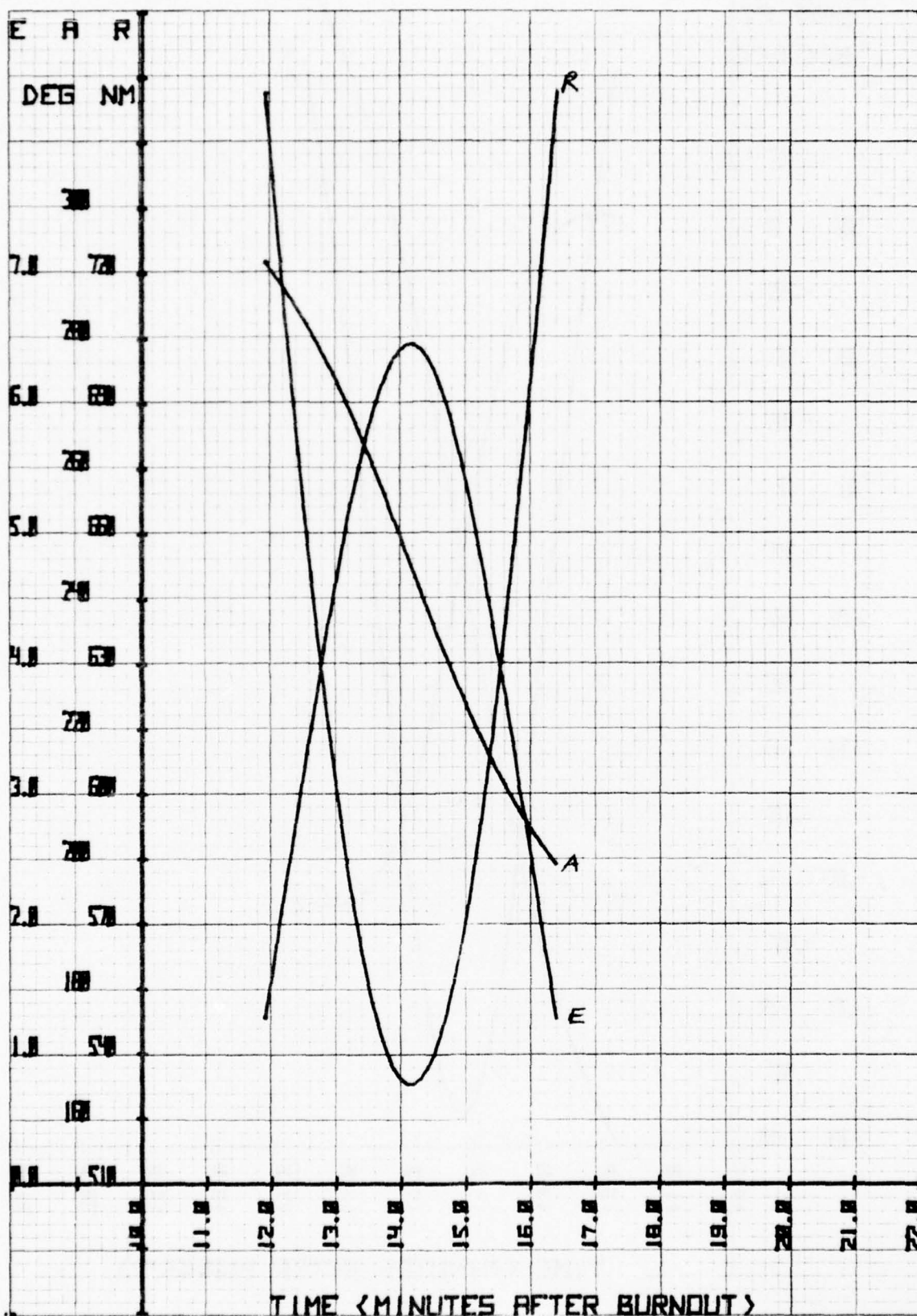


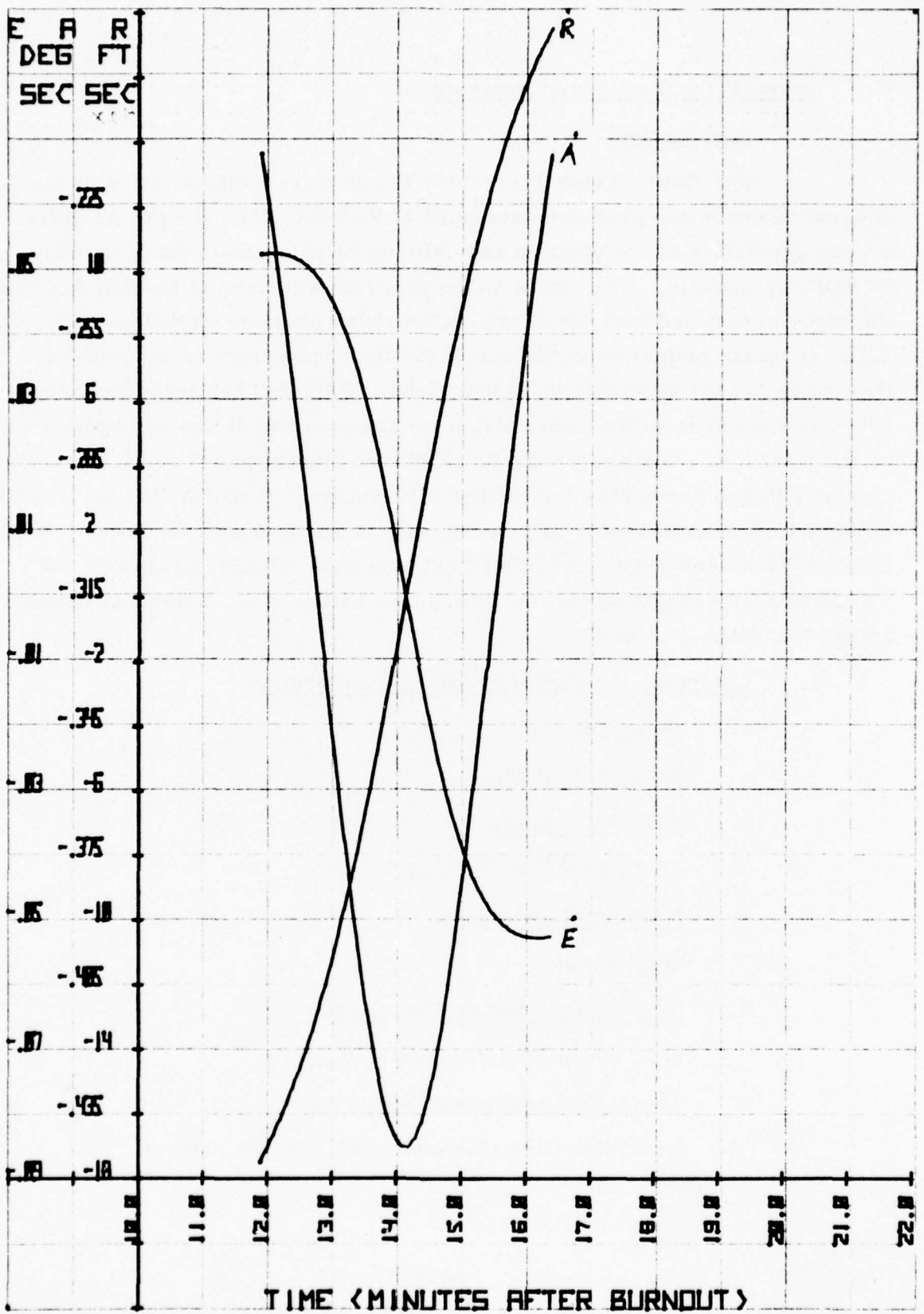












## C. Cobra Talon Trajectory Program

### 1. Introduction

The Cobra Talon Trajectory Program is a modification of the general perturbation program developed at RADC by Mr. George A. Ellis for the prediction of the position and velocity of an earth-orbiting satellite or ballistic missile. The Cobra Talon program was used to furnish data for the study associated with the Cobra Talon radar project. It differs from Mr. Ellis' program primarily in the use of the first trajectory as the nominal trajectory for the perturbation calculations. PRC/ISC has made the necessary modifications to the Cobra Talon program so that it can be implemented on the interactive system for the RADC Radar Simulator. The reader is referred to two documents for further information: "COBRA TALON STUDY COMPUTER PROGRAMS," by John C. Cleary and Leonard C. Gratch, RADC/OC-TM-71-4, and "SIMULATION PROGRAM FOR THREE DEGREES OF FREEDOM TRAJECTORIES," by George A. Ellis, et al, Technical Memorandum No. EMA-TM-66-5.

### 2. Computer Program Operating Environment

#### a. Computer

Honeywell 6000.

#### b. Source Language

FORTRAN Y under GCOS.

#### c. Memory Requirement

16 K words

#### d. Typical Processing Time Required

0.25 hours (900 seconds)

#### e. Peripheral Equipment Requirement

Four disc files (file codes: 02, 03, 04, 07).

f. Non-system Subroutines Required

|        |   |
|--------|---|
| ATMOSP | Atmospheric model.  |
| CONVER | Conversion of trajectory to radar coordinates.                          |
| EQTNX  | Computation of acceleration components.                                 |
| ICERBM | Performs initialization for trajectory computations.                    |
| INPUTT | Input subroutine.   |
| OUTPUT | Stores trajectory data in an array for outputting.                      |
| PRINT2 | Prints out trajectory and radar data.                                   |
| RKG    | Performs 4th order Runge-Kutta-Gill integration of equations of motion. |
| SAVE   | Outputs trajectory and radar data onto files.                           |

3. Inputs

The following is the set of input parameters required for the Cobra Talon Trajectory Program:

NAMelist IN1

TM - Maximum forward trajectory run time (minutes)

TMI - Cut-off time for backwards trajectory (minutes)

NAMelist IN2

CA - Surface range - dummy variable (degrees)

BETA - Missile heading angle measured clockwise from north (degrees).

GAM - Missile re-entry angle relative to vertical (degrees).

HX - Height of missile at burnout (feet), referenced to earth's surface.

NAMelist IN3

KZ - Program control variable.

=0 differences are calculated relative to third trajectory.



=1 differences are calculated relative to first trajectory.

#### NAMELIST IN4

ELIM - Maximum co-latitude of elevation angle for which radar coverage parameters are determined (degrees).

#### NAMELIST IN5

VO - Initial velocity of missile (ft./min.).

INERTL - Initial velocity option variable.

=1, initial velocity is inertial velocity (SATELLITE orbit).

=0, initial velocity is burnout velocity (MISSILE trajectories)

#### NAMELIST IN6

ZK -  $ZK = g/2Bc$  ( $Bc$ =ballistic coefficient in lbs./ft.<sup>2</sup> and  $g=32.2$  ft./sec.<sup>2</sup>), measured in ft.<sup>2</sup>/slugs.

KAT - Atmospheric model option variable.

=0, sets the atmospheric density to zero.

=1, use the atmospheric model.

#### NAMELIST IN7

A - Out of trajectory plane perturbation, + ejected to the left of nominal trajectory (ft./sec.)

B - In plane perturbation, + ejected backward from nominal trajectory (ft./sec.).

C - In plane perturbation, + ejected upwards from nominal trajectory (ft./sec.).

MM - MM=3 gives nominal trajectory, MM greater than 3 gives MM minus 3 perturbed trajectories.

#### NAMELIST IN8

SC1 - Radar latitude (positive north and negative south of equator) (degrees).

SC2 - Radar longitude west of Greenwich (degrees).

AH - Altitude above sea level of radar (feet).

#### NAMELIST IN9

GLAM - Launch longitude east of Greenwich (degrees).

THE - Launch latitude (positive north and negative south of equator in degrees).

GLAMI - Impact longitude east of Greenwich (degrees).

THEI - Impact latitude (positive north and negative south of equator, in degrees).

#### 4. Output

Output from the Cobra Talon Trajectory Program first consists of a printout of the input data for the computer run. Secondly, the output consists of a printout of data generated for the first trajectory. This data is printed out as a list of trajectory parameters (e.g., radius, latitude, longitude, etc.) versus incremental trajectory time points (generally separated by 0.1 min. increments) from start time to end time. If the target, whose trajectory has been generated, is detected by a radar site, a listing of the radar parameters computed for the site, from initial time of detection to time of leaving coverage, is also produced. A description of the complete set of output quantities for the first trajectory follows:

| <u>Output Parameter</u> | <u>Units</u> | <u>Description</u>  |
|-------------------------|--------------|---|
| Time                    | Min.         | The time from burnout of the missile along its trajectory or time from the initiation of the satellite orbit, if that is appropriate. |
| Radius                  | Ft.          | Earth-centered radius of the trajectory or the distance of the missile or satellite from the earth center at the time point above.    |
| Latitude                | Deg.         | Position in latitude of the missile/satellite in its trajectory at the above time point.  |
| Longitude               | Deg.         | Position in longitude of the missile/satellite, east of Greenwich.  |
| Height                  | Ft.          | Altitude above sea level of the missile.  |
| Velocity                | Ft./Sec.     | Inertial velocity of the missile/satellite along its trajectory.  |

| <u>Output Parameter</u> | <u>Units</u>           | <u>Description</u>                              |
|-------------------------|------------------------|---|
| R(Sea Level)            | Ft.                    | Radius of spherical earth model.                |
| Density                 | Slugs/Ft. <sup>3</sup> | Atmospheric density.                            |
| R-Dot                   | Ft./Sec.               | Geocentric radial component of velocity.        |
| Lat. -Dot               | Deg./Sec.              | Geocentric latitude component of velocity.      |
| Long. -Dot              | Deg./Sec.              | Geocentric longitude component of velocity.     |
| R-Dot Dot               | Ft./Sec. <sup>2</sup>  | Geocentric radial component of acceleration.    |
| Lat. -Dot Dot           | Deg./Sec. <sup>2</sup> | Geocentric latitude component of acceleration.  |
| Long. -Dot Dot          | Deg./Sec. <sup>2</sup> | Geocentric longitude component of acceleration. |

If the target of the first trajectory is detected by radar, the trajectory in terms of radar coordinates is printed out as follows:

|                |                        |   |
|----------------|------------------------|---|
| Time           | Min.                   | Same as for Time described above.                                   |
| Slant Range    | Ft.                    | Radar slant range to the missile/satellite for the time point.      |
| Sl Range Rate  | Ft./Sec.               | Radar slant range rate.   |
| Sl Range R Dot | Ft./Sec. <sup>2</sup>  | Radar slant range acceleration.                                     |
| Azimuth        | Deg.                   | Radar azimuth look-angle to missile, measured clockwise from north. |
| Az Rate        | Deg./Sec.              | Radar azimuth angle rate.   |
| Az R Dot       | Deg./Sec. <sup>2</sup> | Radar azimuth angle acceleration.                                   |
| Elevation      | Deg.                   | Radar elevation look-angle to missile.                              |
| El Rate        | Deg./Sec.              | Radar elevation angle rate.   |
| El R Dot       | Deg./Sec. <sup>2</sup> | Radar elevation angle acceleration.                                 |
| Reentry Angle  | Deg.                   | Missile re-entry angle.   |
| Heading        | Deg.                   | Missile heading angle.  |

If more than one trajectory is generated in the computer run, the above set of trajectory data will be computed for the second, third, etc., trajectories also. Radar parameters for the targets corresponding to the trajectories will also be calculated, if the targets are detected.

Following the last set of trajectory and radar data, radar parameter differences may be calculated and printed out. These differences will be produced for each perturbed trajectory when MM is greater than or equal to 4. The parameter differences represent the values obtained by subtracting the radar parameters for the perturbed trajectories from the corresponding parameters for the nominal trajectory (trajectory #1 or #3). Below is a list of the output quantities comprising the radar parameter differences:

| <u>Output Parameter</u>                  | <u>Units</u>           | <u>Description</u>   |
|--|------------------------|--|
| Time                                     | Min.                   | Same as for Time described previously.   |
| Slant Range ( $\Delta R$ )               | Ft.                    | Difference in radar slant range (nominal trajectory slant range - perturbed trajectory slant range). |
| Sl Range Rate ( $\Delta \dot{R}$ )       | Ft./Sec.               | Difference in radar slant range rate.  |
| Sl Range Rate Dot ( $\Delta \ddot{R}$ )  | Ft./Sec. <sup>2</sup>  | Difference in radar slant range acceleration.  |
| Azimuth ( $\Delta A$ )                   | Deg.                   | Difference in radar azimuth look-angle to missile.   |
| Azimuth Rate ( $\Delta \dot{A}$ )        | Deg./Sec.              | Difference in radar azimuth angle rate.  |
| Azimuth Rate Dot ( $\Delta \ddot{A}$ )   | Deg./Sec. <sup>2</sup> | Difference in radar azimuth acceleration.  |
| Elevation ( $\Delta E$ )                 | Deg.                   | Difference in radar elevation look-angle to missile.   |
| Elevation Rate ( $\Delta \dot{E}$ )      | Deg./Sec.              | Difference in radar elevation angle rate.  |
| Elevation Rate Dot ( $\Delta \ddot{E}$ ) | Deg./Sec. <sup>2</sup> | Difference in radar elevation angle acceleration.  |
| Angular Separation in Radar Beam         | Deg.                   | Total angular separation in the radar beam.  |



The reader is referred to the sample output for an illustration of the printout format. The set of trajectory and radar parameters for the first trajectory only is included there, as is the set of radar parameter differences for the first perturbed trajectory only.

5. Sample Job Stream

The sample job stream on the following page is set up for producing plots of radar data from the first trajectory. This data is placed on file STORE1 and would be punched out onto cards for plotting by means of the Hewlett-Packard 9820A calculator/plotter if plots were desired. If plots are not wanted, line 80 of the job stream could be replaced by 0080\$; DISC: 02, X1R, 10L.

```

0010$:IDENT:CLEARY,CONTI      ,65121104RADC
0020$:USERID:CLEARY$THREE
0030$:LOAD
0040$:OPTION:F3RTRAN
0050$:SELECT:CLEARY/0TRAJT
0060$:EXECUTE
0070$:LIMITS:40,16K,,15000
0080$:PRMFL:02,R/W,L,CLEARY/STORE1
0090$:DISC:03,X2R,50L
0100$:DISC:04,X3R,10L
0110$:DISC:07,X4R,10L
0120$:DATA:05
0130 $INI
0140  TM=44.0D0,
0150  THI = 0.0D0,
0160 $END
0170 $INI2
0180  CA=91.5651D0,BETA=273.0D0,
0190  GAM=55.0D0,HX=4.0D5,
0200 $END
0210 $INI3
0220  KZ=1,
0230 $END
0240 $INI4
0250  ELIM = 39.5D0,
0260 $END
0270 $INI5
0280  V0=1.056D6,
0290  INERTL=0,
0300 $END
0310 $INI6
0320  ZK=0.321D-1,KAT=1,
0330 $END
0340 $INI7
0350  A=7*0.0D0,5.0D0,2*3.533D0,
0360  B=4*0.0D0,5.0D0,3.533D0,-3.533D0,0.0D0,3.533D0,-3.533D0,
0370  C=3*0.0D0,5.0D0,0.0D0,2*3.533D0,3*0.0D0,
0380  MM=3,
0390 $END
0400 $INI8
0410  SC1=13.2D0,SC2=0.53333334D0,
0420  AH = 0.0D0,
0430 $END
0440 $INI9
0450  GLAM=27.0D0,THE=42.5D0,
0460  GLAM1=60.0D0,    THE1=-40.0D0,
0470 $END
0480$:ENDJOB
0490***EOF

```

Sample Job Stream for the Cobra Talon Trajectory Program

| RADC 635/645 BATCH JOB  |       |  |              |        |
|---|-------|--|--------------|--------|
| SNUM NUMBER   |       | DATE   |              | TIME   |
|   |       | 1/7/76   |              | 1000   |
| PROGRAMMER  |       | TELEPHONE  |              |        |
| Conti   |       | 339-1360   |              |        |
| RADC ENGINEER   |       | TELEPHONE  |              | SYMBOL |
| Cleary  |       | 3573   |              | OCSA   |
| TAPES ASSIGNED  |       |  |              |        |
| REEL NO   | WRITE | READ   | DEN          | TITLE  |
| None  |       |  |              |        |
|   |       |  |              |        |
|   |       |  |              |        |
|   |       |  |              |        |
|   |       |  |              |        |
|   |       |  |              |        |
|   |       |  |              |        |
|   |       |  |              |        |
|   |       |  |              |        |
| PERIPHERALS ASSIGNED <input checked="" type="checkbox"/> READER <input checked="" type="checkbox"/> PRINTER <input type="checkbox"/> PUNCH<br><input checked="" type="checkbox"/> DISC # OF LINKS 80 <input type="checkbox"/> DRUM # OF LINKS |       |  |              |        |
| CORE SIZE 16K   |       | ACTIVITIES 1   |              |        |
| PROCESSOR TIME 0.25   |       | ESTIMATED LINES OF PRINT 10,000                                  |              |        |
| TOTAL RUN TIME 0.50   |       |  |              |        |
| DECKS EXPECTED  |       |  |              |        |
| NO. OF BINARY DECKS   |       | NO. OF COMDECKS  |              |        |
| None  |       |  |              |        |
| BMC   |       | TAPE <input type="checkbox"/> DUMP <input type="checkbox"/> COPY |              |        |
| FROM:   | TO:   | MODE   | NO. OF FILES |        |
|   |       | <input type="checkbox"/> BCD                                     |              |        |
|   |       | <input type="checkbox"/> BINARY                                  |              |        |
| SPECIAL OPERATOR INSTRUCTIONS   |       |  |              |        |
|   |       |  |              |        |
|   |       |  |              |        |
|   |       |  |              |        |
|   |       |  |              |        |
|   |       |  |              |        |
| (Use reverse side if required)  |       |  |              |        |

RADC FORM 0-56 APR 69 PREVIOUS EDITION WILL BE USED

HLS 6000 Batch Submittal Form

Source Listing of the Cobra Talon Trajectory Program



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|     |   |          |
|-----|---|----------|
| C   | PROGRAM TRAJ CONVERTED TALON CLEAR                    | 00001000 |
|     | DOUBLE PRECISION X,XD,XDD,TO,TH                       | 00001010 |
|     | DOUBLE PRECISION TC,TI,MK,TH                          | 00001020 |
|     | DOUBLE PRECISION ARRAY,SC1,SC2,T,H,XYZ,RSL,PZ,R,W,P,Q | 00001030 |
|     | DOUBLE PRECISION ARRAY1                               | 00001040 |
|     | DOUBLE PRECISION TN,STN                               | 00001050 |
|     | DOUBLE PRECISION RADANG                               | 00001060 |
|     | COMMON/TS/T,H,XYZ,RSL,PZ                              | 00001070 |
|     | COMMON/A/R,W  | 00001080 |
|     | COMMON/ST/P(3),Q(3)                                   | 00001090 |
|     | COMMON/BS/X(3),XD(3),XDD(3)                           | 00001100 |
|     | COMMON/AX/TH,M  | 00001110 |
|     | COMMON ISW  | 00001120 |
|     | COMMON/PARAM/ARRAY(20),MAX1,MAX2,SC1,SC2,ARRAY1(20)   | 00001130 |
|     | COMMON/NTRAJ/MM                                       | 00001140 |
|     | COMMON/SW1/KZ   | 00001150 |
| C   | KZ .NE. 1 GIVES ORIGINAL PROGRAM                      | 00001160 |
|     | CALL INPUT  | 00001170 |
|     | ICTR = 3  | 00001180 |
|     | ISW = 0   | 00001190 |
|     | CALL FLGEOF (02,IEOFN)                                | 00001200 |
|     | CALL FLGEOF (07,IEOFP)                                | 00001210 |
|     | M = 20925640.00                                       | 00001220 |
|     | N=0.4375269048D-2                                     | 00001230 |
|     | MK=5.72961D1  | 00001240 |
|     | ITM = MM  | 00001250 |
| 4   | DO 17 M = 1,ITM                                       | 00001260 |
|     | IF(KZ.NE.1) GO TO 540                                 | 00001270 |
|     | IF(M.EQ.2) GO TO 17                                   | 00001280 |
|     | IF(M.EQ.3) GO TO 17                                   | 00001290 |
| 540 | CONTINUE  | 00001300 |
|     | CALL SAVE(Q)  | 00001310 |
|     | CALL ICERBM(R)  | 00001320 |
|     | DO 11 I=1,3   | 00001330 |
|     | P(I) = 0.0D0  | 00001340 |
| 11  | Q(I) = 0.0D0  | 00001350 |
|     | IF(M.EQ.2)GO TO 60                                    | 00001360 |
|     | Q0=.1D-1  | 00001370 |
|     | IT=10   | 00001380 |
|     | KA=0  | 00001390 |
|     | MB=0  | 00001400 |
| 20  | DO 16 K=1,60  | 00001410 |
|     | DO 1 K9=1,IT  | 00001420 |
|     | IF(M.LT.0.0D0)GO TO 2                                 | 00001430 |
| 9   | CALL RKG(TO)  | 00001450 |
|     | T = T+ TO   | 00001460 |
|     | CALL EQTNX  | 00001470 |
|     | IF(T-TH)1,2,2   | 00001480 |
| 1   | CONTINUE  | 00001490 |
|     | IF(M.GE.3) GO TO 3                                    | 00001500 |
|     | CALL OUTPUT(K1)                                       | 00001510 |
|     | CALL CONVER   | 00001520 |

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|    |                         |          |
|----|-------------------------|----------|
|    | IF(PZ,NE,0,000)GO TO 92 | 00001530 |
|    | GO TO 16                | 00001540 |
| 92 | IF(KA.EQ.1)GO TO 94     | 00001550 |
|    | KA=1                    | 00001560 |
|    | VB=T                    | 00001570 |
|    | VO=.1D-2                | 00001580 |
|    | IT = 1000               | 00001590 |
|    | GO TO 16                | 00001600 |
| 94 | IF(H-2.0D3)96,96,16     | 00001610 |
| 96 | IF(KB.EQ.1)GO TO 16     | 00001620 |
|    | KB=1                    | 00001630 |
|    | VI=T                    | 00001640 |
|    | VO=.1D-2                | 00001650 |
|    | IT = 1000               | 00001660 |
|    | GO TO 16                | 00001670 |
| 3  | CALL OUTPUT(K1)         | 00001680 |
|    | CALL CONVER             | 00001690 |
|    | IF(PZ,NE,0,000)GO TO 62 | 00001700 |
|    | GO TO 16                | 00001710 |
| 62 | IF(H-2.0D3)63,63,64     | 00001720 |
| 63 | VO=.1D-2                | 00001730 |
|    | VI=1                    | 00001740 |
|    | GO TO 16                | 00001750 |
| 64 | VO=.1D-2                | 00001760 |
|    | IT = 1000               | 00001770 |
| 16 | CONTINUE                | 00001780 |
|    | GO TO 20                | 00001790 |
| 2  | IF(M.EQ.1)GO TO 80      | 00001800 |
|    | CALL PRINT2(1)          | 00001810 |
|    | CALL PRINT2(-1)         | 00001820 |
|    | GO TO 17                | 00001830 |
| 80 | CALL PRINT2(1)          | 00001840 |
|    | CALL PRINT2(-1)         | 00001850 |
|    | GO TO 17                | 00001860 |
| 60 | VO=-.1D-2               | 00001870 |
|    | VI=1                    | 00001880 |
| 70 | DO 18 K6=1,60           | 00001890 |
|    | DO 40 K8=1,IT           | 00001900 |
|    | IF(T.LE.0.0D0)GO TO 86  | 00001910 |
|    | GO TO 10                | 00001920 |
| 86 | CALL PRINT2(1)          | 00001930 |
|    | GO TO 17                | 00001940 |
| 10 | CALL RKG(TO)            | 00001950 |
|    | T = T + TO              | 00001960 |
|    | CALL EQTNX              | 00001970 |
| 40 | CONTINUE                | 00001980 |
|    | CALL OUTPUT(K1)         | 00001990 |
|    | TX=DABS(T-TI)           | 00002000 |
|    | IF(TX.LE..1D-4)GO TO 42 | 00002010 |
|    | IF(T.LE.TI)GO TO 44     | 00002020 |
|    | GO TO 18                | 00002030 |
| 42 | IT=20                   | 00002040 |

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```

      DD=-.1D-2
      GO TO 18
44  TX=DABS(T-TC)
      IF(TX,LE.,.1D-4)GO TO 46
      GO TO 18
46  TY=10
      DD=-.1D-1
18  CONTINUE
      GO TO 70
47  CONTINUE
22  END FILE 2
      REWIND 2
      END FILE 7
      REWIND 7
      READ (02) ARRAY
      IF(IEOFN) 305,69,305
69  BTN = ARRAY(1)
      STN = STN
      BT = ARRAY(1)
      PRINT 330
330  FORMAT(1H1,//////////1//////////66(2H* ),///38X,
      *RADAR PARAMETER DIFFERENCES(PERTURBED-NOMINAL)",
      *//66(2H* ),//66(2H* )//1H1)
      PRINT 440,M
      PRINT 340
      PRINT 337
      PRINT 999
      PRINT 345
      PRINT 336
      PRINT 999
999  FORMAT(1H )
440  FORMAT(1H1,20X,5H M = ,14)
340  FORMAT(1H0,4HTIME,4X,11HSLANT RANGE,7X,13HSL RANGE RATE,6X,17HSL RANGE RATE DOT,7X,7HAZIMUTH,8X,12HAZIMUTH RATE)
345  FORMAT(10X,16HAZIMUTH RATE DOT,4X,9HELEVATION,8X,14HELEVATION RATE,16X,18HELEVATION RATE DOT)
310  READ (07) ARRAY1
      IF(IEOFP) 200,204,200
204  BT1 = ARRAY1(1)
203  IF(STT.EQ.STT1) GO TO 250
      IF(STT.GT.STT1) GO TO 210
214  READ (02) ARRAY
      IF(IEOFN) 305,202,305
202  BT = ARRAY(1)
      GO TO 203
305  ICTR = ICTR + 1
      IF(ITH.EQ.ICTR) GO TO 200
      PRINT 440,M
      PRINT 340
      PRINT 337
      PRINT 999
      PRINT 345

```

00002050  
 00002060  
 00002070  
 00002080  
 00002090  
 00002100  
 00002110  
 00002120  
 00002130  
 00002140  
 00002150  
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 00002170  
 00002180  
 00002190  
 00002200  
 00002210  
 00002220  
 00002230  
 00002240  
 00002250  
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 00002680

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      PRINT 336                                00002690
      PRINT 999                                00002700
337  FORMAT(2X,7HMINUTES,2X,4HFEET,14X,9HFEET/SEC,10X,12HFEET/SEC/SEC, 00002710
      16X,7HDEGREES,8X,11HDEGREES/SEC)        00002720
336  FORMAT(10X,15HDEGREES/SEC/SEC,5X,7HDEGREES,10X,11HDEGREES/SEC,9X, 00002730
      15HDEGREES/SEC/SEC)                     00002740
      REWIND 2                                00002750
      CALL FLGEOF (02,IEOFN)                  00002760
      IF (STT.LE,STT1) GO TO 333              00002770
      GO TO 201                                00002780
333  READ (07) ARRAY1                          00002790
      IF (IEOFN) 200,334,200                  00002800
334  BYT1=ARRAY1(1)                           00002810
      IF (STT.LE,STT1) GO TO 333              00002820
      READ (02) ARRAY                         00002830
      IF (IEOFN) 305,335,305                  00002840
335  BYT=ARRAY(1)                             00002850
      GO TO 203                                00002860
210  IF (SSTN.E0,STT1) GO TO 212             00002870
      GO TO 310                                00002880
212  REWIND 2                                00002890
      CALL FLGEOF (02,IEOFN)                  00002900
      GO TO 214                                00002910
250  DT = ARRAY(1)                           00002920
      DRS = - (ARRAY(2)-ARRAY1(2))            00002930
      DRSD = - (ARRAY(3)-ARRAY1(3))           00002940
      DRSD0 = - (ARRAY(4)-ARRAY1(4))          00002950
      DSIG = - (ARRAY(5)-ARRAY1(5))           00002960
      DSIGD = - (ARRAY(6)-ARRAY1(6))          00002970
      DSIGD0 = - (ARRAY(7)-ARRAY1(7))         00002980
      DEL = - (ARRAY(8)-ARRAY1(8))            00002990
      DELD = - (ARRAY(9)-ARRAY1(9))           00003000
      DELD0 = - (ARRAY(10)-ARRAY1(10))        00003010
      RADANG = DSORT(DSIG**2 + DEL**2)        00003020
      PRINT 350,DT,DRS,DRSD,DRSD0,DSIG,DSIGD,DSIGD0,DEL,DELD,DELD0 00003030
      PRINT 700,RADANG                        00003040
      PRINT 999                              00003050
700  FORMAT(1H0,36H ANGULAR SEPRATION IN RADAR BEAM = ,D22.10) 00003060
350  FORMAT(F7.3,2X,D17.10,2X,D17.10,2X,D17.10,2X,D17.10,2X,D17.10/ 00003070
      1 9X,D17.10,2X,D17.10,2X,D17.10,2X,D17.10) 00003080
201  READ (02) ARRAY                          00003090
      IF (IEOFN) 305,312,305                  00003100
312  BYT = ARRAY(1)                           00003110
      GO TO 310                                00003120
200  STOP                                     00003130
      END                                     00003140

```



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```

SUBROUTINE EQTX                                00003150
DOUBLE PRECISION ARRAY,SC1,SC2,T,H,XYZ,RSL,PZ,R,W,P,Q 00003160
DOUBLE PRECISION V6,EL2,EL3,EL4,EL5,EL6,AA           00003170
DOUBLE PRECISION DV,XYZ,ZK,S1,S2,S3,S4,S6,VA,VDD,VD,S23,Q1,Q2,Q3 00003180
DOUBLE PRECISION X,XD,XDD                           00003190
DOUBLE PRECISION A,R,W                               00003200
DIMENSION DV(5)                                       00003210
COMMON/BS/X(3),XD(3),XDD(3)                          00003220
COMMON/TS/T,H,XYZ,RSL,PZ                            00003230
COMMON/A/R,W                                           00003240
COMMON/EQATMO/Z,K,KAT                                00003250
DATA DV/2.42167*4D12,4*0.0D0/                       00003260
S6=2.0D0                                              00003270
S1=DCOS(X(2))                                         00003280
S2=DSIN(X(2))                                         00003290
S3=DSIN(S6*X(2))                                     00003300
S4=DCOS(S6*X(2))                                     00003310
RSL = R                                               00003320
W= X(1)- RSL                                         00003330
IF (KAT.EQ.1) GO TO 21                              00003340
20 PZ = 0.0D0                                         00003350
GO TO 30                                              00003360
21 CALL ATMOSP                                        00003370
30 VA = (XD(1)*XD(1))/(X(1)*X(1))+XD(2)*XD(2)*(S1*(XD(3)+W))**2 00003380
XYZ=X(1)*DSQRT(VA)                                   00003390
22 VDD= XD(1)*XD(1)+ X(1)*XD(2)*X(1)*XD(2)+(X(1)*(XD(3)+W)*S1)**2 00003400
VD=DSQRT(VDD)                                         00003410
S23=-PZ*ZK*VD                                         00003420
Q1= S23*XD(1)                                         00003430
Q2= S23*XD(2)                                         00003440
Q3= S23*(XD(3)+W)                                     00003450
V6 = R/X(1)                                           00003460
EL2=X(1)*XD(2)*XD(2)+0.5D0*(1.0D0+S4)*(W+XD(3))*(W+XD(3))*X(1) 00003470
EL3=DV(1)/X(1)*V6+DV(2)/X(1)*V6**3*(3.0D0*S4-1.0D0) 00003480
EL4=DV(3)/X(1)*V6**5*(35.0D0*S4*S4-10.0D0*S4-13.0D0) 00003490
XDD(1)= EL2-EL3-EL4+Q1                               00003500
EL5=(-S6*XD(2)*XD(1))/X(1)-0.5D0*S3*(W+XD(3))*(W+XD(3)) 00003510
EL6=-DV(4)/X(1)*X(1)*V6**3*S3+DV(5)/X(1)*X(1)*V6**5*S3*(1.0D0- 00003520
17.0D0*S4)                                           00003530
XDD(2)=EL5+EL6+Q2                                     00003540
AA=-1.0D0*(W+XD(3))                                  00003550
XDD(3)=AA*(S6*XD(1)/X(1))-AA*(S6*XD(2)*S21/S1+Q3) 00003560
RETURN                                                00003570
END                                                  00003580

```

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```

SUBROUTINE ICER34(P)
DOUBLE PRECISION VO,RAT
DOUBLE PRECISION RDP,RTDP,RLDP,C13,GMU,CA,GAM,BETA,GLAM,HX,THE,RO
DOUBLE PRECISION X,XD,XDD
DOUBLE PRECISION ARRAY,SC1,SC2,T,H,XYZ,RSL,PZ,R,W,P,Q
DOUBLE PRECISION P,GEO,GLAMD,ROD,THEI
DOUBLE PRECISION XN,XDN
DOUBLE PRECISION COSGAM,COSHET,SINGAM,SINRET,V2,A,B,C
DOUBLE PRECISION SNI,VBODR,VBO
COMMON/BS/X(3),XD(3),XDD(3)
COMMON/TS/T,H,XYZ,RSL,PZ
COMMON/A/R,W
COMMON/IC/CA,BETA,GAM,HX,GLAM,THE,GLAMI,THEI
COMMON/PTURB/A(2),B(2),C(2)
COMMON/IC2/VO,INERTL
COMMON/SW1/KZ
COMMON/IC3/TMI
DIMENSION RDP(2),RLDP(2),RTDP(2)
DIMENSION XN(3),XDN(3)
DIMENSION XN1(2),XDN1(2)
DOUBLE PRECISION GLAMI,THEI
DOUBLE PRECISION TMI
DOUBLE PRECISION TN,STN,TM
COMMON/AX/TM,M
C13=0.717453292519943205769237
GMU=5.067574019
RO = R + HX
IF(M-2)6,1,15
6 CONTINUE
XD(1)=VO*DCOS(GAM*C13)
XD(2)=VO/RO*DSIN(GAM*C13)*DCOS(BETA*C13)
RAT=RO*DCOS(THE*C13)
XD(3)=VO*DSIN(GAM*C13)*DSIN(BETA*C13)/RAT
IF(INERTL.EQ.1)XD(3)=XD(3)-W
X(1)=RO
X(2)= THE*C13
X(3)= GLAM*C13
4 CALL EQTNX
CALL CONVER
CALL OUTPUT(K)
IF(KZ.NE.1) GO TO 3
DO 32 I=1,3
XN1(I)=X(I)
XDN1(I)=XD(I)
32 CONTINUE
30 CONTINUE
TN=TM
RETURN
C
10 CONTINUE
X(2)= THEI*C13
X(3)= GLAMI*C13

```

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|    |  |         |
|----|--|---------|
|    | TM = TM1   | 0004090 |
|    | CALL OUTPUT(K)   | 0004100 |
|    | RETURN   | 0004110 |
| 16 | T=0.000  | 0004120 |
|    | TM = TN  | 0004130 |
|    | IF(M.GT.3) GO TO 20  | 0004140 |
|    | DO 18 I = 1,3  | 0004150 |
|    | XN(I) = X(I)   | 0004160 |
|    | XDN(I) = XD(I)   | 0004170 |
| 18 | CONTINUE   | 0004180 |
|    | CALL EQTNX   | 0004190 |
|    | CALL OUTPUT(K)   | 0004200 |
|    | RETURN   | 0004210 |
| 20 | IF(KZ.NE.1) GO TO 35   | 0004220 |
|    | DO 25 I=1*3  | 0004230 |
|    | X(I) = XN1(I)  | 0004240 |
|    | XD(I) = XDN1(I)  | 0004250 |
|    | XN(I) = XN1(I)   | 0004260 |
|    | XDN(I) = XDN1(I)   | 0004270 |
| 25 | CONTINUE   | 0004280 |
|    | GO TO 45   | 0004290 |
| 35 | X(I) = XN(I)   | 0004300 |
| 45 | CONTINUE   | 0004310 |
|    | SN1 = DCOS(XN(2)*C13)  | 0004320 |
|    | V80DR = DSQRT((XDN(1)/XN(1))**2 + XDN(2)*XDN(2)+(SN1*XDN(3))**2) | 0004330 |
|    | V80 = XN(1) * V80DR  | 0004340 |
|    | BETA = DATAN2(XDN(3)*SN1,XDN(2))                                 | 0004350 |
|    | COSBET = DCOS(BETA)  | 0004360 |
|    | SINBET = DSIN(BETA)  | 0004370 |
|    | COSGAM = XDN(1) / V80  | 0004380 |
|    | SINGAM = XDN(2) / (V80DR * COSBET)                               | 0004390 |
|    | V2 = B(M)*SINGAM+C(M)*COSGAM                                     | 0004400 |
|    | RDP(M) = (-B(M)*COSGAM+C(M)*SINGAM)*60.000                       | 0004410 |
|    | RTDP(M) = (-V2*COSBET-A(M)*SINBET)*60.000                        | 0004420 |
|    | RLDP(M) = (-V2*SINBET+A(M)*COSBET)*60.000                        | 0004430 |
|    | XD(1) = XDN(1) + RDP(M)  | 0004440 |
|    | XD(2) = XDN(2) + RTDP(M)/XN(1)                                   | 0004450 |
|    | RATN = XN(1)*DCOS(XN(2)*C13)                                     | 0004460 |
|    | XD(3) = XDN(3) + RLDP(M)/RATN                                    | 0004470 |
|    | CALL EQTNX   | 0004480 |
|    | CALL CONVER  | 0004490 |
|    | CALL OUTPUT(K)   | 0004500 |
|    | RETURN   | 0004510 |
|    | END  | 0004520 |

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|    |   |          |
|----|---|----------|
|    | SUBROUTINE ATMOSP                                       | 00004530 |
|    | DOUBLE PRECISION HP, H2P, SK3, HB, PB, SK1, SK2, CD, ST | 00004540 |
|    | DOUBLE PRECISION TS, T, H, V, RSL, PZ, XYZ              | 00004550 |
|    | COMMON/TS/T, H, XYZ, RSL, PZ                            | 00004560 |
|    | HP=.3048D+H   | 00004570 |
|    | H2P=HP*(1.000+HP/7.6356766D7)                           | 00004580 |
|    | IF (HP-5.3D4) 20, 25, 25                                | 00004590 |
| 20 | IF (HP-4.7D4) 21, 29, 29                                | 00004600 |
| 21 | IF (HP-2.5D4) 22, 30, 30                                | 00004610 |
| 22 | IF (HP-1.1D4) 23, 31, 31                                | 00004620 |
| 23 | IF (HP) 28, 28, 32                                      | 00004630 |
| 25 | IF (HP-7.9D4) 33, 33, 28                                | 00004640 |
| 26 | IF (HP-9.0D4) 34, 34, 27                                | 00004650 |
| 27 | IF (HP-1.5D5) 35, 35, 28                                | 00004660 |
| 28 | PZ=0.0D0  | 00004670 |
|    | G1=0.0D0  | 00004680 |
|    | G2=0.0D0  | 00004690 |
|    | G3=0.0D0  | 00004700 |
|    | RETURN  | 00004710 |
| 29 | SK3=.120869D-3  | 00004720 |
|    | HB=4.7D4  | 00004730 |
|    | PB=2.8804D-6  | 00004740 |
|    | GO TO 37  | 00004750 |
| 30 | SK1=.138466D-4  | 00004760 |
|    | SK2=.13883D1  | 00004770 |
|    | PB=7.765D-5   | 00004780 |
|    | HB=2.5D4  | 00004790 |
|    | GO TO 36  | 00004800 |
| 31 | SK3=.157689D-3  | 00004810 |
|    | HB=1.1D4  | 00004820 |
|    | PB=7.062D-4   | 00004830 |
|    | GO TO 37  | 00004840 |
| 32 | SK1=-0.225569D-4  | 00004850 |
|    | SK2=-5.25612D-7   | 00004860 |
|    | PB=2.37692D-3   | 00004870 |
|    | HB=0.0D0  | 00004880 |
|    | GO TO 36  | 00004890 |
| 33 | SK1=-0.159272D-4  | 00004900 |
|    | SK2=-7.59218D-7   | 00004910 |
|    | PB=1.39468D-6   | 00004920 |
|    | HB=5.3D4  | 00004930 |
|    | GO TO 36  | 00004940 |
| 34 | SK3=.216234D-3  | 00004950 |
|    | HB=7.9D4  | 00004960 |
|    | PB=4.1169D-8  | 00004970 |
|    | GO TO 37  | 00004980 |
| 35 | SK1=.241458D-4  | 00004990 |
|    | SK2=.5412D-7  | 00005000 |
|    | PB=4.251D-9   | 00005010 |
|    | HB=9.0D4  | 00005020 |
| 36 | CD=1.0D0+SK1*(42D-HB)                                   | 00005030 |
|    | ST=-(1.0D0+SK2)   | 00005040 |



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|    |                           |          |
|----|---------------------------|----------|
|    | RZ= PB*(CD**SI)           | 00005050 |
|    | RETURN                    | 00005060 |
| 37 | RZ=PB*DEXP(-SK3*(H2P-HB)) | 00005070 |
|    | RETURN                    | 00005080 |
|    | END                       | 00005090 |

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|   |          |
|---|----------|
| SUBROUTINE OUTPUT(K)                                  | 00005100 |
| DOUBLE PRECISION CC                                   | 00005110 |
| DOUBLE PRECISION ARRAY,SC1,SC2,T,H,XYZ,RSL,PZ,R,W,P,O | 00005120 |
| DOUBLE PRECISION X,XD,XDD                             | 00005130 |
| DOUBLE PRECISION ARRAY1                               | 00005140 |
| COMMON/TS/T,H,XYZ,RSL,PZ                              | 00005150 |
| COMMON/PARAM/ARRAY(20),MAX1,MAX2,SC1,SC2,ARRAY1(20)   | 00005160 |
| COMMON/BS/X(3),XD(3),XDD(3)                           | 00005170 |
| DATA CC/57.295779513,8232,876798155/                  | 00005180 |
| ARRAY(1)=T  | 00005190 |
| ARRAY(2)=X(1)   | 00005200 |
| ARRAY(3)= X(2)*CC                                     | 00005210 |
| ARRAY(4)= X(3)*CC                                     | 00005220 |
| ARRAY(5)=H  | 00005230 |
| ARRAY(6)=XYZ/ .6D2                                    | 00005240 |
| ARRAY(7)=RSL  | 00005250 |
| ARRAY(8)=PZ   | 00005260 |
| ARRAY(9)=XD(1)/ .6D2                                  | 00005270 |
| ARRAY(10)=XD(2)*CC/0.6D2                              | 00005280 |
| ARRAY(11)=XD(3)*CC/0.6D2                              | 00005290 |
| ARRAY(12)=XDD(1)/ .36D4                               | 00005300 |
| ARRAY(13)=XDD(2)*CC/0.36D4                            | 00005310 |
| ARRAY(14)=XDD(3)*CC/0.36D4                            | 00005320 |
| CALL SAVE (1)   | 00005330 |
| RETURN  | 00005340 |
| END   | 00005350 |

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|   |  |          |
|---|--|----------|
|   | SUBROUTINE SAVE (N)                                      | 00005360 |
|   | DOUBLE PRECISION ARRAY, SC1, SC2, ARRAY1                 | 00005370 |
|   | COMMON/PARAM/ARRAY(20), MAX1, MAX2, SC1, SC2, ARRAY1(20) | 00005380 |
|   | IF(N)2,3,1   | 00005390 |
| 3 | MAX1= 0  | 00005400 |
|   | MAX2= 0  | 00005410 |
|   | REWIND 3   | 00005420 |
|   | REWIND 4   | 00005430 |
|   | RETURN   | 00005440 |
| 1 | WRITE (3) ARRAY  | 00005450 |
|   | MAX1=MAX1+1  | 00005460 |
|   | RETURN   | 00005470 |
| 2 | WRITE (4) ARRAY  | 00005480 |
|   | MAX2=MAX2+1  | 00005490 |
|   | RETURN   | 00005500 |
|   | END  | 00005510 |

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|      |  |         |
|------|--|---------|
|      | SUBROUTINE PRINT2(N)   | 0 05520 |
|      | DOUBLE PRECISION ARRAY,SC1,SC2,ARRAY1                              | 0 05530 |
|      | COMMON/SW1/KZ  | 0 05540 |
|      | COMMON/AX/TM,4   | 0 05550 |
|      | COMMON/PARAM/ARRAY(20),MAX1,MAX2,SC1,SC2,ARRAY1(20)                | 0 05560 |
|      | DOUBLE PRECISION TM  | 0 05570 |
|      | IF(N)2,1,1   | 0 05580 |
| 1    | REWIND 3   | 0 05590 |
|      | IFLAG=0  | 0 05600 |
|      | DO 3 I=1,MAX1  | 0 05610 |
|      | IF(IFLAG.NE.0)GO TO 5  | 0 05620 |
| 14   | PRINT 1002   | 0 05630 |
| 1002 | FORMAT(1H1,2X,4HTIME,7X,6HRADIUS,12X,6HLATITUDE,7X,9HLONGITUDE,    | 0 05640 |
|      | 112X,6HHEIGHT,11X,8HVELOCITY,9X,12HR(SEA LEVEL),8X,7HDENSITY,//)   | 0 05650 |
|      | IFLAG=52   | 0 05660 |
| 5    | READ (3) ARRAY   | 0 05670 |
|      | PRINT 1000,(ARRAY(J),J=1,8)  | 0 05680 |
| 1000 | FORMAT(1X,F8.4,1X,D17.10,2X,D14.7,2X,D16.9,2X,D15.9,               | 0 05690 |
|      | *2X,D17.1,1X,  | 0 05692 |
|      | 1D17.10,2X,D14.7)  | 0 05700 |
| 3    | IFLAG=IFLAG-1  | 0 05710 |
|      | REWIND 3   | 0 05720 |
|      | IFLAG=0  | 0 05730 |
|      | DO 4 I=1,MAX1  | 0 05740 |
|      | IF(IFLAG.NE.0)GO TO 7  | 0 05750 |
| 6    | PRINT 1003   | 0 05760 |
| 1003 | FORMAT(1H1,2X,4HTIME,9X,5HR-DOT,13X,8HLAT.-DOT,8X,9HLONG.-DOT,     | 0 05770 |
|      | 110X,9HR-DOT DOT,9X,12HLAT.-DOT DOT,8X,13HLONG.-DOT DOT,//)        | 0 05780 |
|      | IFLAG=52   | 0 05790 |
| 7    | READ (3) ARRAY   | 0 05800 |
|      | PRINT 1001,ARRAY(1),(ARRAY(J),J=9,14)                              | 0 05810 |
| 1001 | FORMAT(F9.4,2X,D16.9,4X,D13.6,4X,D13.6,4X,D16.9,4X,D16.7,4X,D16.7, | 0 05820 |
|      | 14X,D16.7)   | 0 05830 |
| 4    | IFLAG=IFLAG-1  | 0 05840 |
|      | RETURN   | 0 05850 |
| 2    | REWIND 4   | 0 05860 |
|      | IFLAG=1  | 0 05870 |
|      | DO 10 I=1,MAX2   | 0 05880 |
|      | IF(IFLAG.NE.0)GO TO 9  | 0 05890 |
| 8    | PRINT 1008,SC1,SC2   | 0 05900 |
| 1008 | FORMAT(1H1,35X,16HSENSOR-LATITUDE ,F9.5,5X,13HLONGITUDE(W),        | 0 05910 |
|      | 1F10.5,//)   | 0 05920 |
|      | PRINT 1004   | 0 05930 |
| 1004 | FORMAT(2X,9HTIME(MIN),7X,15HSLANT RANGE(FT),3X,21HSL RANGE RATE(FT | 0 05940 |
|      | 1/SEC),3X,25HSL RANGE RDOT(FT/SEC/SEC),3X,12HAZIMUTH(DEG),3X,      | 0 05950 |
|      | 216HAZ RATE(DEG/SEC))  | 0 05960 |
|      | IFLAG=52   | 0 05970 |
| 9    | READ (4) ARRAY   | 0 05980 |
|      | PRINT 1005,(ARRAY(J),J=1,6)  | 0 05990 |
| 1005 | FORMAT(F8.4, D21.12,D21.12,D24.12,5X,D16.9,4X,D12.5)               | 0 06000 |
| 10   | IFLAG=IFLAG-1  | 0 06010 |
|      | REWIND 4   | 0 06020 |



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|   |          |
|---|----------|
| IFLAG=0   | 00006030 |
| DO 11 I=1,MAX2  | 00006040 |
| IF(IFLAG.NE.0)GO TO 13  | 00006050 |
| 12 PRINT 1006   | 00006060 |
| 1006 FORMAT(1H1,2X,9HTIME(MIN),2X,20HAZ RDOT(DEG/SEC/SEC),3X,14HELEVATI | 00006070 |
| 10N(DEG),5X,16HEL RATE(DEG/SEC),3X,20HEL RDOT(DEG/SEC/SEC),2X,13HRE     | 00006080 |
| 2ENTRY ANGLE,6X,7HHEADING)  | 00006090 |
| IFLAG=52  | 00006100 |
| 13 READ (4)ARRAY  | 00006110 |
| PRINT 1007,ARRAY(1), (ARRAY(J),J=7,12)                                  | 00006120 |
| 1007 FORMAT(F8.4, D19.8,7X,D16.7,5X,D16.7,D23.12,4X,D12.6,4X,D12.6)     | 00006130 |
| 11 IFLAG=IFLAG-1  | 00006140 |
| PRINT 1010  | 00006150 |
| 1010 FORMAT(53X,13HEND OF OUTPUT)                                       | 00006160 |
| RETURN  | 00006170 |
| END   | 00006180 |

```

SUBROUTINE CONVER
DOUBLE PRECISION CS,SS,XS,YS,ZS,SRS,DSPS,RS,RSD,XNUM1,XNUM2,XNUM3 000 6190
DOUBLE PRECISION COST,COSL,SINT,SINL,EX,Y,Z,EXD,YD,ZD,XDR,YDP,ZDP 000 6200
DOUBLE PRECISION TWOPI,EF,F,REQ,BK2,BK3,BK4,AK,W2,W3,W4,W5,FT,FT2 000 6210
DOUBLE PRECISION XNUM,XNUM,S1K,W9,S2K,S3K,S1K2,S2K2,OPS,E,W6,W7 000 6220
DOUBLE PRECISION XNLM,ED,SIG,W14,W15,SIGD,RSDD,SIGDD,END 000 6230
DOUBLE PRECISION ARRAY,SC1,SC2,T,H,XYZ,RSL,PZ,R,W,P,Q 000 6240
DOUBLE PRECISION X,XD,XDD 000 6250
DOUBLE PRECISION AH,ACTAG1, ACTAG2, ACTAG3 000 6260
DOUBLE PRECISION EL,ELD,ELDD 000 6270
DOUBLE PRECISION TN,STN,TM 000 6280
DOUBLE PRECISION ARRAY1 000 6290
DOUBLE PRECISION PI,HALFPI,THAPI,ARSIN,COSLT,GNUM,GDEM,BETA,GAM 000 6300
DOUBLE PRECISION AH,XPUM,VPRIME,GNUM2,COSR 000 6310
DOUBLE PRECISION ELIM 000 6320
COMMON/COEL/ELIM 000 6330
COMMON ISW 000 6340
COMMON/PARAM/ARRAY(20),MAX1,MAX2,SC1,SC2,ARRAY1(20) 000 6350
COMMON/T3/T,H,XYZ,RSL,PZ 000 6360
COMMON/BS/X(3),XD(3),XDD(3) 000 6370
COMMON/AX/TM,M 000 6380
COMMON/SW1/KZ 000 6390
COMMON/CONV/AH 000 6400
COMMON/CON/IK,JK 000 6410
COST=DCOS(X(2)) 000 6420
COSL=DCOS(X(3)) 000 6430
EF=57.295779513 5232.876798155 000 6440
F=J.000 000 6450
RE=20925640.00 000 6460
BK2=3.372671822D-3 000 6470
BK3=5.68734929D-6 000 6480
BK4=1.2651557D-8 000 6490
AK =0.017453292519943295769237 000 6500
PI = 3.141592653589793238462643400 000 6510
HALFPI = PI/2.000 000 6520
THAPI = 1.5D *PI 000 6530
TWOPI = 2.00D*PI 000 6540
SINT=DSIN(X(2)) 000 6550
SINL=DSIN(X(3)) 000 6560
EX =X(1)*COST*COSL 000 6570
Y =-X(1)*COST*SINL 000 6580
Z =X(1)*SINT 000 6590
EXD =XD(1)*COST*COSL-X(1)*XD(2)*SINT*COSL-X(1)*XD(3)*COST*SINL 000 6600
YD =-XD(1)*COST*SINL+X(1)*XD(2)*SINT*SINL-X(1)*XD(3)*COST*COSL 000 6610
ZD =XD(1)*SINT+X(1)*XD(2)*COST 000 6620
XDD=(XDD(1)-X(1)*(XD(2)*XD(2))-X(1)*(XD(3)*XD(3)))*COST*COSL 000 6630
1 -(2.00D*X(1)*XD(2)+X(1)*XDD(2))*SINT*COSL 000 6640
2 -(2.00D*X(1)*XD(3)+X(1)*XDD(3))*COST*SINL 000 6650
3 +2.00D*X(1)*XD(2)*XD(3)*SINT*SINL 000 6660
YDD=-(XDD(1)-X(1)*(XD(2)*XD(2))-X(1)*(XD(3)*XD(3)))*COST*SINL 000 6670
1 +(2.00D*X(1)*XD(2)+X(1)*XDD(2))*SINT*SINL 000 6680
2 -(X(1)*XDD(3)+2.00D*X(1)*XD(3))*COST*COSL 000 6690

```

|    |   |          |
|----|---|----------|
| 3  | +2.0DU*X(1)*XD(2)*XD(3)*SINT*CSL                  | 00006710 |
|    | SDP=(XDD(1)-X(1)*XD(2)*XD(2))*SINT                | 00006720 |
| 1  | *(2.0DU*XDD(1)*XD(2)+X(1)*XDD(2))*COST            | 00006730 |
|    | W2=DSIN(SC1*AK)                                   | 00006740 |
|    | W3=DCOS(SC1*AK)                                   | 00006750 |
|    | W4=DSIN(SC2*AK)                                   | 00006760 |
|    | W5=DCOS(SC2*AK)                                   | 00006770 |
|    | FT=(1.0DU-F)**2                                   | 00006780 |
|    | FT2=(2.0DU*F)-F**2                                | 00006790 |
|    | CS=REQ/(DSQRT(1.0DU-FT2*W2**2))                   | 00006800 |
|    | BS=(CS*FT)+AH                                     | 00006810 |
|    | XS=(CS*AH)*W3*W5                                  | 00006820 |
|    | YS=(CS*AH)*W3*W4                                  | 00006830 |
|    | ZS=SG*W2  | 00006840 |
|    | BRS=DSQRT(XS**2+YS**2+ZS**2)                      | 00006850 |
|    | DSPS=0.000  | 00006860 |
|    | S1K=-((EX-XS)*W2*W5+(Y-YS)*W2*W4-(Z-ZS)*W3)       | 00006870 |
|    | W9=SC2*AK   | 00006880 |
|    | S2K=X(1)*COST*DSIN(X(3)+W9)                       | 00006890 |
|    | S3K=(EX-XS)*W3*W5+(Y-YS)*W3*W4+(Z-ZS)*W2          | 00006900 |
|    | S1K2=S1K**2                                       | 00006910 |
|    | S2K2=S2K**2                                       | 00006920 |
|    | S3K2=S3K**2                                       | 00006930 |
|    | RS=DSQRT(S1K2+S2K2+S3K2)                          | 00006940 |
|    | RSD=(EXD*(EX-XS)+YD*(Y-YS)+ZD*(Z-ZS))/RS          | 00006950 |
|    | XNUM1=((EX-XS)*XS)/RS                             | 00006960 |
|    | XNUM2=((Y-YS)*YS)/RS                              | 00006970 |
|    | XNUM3=((Z-ZS)*ZS)/RS                              | 00006980 |
|    | XNUM=(XNUM1+XNUM2+XNUM3)/SRS                      | 00006990 |
|    | XNUM=(XNUM1+XNUM2+XNUM3)*RS                       | 00007000 |
|    | OPS=DSQRT(S1K2+S2K2)                              | 00007010 |
|    | ACTAG1=OPS/S3K                                    | 00007020 |
|    | B=DATAN2(OPS,S3K)                                 | 00007030 |
|    | IF(W.EQ.3) GO TO 30                               | 00007040 |
|    | IF(T.LT.TN) GO TO 200                             | 00007050 |
|    | IF(E.LT.0.0DU.AND.ELIM.LT.90.00) GO TO 200        | 00007060 |
|    | IF(E.LE.(ELIM*AK)) GO TO 47                       | 00007062 |
|    | GO TO 200   | 00007064 |
| 30 | IF(E.LE.(ELIM*AK)) GO TO 40                       | 00007070 |
|    | GO TO 200   | 00007080 |
| 40 | IF(ISW.NE.0) GO TO 47                             | 00007090 |
|    | YN = T  | 00007100 |
|    | ISW = 1   | 00007110 |
| 47 | EL = TWOPI/4.0D-E                                 | 00007120 |
| 45 | W6=DSIN(E)  | 00007130 |
|    | W7=DCOS(E)  | 00007140 |
|    | XNLM=XS*EXD+YS*YD+ZS*ZD                           | 00007150 |
|    | ED=(-RS*XNLM+XNUM*RSD)/(SRS*(RS**2)*DSIN(E+DSPS)) | 00007160 |
|    | ELD=-ED   | 00007170 |
| 60 | ACTAG2= S2K/S1K                                   | 00007180 |
|    | SIG=DATAN2(S2K,S1K)                               | 00007190 |
|    | IF(SIG-GE.0.000) GO TO 9                          | 00007200 |

|     |  |          |
|-----|--|----------|
| 90  | SIG=SIG+TWOPI  | 00007210 |
|     | W14=DSIN(SIG)  | 00007220 |
|     | W15=DCOS(SIG)  | 00007230 |
|     | IF(DABS(W14).GE.1.0D-16.AND.W6.GT.0.000)GO TO 105              | 00007240 |
| 100 | SIGD=0.000   | 00007250 |
|     | GO TO 110  | 00007260 |
| 105 | SIGD=(EXP*W2*W5 + YD*W2*W4-ZD*W3 + (RSD*W6+RS*ED*W7)*W15)      | 00007270 |
|     | 1/(RS*W6*W14)  | 00007280 |
| 110 | XPUM1=(XS/SRS)*(XDP/RS)  | 00007290 |
|     | XPUM2=(YS/SRS)*(YDP/RS)  | 00007300 |
|     | XPUM3=(ZS/SRS)*(ZDP/RS)  | 00007310 |
|     | XPUM=(XPUM1+XPUM2+XPUM3)/(DSIN(E+DSPS))                        | 00007320 |
|     | RSDD=((EX-XS)*XDP+(Y-YS)*YDP+(Z-ZS)*ZDP                        | 00007330 |
| 1   | + (EXP*EXP+YD*YD+ZD*ZD-RSD*RS))/RS                             | 00007340 |
|     | EDD=-XPUM*((XNUM/DSIN(E+DSPS))*(RSDD/RS))-(ED*ED*(DCOS(E+DSPS) | 00007350 |
| 1   | /DSIN(E+DSPS))-(2.0D*ED*(RSD/RS))                              | 00007360 |
|     | ELDD=-EDD  | 00007370 |
|     | IF(DABS(W14).GE.1.0D-16.AND.W6.GT.0.000)GO TO 108              | 00007380 |
|     | SIGDD=0.000  | 00007390 |
|     | GO TO 109  | 00007400 |
| 108 | SIGDD=(XDP*W2*W5+YDP*W2*W4-ZDP*W3-2.000*RSD*W6*W14*SIGD        | 00007410 |
| 1   | -2.000*RS*W7*W14*ED*SIGD-2.000*RS*W6*W15*SIGD*SIGD             | 00007420 |
| 2   | +2.000*RSD*W7*W15*ED*RSDD*W6*W15+RS*EDD*W7*W15)/(RS*W6*W14)    | 00007430 |
| 109 | SIGD=SIGD*EF   | 00007440 |
|     | EL=EL*EF   | 00007450 |
|     | ELD=ELD*EF/0.602   | 00007460 |
|     | ELDD=ELDD*EF/0.3604  | 00007470 |
|     | SIG=SIG*EF   | 00007480 |
|     | SIGDD=SIGDD*EF   | 00007490 |
|     | ARRAY(1)=T   | 00007500 |
|     | ARRAY(2)=RS  | 00007510 |
|     | ARRAY(3)=RSD/0.602   | 00007520 |
|     | ARRAY(4)=RSDD/0.3604   | 00007530 |
|     | ARRAY(5)=SIG   | 00007540 |
|     | ARRAY(6)=SIGD/0.602  | 00007550 |
|     | ARRAY(7)=SIGDD/0.3604  | 00007560 |
|     | ARRAY(8)=EL  | 00007570 |
|     | ARRAY(9)=ELD   | 00007580 |
|     | ARRAY(10)=ELDD   | 00007590 |
| C   | CALCULATION OF HEADING ANGLE(CLOCKWISE 0 TO 2PI)               | 00007600 |
|     | COSLT=XD(3)*COS/XD(2)  | 00007610 |
|     | IF(XD(2))1,2,3   | 00007620 |
| C   | ZERO XD(2)   | 00007630 |
| 2   | IF(COSLT)4,5,6   | 00007640 |
| C   | NEGATIVE COSLT   | 00007650 |
| 4   | BETA=TIHPI   | 00007660 |
|     | GO TO 60   | 00007670 |
| C   | ZERO COSLT   | 00007680 |
| 5   | BETA=1.001*PI  | 00007690 |
|     | GO TO 60   | 00007700 |
| C   | POSITIVE COSLT   | 00007710 |
| 6   | BETA=HALFPI  | 00007720 |



|    |   |          |
|----|---|----------|
|    | GO TO 60  | 00007730 |
| C  | NEGATIVE XD(2)                                    | 00007740 |
| 1  | IF (COSLT) 9,8,9                                  | 00007750 |
| C  | NEGATIVE OR POSITIVE COSLT                        | 00007760 |
| 9  | BETA = PI + DATAN(COSLT)                          | 00007770 |
|    | GO TO 60  | 00007780 |
| C  | ZERO COSLT  | 00007790 |
| 8  | BETA = PI   | 00007800 |
|    | GO TO 60  | 00007810 |
| C  | POSITIVE XD(2)                                    | 00007820 |
| 3  | IF (COSLT) 10,11,12                               | 00007830 |
| C  | NEGATIVE COSLT                                    | 00007840 |
| 10 | BETA = TWOPI + DATAN(COSLT)                       | 00007850 |
|    | GO TO 60  | 00007860 |
| C  | ZERO COSLT  | 00007870 |
| 11 | BETA = 0.0000                                     | 00007880 |
|    | GO TO 60  | 00007890 |
| C  | POSITIVE COSLT                                    | 00007900 |
| 12 | BETA = DATAN(COSLT)                               | 00007910 |
| C  | CALCULATION OF RE/ENTRY ANGLE(CLOCKWISE 0 TO 2PI) | 00007920 |
| 60 | GNUM = X(1)*XD(2)                                 | 00007930 |
|    | DCSB = DCOS(BETA)                                 | 00007940 |
|    | GDEM = XD(1)*DCSB                                 | 00007950 |
|    | IF(GDEM) 13,14,15                                 | 00007960 |
| C  | ZERO GDEM   | 00007970 |
| 14 | IF (GNUM) 16,17,18                                | 00007980 |
| C  | NEGATIVE GNUM                                     | 00007990 |
| 16 | ARSIN = TIHAPI                                    | 00008000 |
|    | GO TO 62  | 00008010 |
| C  | ZERO GNUM   | 00008020 |
| 17 | ARSIN = 1.001*PI                                  | 00008030 |
|    | GO TO 62  | 00008040 |
| C  | POSITIVE GNUM                                     | 00008050 |
| 18 | ARSIN = HALFPI                                    | 00008060 |
|    | GO TO 62  | 00008070 |
| C  | NEGATIVE GDEM                                     | 00008080 |
| 13 | IF (GNUM) 19,20,19                                | 00008090 |
| C  | NEGATIVE OR POSITIVE GNUM                         | 00008100 |
| 19 | ACTAG3 = GNUM/GDEM                                | 00008110 |
|    | ARSIN = PI+DATAN(ACTAG3)                          | 00008120 |
|    | GO TO 62  | 00008130 |
| C  | ZERO GNUM   | 00008140 |
| 20 | ARSIN = PI  | 00008150 |
|    | GO TO 62  | 00008160 |
| C  | POSITIVE GDEM                                     | 00008170 |
| 19 | IF (GNUM) 21,22,23                                | 00008180 |
| C  | NEGATIVE GNUM                                     | 00008190 |
| 21 | ACTAG3 = GNUM/GDEM                                | 00008200 |
|    | ARSIN=TWOPI + DATAN(ACTAG3)                       | 00008210 |
|    | GO TO 62  | 00008220 |
| C  | ZERO GNUM   | 00008230 |
| 22 | ARSIN = 0.000                                     | 00008240 |

```

      GO TO 62
C    POSITIVE GNUM
23   ACTAG3 = GNUM/GDEM
      ARSIN = DATAN(ACTAG3)
      GO TO 62
62   GAM = ARSIN
      GAM = GAM*EF
      ARRAY(11) = GAM
      BETA = BETA*EF
      ARRAY(12) = BETA
      IF(KZ.NE.1) GO TO 540
      IF(M.EQ.1) GO TO 190
      GO TO 640
540  IF(M.EQ.3) GO TO 190
640  CONTINUE
      WRITE(07) ARRAY
      GO TO 190
190  WRITE (02) ARRAY
190  CALL SAVE (-1)
200  RETURN
      END

```

```

00008250
00008260
00008270
00008280
00008290
00008300
00008310
00008320
00008330
00008340
00008350
00008360
00008370
00008380
00008390
00008400
00008410
00008420
00008430
00008440
00008450

```

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|   |          |
|---|----------|
| SUBROUTINE RKG(TO)  | 00008460 |
| DOUBLE PRECISION C,F,D,A,B,DEG,DXN,DXDX,DL,SAD,ABLE,BAKER | 00008470 |
| DOUBLE PRECISION X,XD,XDD                                 | 00008480 |
| DOUBLE PRECISION P,Q                                      | 00008490 |
| DIMENSION C(4), F(4), D(4), A(3),B(3)                     | 00008500 |
| COMMON /R57/ X(3),XD(3),XDD(3)                            | 00008510 |
| COMMON /ST/ P(3), Q(3)                                    | 00008520 |
| DATA C/0.5D0,.2928932188,1.707106781,.1666666667/         | 00008530 |
| DATA D/0.5D0,.2928932188,1.707106781,0.5D0/               | 00008540 |
| DATA F/2.0D0,1.0D0,1.0D0,2.0D0/                           | 00008550 |
| GF=57.295779513,82320876798155                            | 00008560 |
| DO 10 J=1,4   | 00008570 |
| CALL EOTNX  | 00008580 |
| DO 10 I=1,3   | 00008590 |
| A(I)=X(I)   | 00008600 |
| B(I)=XD(I)  | 00008610 |
| DXN=(A(I)-F(J)+3(I))*C(J)                                 | 00008620 |
| DXDX=(A(I)-F(J)+P(I))*C(J)                                | 00008630 |
| DL=TO*DXN   | 00008640 |
| X(I)=X(I)+DL  | 00008650 |
| XD(I)=XD(I)+TO*DXDX                                       | 00008660 |
| B(I)=Q(I)+3.0D0*DXN-D(J)*A(I)                             | 00008670 |
| 10 P(I)=P(I)+3.0D0*DXDX-D(J)*B(I)                         | 00008680 |
| SAD=X(3)-6.283185307179586476925287                       | 00008690 |
| IF ( SAD ) 12,11,11                                       | 00008700 |
| 11 X(3)=SAD   | 00008710 |
| 12 RETURN   | 00008720 |
| END   | 00008730 |

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|   |         |
|---|---------|
| ROUTINE INPUT   | 0008740 |
| COMMON/SW1/KZ   | 0008750 |
| COMMON/AX/TM,MT   | 0008760 |
| COMMON/IC/CA,BETA,GAM,HX,GLAM,THE,GLAMI,THEI              | 0008770 |
| COMMON/IC2/VO,INERTL                                      | 0008780 |
| COMMON/IC3/TMI  | 0008790 |
| *PARAM/ARRAY(20),MAX1,MAX2,SC1,SC2,ARRAY1(20)             | 0008800 |
| COMMON/THS/T,H,XYZ,RSL,PZ                                 | 0008810 |
| COMMON/PTURB/A(2),B(20),C(2)                              | 0008820 |
| COMMON/CONV/AH  | 0008830 |
| COMMON/NTRAJ/MM   | 0008840 |
| COMMON/EQATMO/ZK,KAT                                      | 0008850 |
| COMMON/CON/IK,JK  | 0008860 |
| COMMON/COEL/ELIM  | 0008870 |
| DOUBLE PRECISION TM,CA,BETA,GAM,HX                        | 0008880 |
| DOUBLE PRECISION TMI                                      | 0008890 |
| DOUBLE PRECISION A,B,C                                    | 0008900 |
| DOUBLE PRECISION SC1,SC2,AH                               | 0008910 |
| *ARRAY,ARRAY1   | 0008920 |
| DOUBLE PRECISION T,H,XYZ,RSL,PZ                           | 0008930 |
| DOUBLE PRECISION ZK                                       | 0008940 |
| DOUBLE PRECISION GLAM,THE,GLAMI,THEI                      | 0008950 |
| DOUBLE PRECISION VO                                       | 0008960 |
| DOUBLE PRECISION ELIM,EELIM                               | 0008970 |
| IK = 0  | 0008980 |
| JK = 10   | 0008990 |
| NAMelist/IN1/TM,TMI                                       | 0009000 |
| NAMelist/IN2/CA,BETA,GAM,HX                               | 0009010 |
| NAMelist/IN3/KZ   | 0009020 |
| NAMelist/IN4/ELIM   | 0009030 |
| *IN5/VO,INERTL  | 0009040 |
| NAMelist/IN6/ZK,KAT                                       | 0009050 |
| C KAT = 1 CALL ATMOSPHERE                                 | 0009060 |
| C KAT = 0 SET ATMOSPHERIC DENSITY = U                     | 0009070 |
| NAMelist/IN7/A,B,C,MM                                     | 0009080 |
| C MM EQUAL 3 GIVES NOMINAL TRAJECTORY                     | 0009090 |
| C MM GREATER THAN 3 GIVES MM-3 PERTURBED TRAJECTORIES     | 0009100 |
| NAMelist/IN8/SC1,SC2,AH                                   | 0009110 |
| NAMelist/IN9/GLAM,THE,GLAMI,THEI                          | 0009120 |
| C GLAM = LAUNCH LONGITUDE **AND** THE = LAUNCH LATITUDE   | 0009130 |
| C IN DEGREES  | 0009140 |
| C GLAMI = IMPACT LONGITUDE **AND** THEI = IMPACT LATITUDE | 0009150 |
| C IN DEGREES  | 0009160 |
| C FOR SOUTH LATITUDES USE A NEGATIVE THE OR THEI          | 0009170 |
| C SENSOR LONGITUDE MEASURED WEST OF GREENWICH, ALL OTHER  | 0009180 |
| C LONGITUDES ARE MEASURED WEST OF GREENWICH               | 0009190 |
| READ(5,IN1)   | 0009200 |
| IK=0  | 0009205 |
| JK=0  | 0009206 |
| READ(5,IN2)   | 0009210 |
| READ(5,IN3)   | 0009220 |
| READ(5,IN4)   | 0009230 |



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READ(5,IN5)                                00009240
READ(5,IN6)                                00009250
READ(5,IN7)                                00009260
READ(5,IN8)                                00009270
READ(5,IN9)                                00009280
EELIM = 90,000-EELIM                        00009290
WRITE(6,5)                                  00009300
WRITE(6,10) TM,TMI                           00009310
WRITE(6,20) CA,HX                             00009320
WRITE(6,30) BETA                             00009330
WRITE(6,40) GAM,VO,INERTL                     00009340
WRITE(6,50) ZK                                00009350
WRITE(6,53) KAT                               00009360
WRITE(6,140) KZ                              00009370
WRITE(6,54)                                  00009380
WRITE(6,55) MM                               00009390
WRITE(6,60)                                  00009400
WRITE(6,70)                                  00009410
WRITE(6,80) (A(VN),B(NN),C(NN),NN=1,20)      00009420
WRITE(6,90)                                  00009430
WRITE(6,100)                                 00009440
WRITE(6,110) SC1,SC2,AH                      00009450
WRITE(6,120) GLAM,THE                        00009460
WRITE(6,130) GLAMI,THEI                      00009470
WRITE(6,150) EELIM                           00009480
5 FORMAT(1H,55X,"INPUTS")                    00009490
10 FORMAT(1H,34H MAXIMUM RUN TIME (FORWARD) TM = ,D16.8,4HMIN,5X,300009500
*7H CUT-OFF TIME (BACKWARDS) TMI = ,D16.8,"MIN." 00009510
20 FORMAT(1H,21H SURFACE RANGE CA = ,D16.8,8H DEGREES,5X,16H ALTITU00009520
*DE HX = ,D16.8,5H FEET)                    00009530
30 FORMAT(1H,60H MISSILE HEADING ANGLE MEASURED CLOCKWISE FROM NORTH00009540
* BETA = ,D16.8,8H DEGREES)                  00009550
40 FORMAT(1H,22H REENTRY ANGLE GAM = ,D25.8,8H DEGREES,5X,24H INITI00009560
*AL VELOCITY VO = ,D25.18,7H FT/MIN,         00009570
*/50X,"INERTL = ",I3,5X,                     00009572
*/69X,"IF INERTL = ,INITIAL VELOCITY IS BURNOUT VELOCITY", 00009574
*/69X,"IF INERTL = 1,INITIAL VELOCITY IS INERTIAL VELOCITY") 00009576
50 FORMAT(1H,2X,54 ZK = ,D25.18,36H FT*2/SLUGS , BALLISTIC COEFFIC00009580
*ENT)                                         00009590
53 FORMAT(1H,7H KAT = ,I2,1X,55H NO ATMOSPHERE SET KAT = 0 , FOR AT00009600
*OSPHERE SET KAT = 1)                       00009610
54 FORMAT(1H,55H FOR CASE OF NO ATMOSPHERE, ATMOSPHERIC DENSITY PZ 00009620
* = 0)                                       00009630
55 FORMAT(1H,64H MM = ,I4)                   00009640
60 FORMAT(1H,45X,30H PERTURBED VELOCITY COMPONENTS) 00009650
70 FORMAT(1H,4X,30H PERTURBATION TO LEFT - FT/SEC,9X,32H PERTURBATI00009660
*ON BACKWARDS - FT/SEC,9X,30H PERTURBATION UPWARDS - FT/SEC) 00009670
80 FORMAT(1H,7X,D25.18,15X,D25.18,15X,D25.18) 00009680
90 FORMAT(1H,39X,41H SENSOR'S COORDINATES IN DEGREES AND FEET) 00009690
100 FORMAT(1H,10X,18H GEODETIC LATITUDE,12X,38H LONGITUDE, WEST OF GRO00009700
*BENWICH MERIDIAN,8X,25H ALTITUDE ABOVE SEA-LEVEL) 00009710
110 FORMAT(1H,7X,3(D25.18,15X))              00009720

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120 FORMAT(1H0,20H LAUNCH LONGITUDE = ,D25.18,5X,12H LATITUDE = ,D25.100019730
*8) 00019740
130 FORMAT(1H0,20H IMPACT LONGITUDE = ,D25.18,5X,12H LATITUDE = ,D25.100009750
*8) 00019760
140 FORMAT(1H0,1X,5H KZ = ,I5) 00019770
150 FORMAT(1H,4X,35H LOWEST ELEVATION ANGLE PRINTED OUT = ,D12.4) 00019780
RETURN 00019790
END 00019800
```

Listing of the Sample Input for the Program





Sample Output for the Cobra Talon Trajectory Program

| TIME   | RADIUS       | LATITUDE   | LONGITUDE    | HEIGHT       | VELOCITY     | RISSE LEVEL  | DENSITY |
|--------|--------------|------------|--------------|--------------|--------------|--------------|---------|
| 0.     | 0.2132564000 | 0.42580000 | 0.1270000000 | 0.4000000000 | 0.1668343392 | 0.2092564000 | 0.      |
| 0.1000 | 0.2138580280 | 0.42531900 | 0.1266885070 | 0.4601620800 | 0.1657175872 | 0.2092564000 | 0.      |
| 0.2000 | 0.2144515120 | 0.42506910 | 0.1263785240 | 0.5195114750 | 0.1645146976 | 0.2092564000 | 0.      |
| 0.3000 | 0.2150451520 | 0.42503500 | 0.1260694250 | 0.5780018590 | 0.1632555792 | 0.2092564000 | 0.      |
| 0.4000 | 0.2156142580 | 0.42623330 | 0.1257617880 | 0.6357868350 | 0.1624501440 | 0.2092564000 | 0.      |
| 0.5000 | 0.2161836000 | 0.42657770 | 0.1254519000 | 0.6927199480 | 0.1613883020 | 0.2092564000 | 0.      |
| 0.6000 | 0.2167449470 | 0.42687870 | 0.1251502060 | 0.7488346490 | 0.1603999200 | 0.2092564000 | 0.      |
| 0.7000 | 0.2172983420 | 0.42715160 | 0.1248462160 | 0.8041943420 | 0.1593051280 | 0.2092564000 | 0.      |
| 0.8000 | 0.2178438240 | 0.42731130 | 0.1245433950 | 0.8587423420 | 0.1582633680 | 0.2092564000 | 0.      |
| 0.9000 | 0.2183814280 | 0.42756320 | 0.1242417240 | 0.9125019130 | 0.1572756480 | 0.2092564000 | 0.      |
| 1.0000 | 0.2189111560 | 0.42780720 | 0.1239411840 | 0.9654762620 | 0.1562805340 | 0.2092564000 | 0.      |
| 1.1000 | 0.2194339480 | 0.42804340 | 0.1236417480 | 0.1017468480 | 0.1552882080 | 0.2092564000 | 0.      |
| 1.2000 | 0.2199472160 | 0.42827300 | 0.1233430110 | 0.1069881680 | 0.1543302440 | 0.2092564000 | 0.      |
| 1.3000 | 0.2204535920 | 0.42849320 | 0.1230461210 | 0.1119118810 | 0.1533747696 | 0.2092564000 | 0.      |
| 1.4000 | 0.2209522720 | 0.42870690 | 0.1227498880 | 0.1169582860 | 0.1524323456 | 0.2092564000 | 0.      |
| 1.5000 | 0.2214431680 | 0.42891320 | 0.1224546830 | 0.1218676680 | 0.1515293920 | 0.2092564000 | 0.      |
| 1.6000 | 0.2219264320 | 0.42911240 | 0.1221654860 | 0.1267003100 | 0.1506550880 | 0.2092564000 | 0.      |
| 1.7000 | 0.2224024800 | 0.42930450 | 0.1218672810 | 0.1314564880 | 0.1498030256 | 0.2092564000 | 0.      |
| 1.8000 | 0.2228704800 | 0.42948950 | 0.1215750460 | 0.1361364720 | 0.1489924592 | 0.2092564000 | 0.      |
| 1.9000 | 0.2233304510 | 0.42966750 | 0.1212837660 | 0.1407405280 | 0.1479478940 | 0.2092564000 | 0.      |
| 2.0000 | 0.2237832280 | 0.42983870 | 0.1209934220 | 0.1452889130 | 0.1470499760 | 0.2092564000 | 0.      |
| 2.1000 | 0.2242285980 | 0.43001010 | 0.1207039950 | 0.1497218830 | 0.1461980208 | 0.2092564000 | 0.      |
| 2.2000 | 0.2246663580 | 0.43016190 | 0.1204154700 | 0.1540499680 | 0.1453588920 | 0.2092564000 | 0.      |
| 2.3000 | 0.2250966560 | 0.43031200 | 0.1201278280 | 0.1584325630 | 0.1445325940 | 0.2092564000 | 0.      |
| 2.4000 | 0.2255194750 | 0.43046350 | 0.1198410540 | 0.1626307530 | 0.1437191120 | 0.2092564000 | 0.      |
| 2.5000 | 0.2259348480 | 0.43059460 | 0.1195551310 | 0.1667844890 | 0.1429164340 | 0.2092564000 | 0.      |
| 2.6000 | 0.2263428000 | 0.43072630 | 0.1192700410 | 0.1708639960 | 0.1421305540 | 0.2092564000 | 0.      |
| 2.7000 | 0.2267435400 | 0.43085170 | 0.1189857110 | 0.1748650500 | 0.1413554700 | 0.2092564000 | 0.      |
| 2.8000 | 0.2271365210 | 0.43097180 | 0.1187023040 | 0.1788012170 | 0.1405931980 | 0.2092564000 | 0.      |
| 2.9000 | 0.2275223360 | 0.43118370 | 0.1184196220 | 0.1826593580 | 0.1398437280 | 0.2092564000 | 0.      |
| 3.0000 | 0.2279003120 | 0.43139150 | 0.1181377130 | 0.1864441320 | 0.1391170736 | 0.2092564000 | 0.      |
| 3.1000 | 0.2282717440 | 0.43159120 | 0.1178555610 | 0.1901557420 | 0.1383832420 | 0.2092564000 | 0.      |
| 3.2000 | 0.2286358400 | 0.43178590 | 0.1175761500 | 0.1937943850 | 0.1376722464 | 0.2092564000 | 0.      |
| 3.3000 | 0.2289924250 | 0.43197470 | 0.1172964670 | 0.1973302560 | 0.1369740992 | 0.2092564000 | 0.      |
| 3.4000 | 0.2293411530 | 0.43215750 | 0.1170174960 | 0.2008935440 | 0.1362888140 | 0.2092564000 | 0.      |
| 3.5000 | 0.2296838320 | 0.43233450 | 0.1167372220 | 0.2042744300 | 0.1356164128 | 0.2092564000 | 0.      |
| 3.6000 | 0.2300187140 | 0.43250580 | 0.1164616330 | 0.2076230990 | 0.1349569120 | 0.2092564000 | 0.      |
| 3.7000 | 0.2303463710 | 0.43267130 | 0.1161847130 | 0.2108997230 | 0.1343103360 | 0.2092564000 | 0.      |
| 3.8000 | 0.2306664800 | 0.43283110 | 0.1159084510 | 0.2141644750 | 0.1336767020 | 0.2092564000 | 0.      |
| 3.9000 | 0.2309801530 | 0.43298530 | 0.1156363800 | 0.2173752000 | 0.1330560496 | 0.2092564000 | 0.      |
| 4.0000 | 0.2312863080 | 0.43313380 | 0.1153578380 | 0.2202990240 | 0.1324483940 | 0.2092564000 | 0.      |
| 4.1000 | 0.2315853150 | 0.43327690 | 0.1150834620 | 0.2232891420 | 0.1318537608 | 0.2092564000 | 0.      |
| 4.2000 | 0.2318773030 | 0.43341440 | 0.1148068860 | 0.2262800280 | 0.1312721840 | 0.2092564000 | 0.      |
| 4.3000 | 0.2321619340 | 0.43354650 | 0.1145355040 | 0.2292858330 | 0.1307036960 | 0.2092564000 | 0.      |
| 4.4000 | 0.2324396740 | 0.43367310 | 0.1142638960 | 0.2323183200 | 0.1301483280 | 0.2092564000 | 0.      |
| 4.5000 | 0.2327102840 | 0.43379440 | 0.1139918520 | 0.2353587840 | 0.1296061104 | 0.2092564000 | 0.      |
| 4.6000 | 0.2329732930 | 0.43391130 | 0.1137203600 | 0.2377420800 | 0.1290770800 | 0.2092564000 | 0.      |
| 4.7000 | 0.2332301440 | 0.43402100 | 0.1134494060 | 0.2397991070 | 0.1285612740 | 0.2092564000 | 0.      |
| 4.8000 | 0.2334797320 | 0.43412630 | 0.1131789790 | 0.2422336190 | 0.1280587180 | 0.2092564000 | 0.      |
| 4.9000 | 0.2337221350 | 0.43421640 | 0.1129006550 | 0.2446578650 | 0.1275694560 | 0.2092564000 | 0.      |
| 5.0000 | 0.2339579690 | 0.43429130 | 0.1126365640 | 0.2470119680 | 0.1270932640 | 0.2092564000 | 0.      |
| 5.1000 | 0.2341860320 | 0.43435110 | 0.1123707320 | 0.2492960440 | 0.1266309632 | 0.2092564000 | 0.      |

| TIME    | RADIUS           | LATITUDE      | LONGITUDE        | HEIGHT          | VELOCITY          | R (SEA LEVEL)    | DENSITY |
|---------|------------------|---------------|------------------|-----------------|-------------------|------------------|---------|
| 5.2000  | 0.23440742080    | 0.432 9560 02 | 0.1121022910 03  | 0.2515102110 07 | 0.12618180320 05  | 0.20925640000 08 | 0.      |
| 5.3000  | 0.23462185920 08 | 0.432 7510 02 | 0.11183343130 03 | 0.2536545790 07 | 0.12574608840 05  | 0.20925640000 08 | 0.      |
| 5.4000  | 0.23482912480 08 | 0.432 4950 02 | 0.1115667920 03  | 0.2557292570 07 | 0.12533384860 05  | 0.20925640000 08 | 0.      |
| 5.5000  | 0.23502983360 08 | 0.432 1880 02 | 0.1112997130 03  | 0.2577343420 07 | 0.12494513120 05  | 0.20925640000 08 | 0.      |
| 5.6000  | 0.23522339520 08 | 0.43198310 02 | 0.1110330670 03  | 0.2596699420 07 | 0.12451996960 05  | 0.20925640000 08 | 0.      |
| 5.7000  | 0.2354101160 08  | 0.43194340 02 | 0.1107668400 03  | 0.2615361470 07 | 0.12413840160 05  | 0.20925640000 08 | 0.      |
| 5.8000  | 0.23558970560 08 | 0.43188670 02 | 0.1105010220 03  | 0.2633330520 07 | 0.1237704680 05   | 0.20925640000 08 | 0.      |
| 5.9000  | 0.23576247360 08 | 0.43184600 02 | 0.1102335030 03  | 0.2650607420 07 | 0.12341619680 05  | 0.20925640000 08 | 0.      |
| 6.0000  | 0.23592832960 08 | 0.43179030 02 | 0.1099705710 03  | 0.266793080 07  | 0.12307563360 05  | 0.20925640000 08 | 0.      |
| 6.1000  | 0.23608738320 08 | 0.43172980 02 | 0.1097059130 03  | 0.2683868320 07 | 0.12274881360 05  | 0.20925640000 08 | 0.      |
| 6.2000  | 0.23623933760 08 | 0.43166430 02 | 0.1094416220 03  | 0.2698293850 07 | 0.12243576960 05  | 0.20925640000 08 | 0.      |
| 6.3000  | 0.23638430560 08 | 0.43159400 02 | 0.1091776830 03  | 0.2712810460 07 | 0.12213653760 05  | 0.20925640000 08 | 0.      |
| 6.4000  | 0.2365227740 08  | 0.43151870 02 | 0.1089140880 03  | 0.2726638880 07 | 0.1218115440 05   | 0.20925640000 08 | 0.      |
| 6.5000  | 0.23665419840 08 | 0.43143860 02 | 0.1086508250 03  | 0.2739779740 07 | 0.12157264320 05  | 0.20925640000 08 | 0.      |
| 6.6000  | 0.2367817360 08  | 0.43135370 02 | 0.108388840 03   | 0.2752233760 07 | 0.12133204480 05  | 0.20925640000 08 | 0.      |
| 6.7000  | 0.2368964160 08  | 0.43126390 02 | 0.1081252540 03  | 0.2764011440 07 | 0.12107838720 05  | 0.20925640000 08 | 0.      |
| 6.8000  | 0.2370073520 08  | 0.43116930 02 | 0.1078692240 03  | 0.2775833450 07 | 0.12084870240 05  | 0.20925640000 08 | 0.      |
| 6.9000  | 0.23711120320 08 | 0.43107000 02 | 0.1076008840 03  | 0.2785480250 07 | 0.12063301440 05  | 0.20925640000 08 | 0.      |
| 7.0000  | 0.23720832320 08 | 0.43096580 02 | 0.1073391250 03  | 0.2795192410 07 | 0.12043135360 05  | 0.20925640000 08 | 0.      |
| 7.1000  | 0.23729860480 08 | 0.43085680 02 | 0.1070776340 03  | 0.2804220380 07 | 0.1202377440 05   | 0.20925640000 08 | 0.      |
| 7.2000  | 0.2373824480 08  | 0.43074300 02 | 0.1068184030 03  | 0.2812584600 07 | 0.1200702960 05   | 0.20925640000 08 | 0.      |
| 7.3000  | 0.2374586560 08  | 0.43062450 02 | 0.1065554200 03  | 0.2820225470 07 | 0.11991077440 05  | 0.20925640000 08 | 0.      |
| 7.4000  | 0.23752843520 08 | 0.43050120 02 | 0.1062946750 03  | 0.2827203360 07 | 0.11974545760 05  | 0.20925640000 08 | 0.      |
| 7.5000  | 0.23759139560 08 | 0.43037310 02 | 0.1060341580 03  | 0.2833486620 07 | 0.11958427840 05  | 0.20925640000 08 | 0.      |
| 7.6000  | 0.2376471680 08  | 0.43024030 02 | 0.1057738600 03  | 0.2839111520 07 | 0.11941725440 05  | 0.20925640000 08 | 0.      |
| 7.7000  | 0.23769682240 08 | 0.43010270 02 | 0.1055137690 03  | 0.2844042360 07 | 0.11924440320 05  | 0.20925640000 08 | 0.      |
| 7.8000  | 0.2377431520 08  | 0.42996140 02 | 0.1052538760 03  | 0.2848213390 07 | 0.11907537360 05  | 0.20925640000 08 | 0.      |
| 7.9000  | 0.23777438880 08 | 0.42981330 02 | 0.1049941710 03  | 0.2851858780 07 | 0.11891212620 05  | 0.20925640000 08 | 0.      |
| 8.0000  | 0.23780334640 08 | 0.42966150 02 | 0.1047346440 03  | 0.2854744730 07 | 0.11874100480 05  | 0.20925640000 08 | 0.      |
| 8.1000  | 0.23782589440 08 | 0.42950500 02 | 0.1044752840 03  | 0.2856949400 07 | 0.11857449540 05  | 0.20925640000 08 | 0.      |
| 8.2000  | 0.23784112960 08 | 0.42934360 02 | 0.1042160820 03  | 0.2858472830 07 | 0.11841313440 05  | 0.20925640000 08 | 0.      |
| 8.3000  | 0.2378495320 08  | 0.42917760 02 | 0.1039570280 03  | 0.2859315130 07 | 0.11825553760 05  | 0.20925640000 08 | 0.      |
| 8.4000  | 0.23785115480 08 | 0.42900680 02 | 0.1036981110 03  | 0.2859476380 07 | 0.11809216960 05  | 0.20925640000 08 | 0.      |
| 8.5000  | 0.23784595480 08 | 0.42883120 02 | 0.1034393220 03  | 0.2858956510 07 | 0.11793030340 05  | 0.20925640000 08 | 0.      |
| 8.6000  | 0.23783395520 08 | 0.42865180 02 | 0.1031806510 03  | 0.2857755550 07 | 0.11776811840 05  | 0.20925640000 08 | 0.      |
| 8.7000  | 0.23781513290 08 | 0.42846570 02 | 0.1029220880 03  | 0.2855873440 07 | 0.11761574320 05  | 0.20925640000 08 | 0.      |
| 8.8000  | 0.2377895080 08  | 0.42827580 02 | 0.1026636240 03  | 0.2853310040 07 | 0.11746730080 05  | 0.20925640000 08 | 0.      |
| 8.9000  | 0.2377575290 08  | 0.42808110 02 | 0.1024052470 03  | 0.2850095310 07 | 0.117328870880 05 | 0.20925640000 08 | 0.      |
| 9.0000  | 0.2377179880 08  | 0.42788170 02 | 0.1021465480 03  | 0.2846139000 07 | 0.11719306500 05  | 0.20925640000 08 | 0.      |
| 9.1000  | 0.23767170880 08 | 0.42767740 02 | 0.1018887180 03  | 0.284139000 07  | 0.11706679360 05  | 0.20925640000 08 | 0.      |
| 9.2000  | 0.23761830960 08 | 0.42746830 02 | 0.1016305470 03  | 0.2836241020 07 | 0.11693710880 05  | 0.20925640000 08 | 0.      |
| 9.3000  | 0.2375593880 08  | 0.42725440 02 | 0.1013724240 03  | 0.2830268860 07 | 0.11677158880 05  | 0.20925640000 08 | 0.      |
| 9.4000  | 0.2374928490 08  | 0.42703560 02 | 0.1011143400 03  | 0.2823614200 07 | 0.11660211440 05  | 0.20925640000 08 | 0.      |
| 9.5000  | 0.2374191580 08  | 0.42681200 02 | 0.1008562840 03  | 0.2816276730 07 | 0.11643296800 05  | 0.20925640000 08 | 0.      |
| 9.6000  | 0.2373389630 08  | 0.42658350 02 | 0.1005982480 03  | 0.2808256090 07 | 0.11626598340 05  | 0.20925640000 08 | 0.      |
| 9.7000  | 0.2372519200 08  | 0.4263510 02  | 0.1003402200 03  | 0.2799551900 07 | 0.11609777200 05  | 0.20925640000 08 | 0.      |
| 9.8000  | 0.2371583840 08  | 0.42611190 02 | 0.1000841910 03  | 0.2790163710 07 | 0.11592579040 05  | 0.20925640000 08 | 0.      |
| 9.9000  | 0.2370573120 08  | 0.42586870 02 | 0.9998241500 02  | 0.2780091100 07 | 0.11574484000 05  | 0.20925640000 08 | 0.      |
| 10.0000 | 0.23694973440 08 | 0.42562160 02 | 0.9995660890 02  | 0.2769333560 07 | 0.11556790340 05  | 0.20925640000 08 | 0.      |
| 10.1000 | 0.23683530560 08 | 0.42536750 02 | 0.99930799740 02 | 0.2757890560 07 | 0.11538449420 05  | 0.20925640000 08 | 0.      |
| 10.2000 | 0.2367141600 08  | 0.42510950 02 | 0.99904986360 02 | 0.2745761560 07 | 0.115195594880 05 | 0.20925640000 08 | 0.      |
| 10.3000 | 0.23658585920 08 | 0.42484640 02 | 0.9897916780 02  | 0.2732945980 07 | 0.11500787320 05  | 0.20925640000 08 | 0.      |



| TIME    | RADIUS           | LATITUDE      | LONGITUDE       | HEIGHT          | VELOCITY          | RISEA LEVEL     | DENSITY |
|---------|------------------|---------------|-----------------|-----------------|-------------------|-----------------|---------|
| 10.4000 | 0.2364508320 08  | 0.42457840 02 | 0.9853343230 02 | 0.2719443160 07 | 0.1299969600 05   | 0.2092564000 08 | 0.0     |
| 10.5000 | 0.2363892480 08  | 0.42305050 02 | 0.9827511120 02 | 0.2705252440 07 | 0.1229237760 05   | 0.2092564000 08 | 0.0     |
| 10.6000 | 0.23610013120 08 | 0.42427120 02 | 0.9801671350 02 | 0.2690373150 07 | 0.1225988960 05   | 0.2092564000 08 | 0.0     |
| 10.7000 | 0.2360044480 08  | 0.42374380 02 | 0.9775822330 02 | 0.2674804570 07 | 0.1229198880 05   | 0.2092564000 08 | 0.0     |
| 10.8000 | 0.23584185320 08 | 0.42345540 02 | 0.9749962880 02 | 0.2658545580 07 | 0.1225334960 05   | 0.2092564000 08 | 0.0     |
| 10.9000 | 0.2356233480 08  | 0.42316190 02 | 0.9724092280 02 | 0.2641596350 07 | 0.12360103360 05  | 0.2092564000 08 | 0.0     |
| 11.0000 | 0.2354959520 08  | 0.42286310 02 | 0.9698209280 02 | 0.2623955070 07 | 0.1239620400 05   | 0.2092564000 08 | 0.0     |
| 11.1000 | 0.23531261120 08 | 0.42255920 02 | 0.9673129600 02 | 0.2605621140 07 | 0.1233732240 05   | 0.2092564000 08 | 0.0     |
| 11.2000 | 0.2351233320 08  | 0.42225500 02 | 0.9648402170 02 | 0.2586593320 07 | 0.1237265360 05   | 0.2092564000 08 | 0.0     |
| 11.3000 | 0.2349325120 08  | 0.42193560 02 | 0.9620476330 02 | 0.2566872160 07 | 0.12412885760 05  | 0.2092564000 08 | 0.0     |
| 11.4000 | 0.23474095120 08 | 0.42161580 02 | 0.9594533370 02 | 0.2546454970 07 | 0.1245449920 05   | 0.2092564000 08 | 0.0     |
| 11.5000 | 0.23451981440 08 | 0.42129070 02 | 0.9569573150 02 | 0.2525341170 07 | 0.1249733400 05   | 0.2092564000 08 | 0.0     |
| 11.6000 | 0.2342917040 08  | 0.42096720 02 | 0.9543594440 02 | 0.2503330300 07 | 0.1254168400 05   | 0.2092564000 08 | 0.0     |
| 11.7000 | 0.2340666800 08  | 0.42062430 02 | 0.9516595320 02 | 0.2481020640 07 | 0.12587286240 05  | 0.2092564000 08 | 0.0     |
| 11.8000 | 0.23383451120 08 | 0.42028290 02 | 0.9490575870 02 | 0.2457811190 07 | 0.12634246880 05  | 0.2092564000 08 | 0.0     |
| 11.9000 | 0.23359541120 08 | 0.41993610 02 | 0.9464534440 02 | 0.2433901180 07 | 0.1268252240 05   | 0.2092564000 08 | 0.0     |
| 12.0000 | 0.2333492960 08  | 0.41958330 02 | 0.9438469880 02 | 0.2409288800 07 | 0.12732186640 05  | 0.2092564000 08 | 0.0     |
| 12.1000 | 0.23309613120 08 | 0.41922570 02 | 0.9412381190 02 | 0.2383973180 07 | 0.12783125560 05  | 0.2092564000 08 | 0.0     |
| 12.2000 | 0.23283592360 08 | 0.41886210 02 | 0.9386267130 02 | 0.2357953320 07 | 0.1283540000 05   | 0.2092564000 08 | 0.0     |
| 12.3000 | 0.23256866880 08 | 0.41849280 02 | 0.9360126840 02 | 0.2329122610 07 | 0.1288997920 05   | 0.2092564000 08 | 0.0     |
| 12.4000 | 0.2322943360 08  | 0.41811780 02 | 0.9333958910 02 | 0.2303793330 07 | 0.12943912480 05  | 0.2092564000 08 | 0.0     |
| 12.5000 | 0.23201291320 08 | 0.41773710 02 | 0.9307762170 02 | 0.2275651480 07 | 0.1300110480 05   | 0.2092564000 08 | 0.0     |
| 12.6000 | 0.2317433260 08  | 0.41735050 02 | 0.9281535740 02 | 0.2246799320 07 | 0.1305768880 05   | 0.2092564000 08 | 0.0     |
| 12.7000 | 0.2314287520 08  | 0.41695810 02 | 0.9255278200 02 | 0.2217235580 07 | 0.13116584160 05  | 0.2092564000 08 | 0.0     |
| 12.8000 | 0.23112599720 08 | 0.41655970 02 | 0.9228988280 02 | 0.2186958720 07 | 0.1317654160 05   | 0.2092564000 08 | 0.0     |
| 12.9000 | 0.2308167740 08  | 0.41615540 02 | 0.9202665680 02 | 0.2155967160 07 | 0.13238114320 05  | 0.2092564000 08 | 0.0     |
| 13.0000 | 0.23049892320 08 | 0.41574510 02 | 0.9176307200 02 | 0.2124259340 07 | 0.1330083440 05   | 0.2092564000 08 | 0.0     |
| 13.1000 | 0.2301747360 08  | 0.41532860 02 | 0.9149913470 02 | 0.2091833380 07 | 0.1336491640 05   | 0.2092564000 08 | 0.0     |
| 13.2000 | 0.22984329320 08 | 0.41490600 02 | 0.9123482750 02 | 0.2058688200 07 | 0.1343026680 05   | 0.2092564000 08 | 0.0     |
| 13.3000 | 0.22951461440 08 | 0.41447720 02 | 0.9097013500 02 | 0.2024821470 07 | 0.1349686640 05   | 0.2092564000 08 | 0.0     |
| 13.4000 | 0.2291597180 08  | 0.41404220 02 | 0.9070504830 02 | 0.1990203180 07 | 0.1356485280 05   | 0.2092564000 08 | 0.0     |
| 13.5000 | 0.2288055580 08  | 0.41360080 02 | 0.9043955070 02 | 0.1954916760 07 | 0.1363401120 05   | 0.2092564000 08 | 0.0     |
| 13.6000 | 0.2284451320 08  | 0.41315330 02 | 0.9017363320 02 | 0.1918875100 07 | 0.13704502720 05  | 0.2092564000 08 | 0.0     |
| 13.7000 | 0.2280774440 08  | 0.41269830 02 | 0.8990728160 02 | 0.1882104700 07 | 0.1377622840 05   | 0.2092564000 08 | 0.0     |
| 13.8000 | 0.2277024320 08  | 0.41223780 02 | 0.8964047870 02 | 0.1844603600 07 | 0.1384933680 05   | 0.2092564000 08 | 0.0     |
| 13.9000 | 0.2273209920 08  | 0.41177150 02 | 0.8937321720 02 | 0.1806369790 07 | 0.139240267120 05 | 0.2092564000 08 | 0.0     |
| 14.0000 | 0.2269304120 08  | 0.41129640 02 | 0.8910547960 02 | 0.1767401330 07 | 0.1400029840 05   | 0.2092564000 08 | 0.0     |
| 14.1000 | 0.2265333560 08  | 0.41081540 02 | 0.8883725440 02 | 0.1727695900 07 | 0.1407762000 05   | 0.2092564000 08 | 0.0     |
| 14.2000 | 0.2261289120 08  | 0.41032790 02 | 0.8856852600 02 | 0.1687251360 07 | 0.1415584000 05   | 0.2092564000 08 | 0.0     |
| 14.3000 | 0.2257173600 08  | 0.40983330 02 | 0.8829928660 02 | 0.1646065710 07 | 0.1423384400 05   | 0.2092564000 08 | 0.0     |
| 14.4000 | 0.2252977560 08  | 0.40933170 02 | 0.8802950500 02 | 0.1604136590 07 | 0.1431145640 05   | 0.2092564000 08 | 0.0     |
| 14.5000 | 0.2248611160 08  | 0.40882300 02 | 0.8775918460 02 | 0.1561461710 07 | 0.1438860960 05   | 0.2092564000 08 | 0.0     |
| 14.6000 | 0.2244367920 08  | 0.40830720 02 | 0.8748830330 02 | 0.1518038700 07 | 0.1446660960 05   | 0.2092564000 08 | 0.0     |
| 14.7000 | 0.2239950520 08  | 0.40778410 02 | 0.8721684730 02 | 0.1473865180 07 | 0.1454464520 05   | 0.2092564000 08 | 0.0     |
| 14.8000 | 0.2235457960 08  | 0.40725350 02 | 0.8694480120 02 | 0.1428938680 07 | 0.1462268000 05   | 0.2092564000 08 | 0.0     |
| 14.9000 | 0.2230895640 08  | 0.40671570 02 | 0.8667214870 02 | 0.1383256700 07 | 0.1470080000 05   | 0.2092564000 08 | 0.0     |
| 15.0000 | 0.2226245640 08  | 0.40617730 02 | 0.8639887740 02 | 0.1338256700 07 | 0.1477901920 05   | 0.2092564000 08 | 0.0     |
| 15.1000 | 0.2221525000 08  | 0.40561720 02 | 0.8612496680 02 | 0.1293816590 07 | 0.1485725840 05   | 0.2092564000 08 | 0.0     |
| 15.2000 | 0.2216729180 08  | 0.40505640 02 | 0.8585040660 02 | 0.1241651880 07 | 0.1493549560 05   | 0.2092564000 08 | 0.0     |
| 15.3000 | 0.2211956160 08  | 0.40448780 02 | 0.8557517360 02 | 0.1192921740 07 | 0.1501374800 05   | 0.2092564000 08 | 0.0     |
| 15.4000 | 0.22070962720 08 | 0.40391120 02 | 0.8529925950 02 | 0.1143422720 07 | 0.1509200560 05   | 0.2092564000 08 | 0.0     |
| 15.5000 | 0.2202187920 08  | 0.40332660 02 | 0.8502264060 02 | 0.1093151950 07 | 0.15169265280 05  | 0.2092564000 08 | 0.0     |



| TIME    | RADIUS           | LATITUDE      | LONGITUDE       | HEIGHT          | VELOCITY         | R (SEA LEVEL)    | DENSITY       |
|---------|------------------|---------------|-----------------|-----------------|------------------|------------------|---------------|
| 15.6800 | 0.2196774556D 08 | 0.4027337D 02 | 0.847453017D 02 | 0.104210654D 07 | 0.1548386224D 05 | 0.2092564000D 08 | 0.            |
| 15.7000 | 0.2191592352D 08 | 0.4021332D 02 | 0.844672262D 02 | 0.990283520D 06 | 0.1558171136D 05 | 0.2092564000D 08 | 0.            |
| 15.8000 | 0.2186332070D 08 | 0.4015233D 02 | 0.841883961D 02 | 0.937679946D 06 | 0.1568027776D 05 | 0.2092564000D 08 | 0.            |
| 15.9000 | 0.2180993244D 08 | 0.4009040D 02 | 0.838087939D 02 | 0.884292441D 06 | 0.1578046704D 05 | 0.2092564000D 08 | 0.            |
| 16.0000 | 0.2175575880D 08 | 0.4002780D 02 | 0.834583967D 02 | 0.830118112D 06 | 0.1588198464D 05 | 0.2092564000D 08 | 0.            |
| 16.1000 | 0.2170793600D 08 | 0.3996420D 02 | 0.833471948D 02 | 0.773153844D 06 | 0.1598485712D 05 | 0.2092564000D 08 | 0.            |
| 16.2000 | 0.2164503984D 08 | 0.3989980D 02 | 0.830951628D 02 | 0.719395756D 06 | 0.1608903104D 05 | 0.2092564000D 08 | 0.            |
| 16.3000 | 0.2158048096D 08 | 0.3983448D 02 | 0.827822832D 02 | 0.662841168D 06 | 0.1619457360D 05 | 0.2092564000D 08 | 0.            |
| 16.4000 | 0.2153126880D 08 | 0.3976821D 02 | 0.824985337D 02 | 0.605486163D 06 | 0.1630147232D 05 | 0.2092564000D 08 | 0.            |
| 16.5000 | 0.2147967920D 08 | 0.3970110D 02 | 0.822138976D 02 | 0.547327539D 06 | 0.1640973520D 05 | 0.2092564000D 08 | 0.            |
| 16.6000 | 0.214140150D 08  | 0.3963280D 02 | 0.819283532D 02 | 0.488366119D 06 | 0.1651937104D 05 | 0.2092564000D 08 | 0.            |
| 16.7000 | 0.213542240D 08  | 0.3956370D 02 | 0.81618796D 02  | 0.429584761D 06 | 0.1663038880D 05 | 0.2092564000D 08 | 0.            |
| 16.8000 | 0.2129363380D 08 | 0.3949364D 02 | 0.813344556D 02 | 0.367993348D 06 | 0.1674279888D 05 | 0.2092564000D 08 | 0.            |
| 16.9000 | 0.2123222336D 08 | 0.3942255D 02 | 0.810560595D 02 | 0.309583312D 06 | 0.1685656592D 05 | 0.2092564000D 08 | 0.2662197D-08 |

| TIME   | R-DOT            | LAT.-DOT       | LONG.-DOT      | R-DOT DOT        | LAT.-DOT DOT   | LONG.-DOT DOT |
|--------|------------------|----------------|----------------|------------------|----------------|---------------|
| 0.     | 0.10949453D 05   | 0.539180D-02   | -0.520259D-01  | -0.226787923D 02 | -0.2500639D-04 | 0.3704917D-04 |
| 0.1000 | 0.095918643D 04  | 0.524197D-02   | -0.518057D-01  | -0.225745155D 02 | -0.246048D-04  | 0.363649D-04  |
| 0.2000 | 0.082404592D 04  | 0.519552D-02   | -0.515895D-01  | -0.22473164D 02  | -0.2421372D-04 | 0.356940D-04  |
| 0.3000 | 0.068951449D 04  | 0.495138D-02   | -0.513773D-01  | -0.223721555D 02 | -0.238345D-04  | 0.350361D-04  |
| 0.4000 | 0.05555778D 04   | 0.46949D-02    | -0.51169D-01   | -0.222739958D 02 | -0.234665D-04  | 0.343908D-04  |
| 0.5000 | 0.04222227D 04   | 0.446977D-02   | -0.509646D-01  | -0.221778006D 02 | -0.231083D-04  | 0.337578D-04  |
| 0.6000 | 0.028943961D 04  | 0.423163D-02   | -0.507635D-01  | -0.220835344D 02 | -0.2276193D-04 | 0.333664D-04  |
| 0.7000 | 0.015721551D 04  | 0.399661D-02   | -0.505669D-01  | -0.219911625D 02 | -0.224245D-04  | 0.329695D-04  |
| 0.8000 | 0.002534188D 04  | 0.376305D-02   | -0.503738D-01  | -0.219006521D 02 | -0.2209687D-04 | 0.31284D-04   |
| 0.9000 | 0.088944499D 04  | 0.35142D-02    | -0.501838D-01  | -0.218119705D 02 | -0.217769D-04  | 0.31407D-04   |
| 1.0000 | 0.076379468D 04  | 0.32737D-02    | -0.499975D-01  | -0.217250857D 02 | -0.214695D-04  | 0.309655D-04  |
| 1.1000 | 0.06337048D 04   | 0.30377D-02    | -0.49814D-01   | -0.216399476D 02 | -0.2116936D-04 | 0.306394D-04  |
| 1.2000 | 0.050411161D 04  | 0.279763D-02   | -0.496351D-01  | -0.215565862D 02 | -0.208787D-04  | 0.299292D-04  |
| 1.3000 | 0.037501798D 04  | 0.256232D-02   | -0.494585D-01  | -0.214743123D 02 | -0.205952D-04  | 0.292043D-04  |
| 1.4000 | 0.02464934D 04   | 0.232747D-02   | -0.492860D-01  | -0.213949182D 02 | -0.203207D-04  | 0.28539D-04   |
| 1.5000 | 0.011827564D 04  | 0.209335D-02   | -0.491162D-01  | -0.213165764D 02 | -0.200530D-04  | 0.28248D-04   |
| 1.6000 | 0.09906715D 04   | 0.185982D-02   | -0.489496D-01  | -0.212398604D 02 | -0.197937D-04  | 0.279293D-04  |
| 1.7000 | 0.078339411D 04  | 0.16248D-02    | -0.487862D-01  | -0.211647443D 02 | -0.195413D-04  | 0.276092D-04  |
| 1.8000 | 0.05736327D 04   | 0.139231D-02   | -0.486257D-01  | -0.210912030D 02 | -0.192965D-04  | 0.26895D-04   |
| 1.9000 | 0.036109557D 04  | 0.116024D-02   | -0.484683D-01  | -0.210192123D 02 | -0.190586D-04  | 0.259942D-04  |
| 2.0000 | 0.014849347D 04  | 0.0929659D-02  | -0.483138D-01  | -0.209487486D 02 | -0.188277D-04  | 0.25067D-04   |
| 2.1000 | 0.073589186D 04  | 0.069430D-02   | -0.481622D-01  | -0.208797886D 02 | -0.186037D-04  | 0.250000D-04  |
| 2.2000 | 0.04233838D 04   | 0.046330D-02   | -0.48013D-01   | -0.208123102D 02 | -0.183855D-04  | 0.24544D-04   |
| 2.3000 | 0.010913793D 04  | 0.023636D-02   | -0.478675D-01  | -0.207462160D 02 | -0.181739D-04  | 0.240891D-04  |
| 2.4000 | 0.048487468D 04  | 0.002523D-02   | -0.477244D-01  | -0.206817120D 02 | -0.179680D-04  | 0.233082D-04  |
| 2.5000 | 0.068067459D 04  | 0.024802D-02   | -0.475839D-01  | -0.206185804D 02 | -0.177690D-04  | 0.233793D-04  |
| 2.6000 | 0.047374928D 04  | 0.04199D-02    | -0.474462D-01  | -0.205567873D 02 | -0.175755D-04  | 0.223343D-04  |
| 2.7000 | 0.061493943D 04  | 0.023710D-02   | -0.47311D-01   | -0.204966032D 02 | -0.173877D-04  | 0.222585D-04  |
| 2.8000 | 0.049148972D 04  | 0.013333D-02   | -0.471786D-01  | -0.204373793D 02 | -0.1720547D-04 | 0.216353D-04  |
| 2.9000 | 0.036993915D 04  | 0.013063D-02   | -0.470487D-01  | -0.203796760D 02 | -0.170286D-04  | 0.213728D-04  |
| 3.0000 | 0.02463068D 04   | 0.012897D-02   | -0.46921D-01   | -0.203233010D 02 | -0.168568D-04  | 0.211688D-04  |
| 3.1000 | 0.012515548D 04  | 0.012833D-02   | -0.467965D-01  | -0.202682899D 02 | -0.166904D-04  | 0.208220D-04  |
| 3.2000 | 0.060371967D 04  | 0.012868D-02   | -0.466744D-01  | -0.202145300D 02 | -0.165295D-04  | 0.201930D-04  |
| 3.3000 | 0.058827958D 04  | 0.012997D-02   | -0.465542D-01  | -0.201620440D 02 | -0.163726D-04  | 0.197892D-04  |
| 3.4000 | 0.07611616D 04   | 0.013220D-02   | -0.464368D-01  | -0.201108174D 02 | -0.162210D-04  | 0.19907D-04   |
| 3.5000 | 0.064124729D 04  | 0.013351D-02   | -0.463215D-01  | -0.200608336D 02 | -0.160740D-04  | 0.189972D-04  |
| 3.6000 | 0.0552112919D 04 | 0.013393D-02   | -0.462087D-01  | -0.200120784D 02 | -0.159317D-04  | 0.18087D-04   |
| 3.7000 | 0.04011999D 04   | 0.014412D-02   | -0.46098D-01   | -0.19964571D 02  | -0.15793D-04   | 0.18250D-04   |
| 3.8000 | 0.028145228D 04  | 0.0149762D-03  | -0.45990D-01   | -0.199181961D 02 | -0.1566047D-04 | 0.178459D-04  |
| 3.9000 | 0.01627915D 04   | 0.0156188D-03  | -0.45884D-01   | -0.19873447D 02  | -0.155315D-04  | 0.174713D-04  |
| 4.0000 | 0.030429344D 04  | 0.016337D-03   | -0.457803D-01  | -0.19829611D 02  | -0.154067D-04  | 0.171011D-04  |
| 4.1000 | 0.049242812D 04  | 0.016130D-03   | -0.45678D-01   | -0.19786212D 02  | -0.152852D-04  | 0.167351D-04  |
| 4.2000 | 0.048053525D 04  | 0.0159940D-03  | -0.455795D-01  | -0.19744570D 02  | -0.151694D-04  | 0.163737D-04  |
| 4.3000 | 0.046871914D 04  | 0.0158266D-03  | -0.454823D-01  | -0.197043356D 02 | -0.150563D-04  | 0.161555D-04  |
| 4.4000 | 0.045691855D 04  | 0.015697D-03   | -0.45387D-01   | -0.196643264D 02 | -0.149473D-04  | 0.156615D-04  |
| 4.5000 | 0.044511331D 04  | 0.015588D-03   | -0.45294D-01   | -0.196263513D 02 | -0.1484256D-04 | 0.153110D-04  |
| 4.6000 | 0.043336742D 04  | 0.015489D-03   | -0.4521138D-01 | -0.195891393D 02 | -0.147435D-04  | 0.149646D-04  |
| 4.7000 | 0.042161414D 04  | 0.015398D-03   | -0.451146D-01  | -0.195531404D 02 | -0.146483D-04  | 0.146218D-04  |
| 4.8000 | 0.040982875D 04  | 0.01531D-04    | -0.45028D-01   | -0.195181241D 02 | -0.145495D-04  | 0.143822D-04  |
| 4.9000 | 0.039819231D 04  | 0.015219D-04   | -0.44943D-01   | -0.194846809D 02 | -0.144562D-04  | 0.140960D-04  |
| 5.0000 | 0.038651766D 04  | 0.0151317D-03  | -0.448607D-01  | -0.194512114D 02 | -0.143781D-04  | 0.138129D-04  |
| 5.1000 | 0.0374851645D 04 | 0.01504102D-03 | -0.44780D-01   | -0.194193764D 02 | -0.1429945D-04 | 0.135829D-04  |

| TIME    | R-DOT             | LAT,-DOT      | LONG,-DOT     | R-DOT DOT        | LAT,-DOT DOT   | LONG,-DOT DOT  |
|---------|-------------------|---------------|---------------|------------------|----------------|----------------|
| 5.2000  | 0.163208370 04    | -0.295980-03  | -0.4470130-01 | -0.1938659740 02 | -0.14209430-04 | 0.12956040-04  |
| 5.3000  | 0.151581210 04    | -0.3846230-03 | -0.4482450-01 | -0.1935885560 02 | -0.1432880-04  | 0.12631990-04  |
| 5.4000  | 0.139977470 04    | -0.4691980-03 | -0.4494970-01 | -0.1933014330 02 | -0.1432880-04  | 0.123310750-04 |
| 5.5000  | 0.1283877470 04   | -0.5533440-03 | -0.4447680-01 | -0.1930245360 02 | -0.14358940-04 | 0.11992210-04  |
| 5.6000  | 0.1168143290 04   | -0.6377850-03 | -0.4405560-01 | -0.1927577580 02 | -0.14322530-04 | 0.11676300-04  |
| 5.7000  | 0.1052565140 04   | -0.7204200-03 | -0.4433670-01 | -0.1925010370 02 | -0.14358880-04 | 0.11369900-04  |
| 5.8000  | 0.093714330 04    | -0.833900-03  | -0.4426940-01 | -0.1922543580 02 | -0.14379810-04 | 0.11051940-04  |
| 5.9000  | 0.0821853940 04   | -0.8660040-03 | -0.4420400-01 | -0.1920175500 02 | -0.14374060-04 | 0.10743320-04  |
| 6.0000  | 0.0706715950 04   | -0.962830-03  | -0.4444500-01 | -0.1917903620 02 | -0.14368610-04 | 0.10433950-04  |
| 6.1000  | 0.059173160 04    | -1.05240-02   | -0.4407880-01 | -0.1915736140 02 | -0.1436450-04  | 0.10132750-04  |
| 6.2000  | 0.0476826650 04   | -1.11900-02   | -0.4411890-01 | -0.1913662870 02 | -0.14358600-04 | 0.98306300-05  |
| 6.3000  | 0.0362065630 04   | -1.23280-02   | -0.4366080-01 | -0.191166670 02  | -0.14354040-04 | 0.95305090-05  |
| 6.4000  | 0.024742240 04    | -0.1294390-02 | -0.4304500-01 | -0.1909806320 02 | -0.14349760-04 | 0.92323020-05  |
| 6.5000  | 0.013288910 04    | -1.375260-02  | -0.4385000-01 | -0.1908022300 02 | -0.14345780-04 | 0.89435280-05  |
| 6.6000  | 0.001845780 04    | -1.455890-02  | -0.4379730-01 | -0.1906333760 02 | -0.14342080-04 | 0.86413050-05  |
| 6.7000  | 0.000412630 04    | -1.536320-02  | -0.4374630-01 | -0.1904740250 02 | -0.14338660-04 | 0.83485550-05  |
| 6.8000  | 0.0078988780 04   | -1.616540-02  | -0.4369710-01 | -0.1903241370 02 | -0.14335920-04 | 0.80569980-05  |
| 6.9000  | 0.0167573210 04   | -1.696580-02  | -0.4364970-01 | -0.1901836700 02 | -0.14332660-04 | 0.77671560-05  |
| 7.0000  | 0.0156164810 04   | -0.1776470-02 | -0.4360390-01 | -0.1900525500 02 | -0.14330080-04 | 0.74787520-05  |
| 7.1000  | 0.01447670240 04  | -0.1856200-02 | -0.4355990-01 | -0.1899308600 02 | -0.14327770-04 | 0.71917110-05  |
| 7.2000  | 0.01337435920 04  | -0.1935800-02 | -0.4351760-01 | -0.1898184510 02 | -0.14325730-04 | 0.69059570-05  |
| 7.3000  | 0.01219885240 04  | -2.15290-02   | -0.4347700-01 | -0.1897153320 02 | -0.14323670-04 | 0.66214140-05  |
| 7.4000  | 0.0106085650 04   | -2.29460-02   | -0.4343820-01 | -0.1896221460 02 | -0.14321620-04 | 0.63381090-05  |
| 7.5000  | 0.0092335240 03   | -2.173990-02  | -0.4340100-01 | -0.1895368600 02 | -0.14319220-04 | 0.60558690-05  |
| 7.6000  | 0.0078639590 03   | -2.223240-02  | -0.4336550-01 | -0.1894614620 02 | -0.14316260-04 | 0.57743320-05  |
| 7.7000  | 0.0064983330 03   | -2.332430-02  | -0.4333170-01 | -0.1893955280 02 | -0.14313950-04 | 0.54935910-05  |
| 7.8000  | 0.0051363440 03   | -2.411590-02  | -0.4329660-01 | -0.1893382750 02 | -0.14311920-04 | 0.52144080-05  |
| 7.9000  | 0.0037772380 03   | -2.497730-02  | -0.4326910-01 | -0.1892903300 02 | -0.14310950-04 | 0.49355010-05  |
| 8.0000  | 0.0024211450 03   | -2.569870-02  | -0.4324630-01 | -0.1892516590 02 | -0.14309410-04 | 0.46573990-05  |
| 8.1000  | 0.0010674550 03   | -2.649020-02  | -0.4321320-01 | -0.1892211340 02 | -0.14307940-04 | 0.43793300-05  |
| 8.2000  | 0.0001714760 03   | -2.728200-02  | -0.4318780-01 | -0.1892017150 02 | -0.14306000-04 | 0.41030230-05  |
| 8.3000  | 0.0036277570 02   | -2.817430-02  | -0.4316400-01 | -0.1891904270 02 | -0.14304870-04 | 0.38226610-05  |
| 8.4000  | 0.0043401660 03   | -2.886710-02  | -0.4314180-01 | -0.1891882850 02 | -0.14302020-04 | 0.35505190-05  |
| 8.5000  | 0.002569235760 03 | -2.966080-02  | -0.4312140-01 | -0.1891952320 02 | -0.14304310-04 | 0.32745610-05  |
| 8.6000  | 0.003704555840 03 | -3.05530-02   | -0.4310250-01 | -0.1892113380 02 | -0.14309970-04 | 0.29996250-05  |
| 8.7000  | 0.004840073720 03 | -3.125090-02  | -0.4306990-01 | -0.1892365580 02 | -0.14307020-04 | 0.27244820-05  |
| 8.8000  | 0.0057585210 03   | -3.24600-02   | -0.4305600-01 | -0.1892144660 02 | -0.14316770-04 | 0.24494810-05  |
| 8.9000  | 0.00711855340 03  | -3.364590-02  | -0.4304380-01 | -0.1893671230 02 | -0.14344010-04 | 0.21745540-05  |
| 9.0000  | 0.00824824720 03  | -3.444740-02  | -0.4303320-01 | -0.1894289760 02 | -0.14373910-04 | 0.18996300-05  |
| 9.1000  | 0.009385011420 03 | -3.525080-02  | -0.4302430-01 | -0.1895000170 02 | -0.14366480-04 | 0.16244390-05  |
| 9.2000  | 0.0105225750 04   | -3.605620-02  | -0.4301700-01 | -0.1895802850 02 | -0.14364770-04 | 0.13495110-05  |
| 9.3000  | 0.0116601310 04   | -3.686380-02  | -0.4301140-01 | -0.1896697480 02 | -0.14341770-04 | 0.10717480-05  |
| 9.4000  | 0.0127983230 04   | -3.767380-02  | -0.4300740-01 | -0.1897684730 02 | -0.14379730-04 | 0.79855970-06  |
| 9.5000  | 0.01393735320 04  | -3.848630-02  | -0.4300510-01 | -0.1898764310 02 | -0.14352040-04 | 0.522259540-06 |
| 9.6000  | 0.01507685930 04  | -3.93150-02   | -0.4300450-01 | -0.1899937950 02 | -0.14363680-04 | 0.24624020-06  |
| 9.7000  | 0.01621713740 04  | -4.011960-02  | -0.4300550-01 | -0.1901204440 02 | -0.14361020-04 | -0.30667920-07 |
| 9.8000  | 0.01735832350 04  | -4.094070-02  | -0.4300820-01 | -0.1902566430 02 | -0.14371070-04 | -0.30810700-06 |
| 9.9000  | 0.01850023370 04  | -4.165500-02  | -0.4301250-01 | -0.1904018880 02 | -0.14365350-04 | -0.58619140-06 |
| 10.0000 | 0.01964315490 04  | -4.239260-02  | -0.4301850-01 | -0.1905567320 02 | -0.14362270-04 | -0.86499330-06 |
| 10.1000 | 0.02078669370 04  | -4.312370-02  | -0.4302620-01 | -0.1907211100 02 | -0.14362050-04 | -0.11445060-05 |
| 10.2000 | 0.02193113710 04  | -4.445860-02  | -0.4303560-01 | -0.1908949760 02 | -0.14346240-04 | -0.14249960-05 |
| 10.3000 |                   |               |               |                  |                | -0.17068680-05 |



| TIME    | R-DOY            | LAT.-DOY      | LONG.-DOY     | R-DOY            | LAT.-DOY       | LONG.-DOY       |
|---------|------------------|---------------|---------------|------------------|----------------|-----------------|
| 10.4000 | -0.2307775260 04 | -0.4509730-02 | -0.4304670-01 | -0.1910784220 02 | -0.1401240D-04 | -0.1988750D-05  |
| 10.5000 | -0.2422479740 04 | -0.4594020-02 | -0.4305950-01 | -0.1912714910 02 | -0.140815D-04  | -0.2272219D-05  |
| 10.6000 | -0.2537302970 04 | -0.4678720-02 | -0.4307400-01 | -0.1914742300 02 | -0.14159520-04 | -0.2556854D-05  |
| 10.7000 | -0.2652253750 04 | -0.4763860-02 | -0.4309000-01 | -0.1916866940 02 | -0.1422876D-04 | -0.2842733D-05  |
| 10.8000 | -0.2767323990 04 | -0.4849470-02 | -0.4310810-01 | -0.1919080940 02 | -0.1430637D-04 | -0.3129936D-05  |
| 10.9000 | -0.2882543450 04 | -0.4935550-02 | -0.4312700-01 | -0.1921412800 02 | -0.14386320-04 | -0.3418542D-05  |
| 11.0000 | -0.2997909190 04 | -0.5022140-02 | -0.4314910-01 | -0.1923831700 02 | -0.1447277D-04 | -0.3708350D-05  |
| 11.1000 | -0.3113455980 04 | -0.5109230-02 | -0.4317200-01 | -0.1926349740 02 | -0.1456044D-04 | -0.4000296D-05  |
| 11.2000 | -0.3229064150 04 | -0.5196870-02 | -0.4319710-01 | -0.1928969680 02 | -0.1465150D-04 | -0.4293610D-05  |
| 11.3000 | -0.3344883450 04 | -0.5285060-02 | -0.4322350-01 | -0.1931690650 02 | -0.1474939D-04 | -0.4588662D-05  |
| 11.4000 | -0.3460695500 04 | -0.5373820-02 | -0.4325220-01 | -0.1934513420 02 | -0.1484809D-04 | -0.4885538D-05  |
| 11.5000 | -0.3577027110 04 | -0.5463180-02 | -0.4328240-01 | -0.1937433760 02 | -0.1494411D-04 | -0.5184328D-05  |
| 11.6000 | -0.3693363720 04 | -0.5553160-02 | -0.4331440-01 | -0.1940461450 02 | -0.1504038D-04 | -0.5485121D-05  |
| 11.7000 | -0.3809885250 04 | -0.5643770-02 | -0.4334820-01 | -0.1943600330 02 | -0.1513624D-04 | -0.5788007D-05  |
| 11.8000 | -0.3926597920 04 | -0.5735040-02 | -0.4338330-01 | -0.1946838240 02 | -0.1523676D-04 | -0.6093079D-05  |
| 11.9000 | -0.4043559300 04 | -0.5826990-02 | -0.4342140-01 | -0.1950180800 02 | -0.1533827D-04 | -0.6400431D-05  |
| 12.0000 | -0.4160621880 04 | -0.5919640-02 | -0.4346270-01 | -0.1953635780 02 | -0.1550171D-04 | -0.6710164D-05  |
| 12.1000 | -0.4277945900 04 | -0.6013010-02 | -0.4350190-01 | -0.1957191310 02 | -0.1562337D-04 | -0.7023710D-05  |
| 12.2000 | -0.4395487400 04 | -0.6107130-02 | -0.4354500-01 | -0.1960855620 02 | -0.1575015D-04 | -0.7337154D-05  |
| 12.3000 | -0.4513251320 04 | -0.6202020-02 | -0.4358990-01 | -0.1964635770 02 | -0.1588030D-04 | -0.7654614D-05  |
| 12.4000 | -0.4631243560 04 | -0.6297700-02 | -0.4363680-01 | -0.1968523820 02 | -0.1601442D-04 | -0.7974857D-05  |
| 12.5000 | -0.4749475410 04 | -0.6394200-02 | -0.4368560-01 | -0.1972523840 02 | -0.1615126D-04 | -0.8297989D-05  |
| 12.6000 | -0.4867950650 04 | -0.6491540-02 | -0.4373640-01 | -0.1976637000 02 | -0.1629433D-04 | -0.8624119D-05  |
| 12.7000 | -0.4986675130 04 | -0.6589750-02 | -0.4378910-01 | -0.1980864440 02 | -0.1644413D-04 | -0.8953357D-05  |
| 12.8000 | -0.5105655530 04 | -0.6688850-02 | -0.4384350-01 | -0.1985207400 02 | -0.1659293D-04 | -0.9285819D-05  |
| 12.9000 | -0.5224923300 04 | -0.6788860-02 | -0.4389900-01 | -0.1989667120 02 | -0.1674741D-04 | -0.9621620D-05  |
| 13.0000 | -0.5344919150 04 | -0.6889820-02 | -0.4395590-01 | -0.1994244860 02 | -0.1690671D-04 | -0.9960879D-05  |
| 13.1000 | -0.5464214100 04 | -0.6991750-02 | -0.4402010-01 | -0.1998941980 02 | -0.1707085D-04 | -0.1030372D-04  |
| 13.2000 | -0.5584294590 04 | -0.7094680-02 | -0.4408300-01 | -0.2003759850 02 | -0.1723940D-04 | -0.1050527D-04  |
| 13.3000 | -0.5704667710 04 | -0.7198640-02 | -0.4414790-01 | -0.2008699900 02 | -0.1741330D-04 | -0.1100065D-04  |
| 13.4000 | -0.5825340900 04 | -0.7303650-02 | -0.4421500-01 | -0.2013763550 02 | -0.1759183D-04 | -0.1154995D-04  |
| 13.5000 | -0.5946321850 04 | -0.7409750-02 | -0.4428420-01 | -0.2018952330 02 | -0.1777940D-04 | -0.1204502D-04  |
| 13.6000 | -0.6067617850 04 | -0.7516960-02 | -0.4435560-01 | -0.2024267790 02 | -0.1796334D-04 | -0.1243319D-04  |
| 13.7000 | -0.6189235550 04 | -0.7625320-02 | -0.4442910-01 | -0.2029711520 02 | -0.1815760D-04 | -0.12841478D-04 |
| 13.8000 | -0.6311183790 04 | -0.7734860-02 | -0.4450400-01 | -0.2035288160 02 | -0.1835632D-04 | -0.13281478D-04 |
| 13.9000 | -0.6433347340 04 | -0.7845610-02 | -0.4458200-01 | -0.2040990430 02 | -0.1856085D-04 | -0.1379105D-04  |
| 14.0000 | -0.6556107320 04 | -0.7957600-02 | -0.4466320-01 | -0.2046829040 02 | -0.1877099D-04 | -0.14357215D-04 |
| 14.1000 | -0.6679095560 04 | -0.8070870-02 | -0.4474580-01 | -0.2052802810 02 | -0.1898660D-04 | -0.1495824D-04  |
| 14.2000 | -0.6802445400 04 | -0.8185450-02 | -0.4483070-01 | -0.2058913610 02 | -0.1920882D-04 | -0.1549488D-04  |
| 14.3000 | -0.6926168300 04 | -0.8301360-02 | -0.4491800-01 | -0.2065163310 02 | -0.1943642D-04 | -0.1547460D-04  |
| 14.4000 | -0.7050269810 04 | -0.8418700-02 | -0.4500770-01 | -0.2071553880 02 | -0.1967041D-04 | -0.1514810D-04  |
| 14.5000 | -0.7174757310 04 | -0.8537440-02 | -0.4509980-01 | -0.2078087360 02 | -0.1991075D-04 | -0.1555582D-04  |
| 14.6000 | -0.7299642170 04 | -0.8657640-02 | -0.4519430-01 | -0.2084765820 02 | -0.2015700D-04 | -0.1586939D-04  |
| 14.7000 | -0.7424932150 04 | -0.8779330-02 | -0.4529140-01 | -0.2091591400 02 | -0.2041115D-04 | -0.1638901D-04  |
| 14.8000 | -0.7550635150 04 | -0.8902590-02 | -0.4539130-01 | -0.2098566300 02 | -0.2067137D-04 | -0.1681486D-04  |
| 14.9000 | -0.7676763130 04 | -0.9027420-02 | -0.4549320-01 | -0.2105697780 02 | -0.2093905D-04 | -0.1724714D-04  |
| 15.0000 | -0.7803322350 04 | -0.9153870-02 | -0.4559800-01 | -0.2112973200 02 | -0.2121378D-04 | -0.1768607D-04  |
| 15.1000 | -0.7930323370 04 | -0.9282000-02 | -0.4570550-01 | -0.2120409950 02 | -0.2149597D-04 | -0.1813185D-04  |
| 15.2000 | -0.8057774770 04 | -0.9411840-02 | -0.4581500-01 | -0.2128000480 02 | -0.2178552D-04 | -0.185847D-04   |
| 15.3000 | -0.8185685910 04 | -0.9543450-02 | -0.4592850-01 | -0.2135766360 02 | -0.2208355D-04 | -0.1904487D-04  |
| 15.4000 | -0.8314069500 04 | -0.9676860-02 | -0.4604420-01 | -0.2143683210 02 | -0.2238999D-04 | -0.1951256D-04  |
| 15.5000 | -0.8442932220 04 | -0.9812140-02 | -0.4616270-01 | -0.2151770720 02 | -0.2270337D-04 | -0.1998804D-04  |



| TIME    | R-DOT            | LAT,-DOT      | LONG,-DOT     | R-DOT DOT        | LAT,-DOT DOT   | LONG,-DOT DOT  |
|---------|------------------|---------------|---------------|------------------|----------------|----------------|
| 15.6000 | -0.857228337D 04 | -0.994932D-02 | -0.462840D-01 | -0.216002768D 02 | -0.2302634D-04 | -0.2047154D-04 |
| 15.7000 | -0.87021391D 04  | -0.10885D-01  | -0.464083D-01 | -0.216845689D 02 | -0.233579D-04  | -0.2096333D-04 |
| 15.8000 | -0.88325336D 04  | -0.11229D-01  | -0.46335D-01  | -0.217706134D 02 | -0.236986D-04  | -0.2146368D-04 |
| 15.9000 | -0.89633899D 04  | -0.11372D-01  | -0.46665D-01  | -0.218584306D 02 | -0.240485D-04  | -0.2197286D-04 |
| 16.0000 | -0.90948357D 04  | -0.11518D-01  | -0.467993D-01 | -0.219480812D 02 | -0.244083D-04  | -0.2249116D-04 |
| 16.1000 | -0.92267055D 04  | -0.11665D-01  | -0.469358D-01 | -0.220395676D 02 | -0.247783D-04  | -0.231188D-04  |
| 16.2000 | -0.93592871D 04  | -0.11815D-01  | -0.47075D-01  | -0.221329328D 02 | -0.251586D-04  | -0.235632D-04  |
| 16.3000 | -0.94923696D 04  | -0.11967D-01  | -0.47218D-01  | -0.222282102D 02 | -0.255487D-04  | -0.241038D-04  |
| 16.4000 | -0.96260295D 04  | -0.11122D-01  | -0.473648D-01 | -0.223254355D 02 | -0.259507D-04  | -0.2466166D-04 |
| 16.5000 | -0.97602378D 04  | -0.11279D-01  | -0.475145D-01 | -0.22424644D 02  | -0.263635D-04  | -0.253022D-04  |
| 16.6000 | -0.989512934D 04 | -0.11438D-01  | -0.476676D-01 | -0.22525836D 02  | -0.2678747D-04 | -0.259986D-04  |
| 16.7000 | -0.10030593D 05  | -0.11600D-01  | -0.478242D-01 | -0.226291619D 02 | -0.272239D-04  | -0.2640094D-04 |
| 16.8000 | -0.10166693D 05  | -0.11765D-01  | -0.479844D-01 | -0.227345481D 02 | -0.2767374D-04 | -0.2700383D-04 |
| 16.9000 | -0.10303388D 05  | -0.11932D-01  | -0.481482D-01 | -0.22825638D 02  | -0.2811518D-04 | -0.275514D-04  |

| TIME (MIN) | SLANT RANGE (FT)  | SL RANGE RATE (FT/SEC) | SENSOR ALTITUDE (FT) | SL RANGE ALTITUDE (FT) | 0.50333          | 0.50333 | AZ RATE (DEG/SEC) |
|------------|-------------------|------------------------|----------------------|------------------------|------------------|---------|-------------------|
| 5.8 00     | 0.105519 363220   | 8                      | - 371149781160       | 04                     | 0.479566974380   | 01      | 0.1818523030 02   |
| 5.9 00     | 0.105597 275440   | 8                      | - 368283959920       | 04                     | 0.4779475790     | 02      | - 0.652310-01     |
| 6.0 00     | 0.105577 313970   | 06                     | - 365440.471150      | 04                     | 0.472661846870   | 01      | 0.140245610 02    |
| 6.1 00     | 0.1051586754830   | 04                     | - 36261659101270     | 04                     | 0.469075930400   | 01      | 0.1700632410 02   |
| 6.2 00     | 0.1049419483380   | 08                     | - 35981057171760     | 04                     | 0.4662041941350  | 01      | 0.1661236140 02   |
| 6.3 00     | 0.104268396230    | 06                     | - 357 21172290       | 04                     | 0.463648679370   | 01      | 0.1621425684 02   |
| 6.4 00     | 0.104312 1380     | 06                     | - 354236.859780      | 04                     | 0.4614171389610  | 01      | 0.1581394590 02   |
| 6.5 00     | 0.104433 1811320  | 06                     | - 3514833259010      | 04                     | 0.459496218110   | 01      | 0.1541349510 02   |
| 6.6 00     | 0.104 917378 78   | 08                     | - 3487314921570      | 04                     | 0.457902735470   | 01      | 0.1501021800 02   |
| 6.7 00     | 0.1036833233 08   | 06                     | - 345988.410420      | 04                     | 0.456354459040   | 01      | 0.1460511710 02   |
| 6.8 00     | 0.10367655 8380   | 06                     | - 3432512108270      | 04                     | 0.455696177170   | 01      | 0.1449819540 02   |
| 6.9 00     | 0.1034714199520   | 08                     | - 3405191260120      | 04                     | 0.4550873910690  | 01      | 0.1387945670 02   |
| 7.0 00     | 0.1036792746 08   | 06                     | - 3377894962330      | 04                     | 0.4546311566550  | 01      | 0.1337890510 02   |
| 7.1 00     | 0.10366 724310    | 08                     | - 335160616000       | 04                     | 0.454871296330   | 01      | 0.1296654570 02   |
| 7.2 00     | 0.102689835 220   | 08                     | - 332330308450       | 04                     | 0.455699118970   | 01      | 0.1252338370 02   |
| 7.3 00     | 0.102627676590    | 06                     | - 32959607596680     | 04                     | 0.4556075996680  | 01      | 0.1213642950 02   |
| 7.4 00     | 0.10247034 1690   | 08                     | - 3268575667180      | 04                     | 0.457894346130   | 01      | 0.1171867760 02   |
| 7.5 00     | 0.102275 49 840   | 08                     | - 3241109402740      | 04                     | 0.4585172807710  | 01      | 0.1129914760 02   |
| 7.6 00     | 0.102 814089670   | 08                     | - 3213546891660      | 04                     | 0.463293843490   | 01      | 0.108784340 02    |
| 7.7 00     | 0.10189458120     | 06                     | - 3185867112950      | 04                     | 0.4624241862220  | 01      | 0.105477360 02    |
| 7.8 00     | 0.101699175830    | 08                     | - 3158049112430      | 04                     | 0.4649041.04460  | 01      | 0.1002994770 02   |
| 7.9 00     | 0.1015114631150   | 08                     | - 313 071481230      | 04                     | 0.467743326220   | 01      | 0.09603575550 01  |
| 8.0 00     | 0.101333326330    | 06                     | - 3101912714030      | 04                     | 0.4739424381370  | 01      | 0.09173067860 01  |
| 8.1 00     | 0.101382376510    | 06                     | - 3 73551135710      | 04                     | 0.4745042.02190  | 01      | 0.08745035910 01  |
| 8.2 00     | 0.10156458 9940   | 08                     | - 3 44964899800      | 04                     | 0.4784315.38050  | 01      | 0.08313391680 01  |
| 8.3 00     | 0.101 728468 04   | 04                     | - 3 16131.987370     | 04                     | 0.4827272382660  | 01      | 0.07879847840 01  |
| 8.4 00     | 0.101 59275 5370  | 08                     | - 298787830205890    | 04                     | 0.47444717700    | 01      | 0.0726610-01      |
| 8.5 00     | 0.101 414409 30   | 08                     | - 29576373188390     | 04                     | 0.4924355894080  | 01      | 0.07007915220 01  |
| 8.6 00     | 0.101 32784 3520  | 08                     | - 292793.1302430     | 04                     | 0.4975240587640  | 01      | 0.0656945520 01   |
| 8.7 00     | 0.101 3058 54 930 | 08                     | - 28973887.99870     | 04                     | 0.5030326334350  | 01      | 0.06129352930 01  |
| 8.8 00     | 0.0998911.7160    | 07                     | - 2867484316160      | 04                     | 0.5098342539660  | 01      | 0.05687824470 01  |
| 8.9 00     | 0.09971897351390  | 07                     | - 2836699270260      | 04                     | 0.5164018625290  | 01      | 0.05244286510 01  |
| 9.0 00     | 0.099537.32790    | 07                     | - 2805808314730      | 04                     | 0.523583982450   | 01      | 0.04799358480 01  |
| 9.1 00     | 0.09936323113960  | 07                     | - 2773888425790      | 04                     | 0.5307067862250  | 01      | 0.04352852440 01  |
| 9.2 00     | 0.09921984774570  | 07                     | - 2741815703890      | 04                     | 0.5384994934230  | 01      | 0.03904793160 01  |
| 9.3 00     | 0.099 5331283910  | 07                     | - 2709266474540      | 04                     | 0.54659.8642720  | 01      | 0.03455198060 01  |
| 9.4 00     | 0.0989417575 50   | 07                     | - 2676216789160      | 04                     | 0.5553323310130  | 01      | 0.03004087230 01  |
| 9.5 00     | 0.09873217731850  | 07                     | - 2642642826500      | 04                     | 0.5640772498410  | 01      | 0.02551481420 01  |
| 9.6 00     | 0.0985763965780   | 07                     | - 2608519394110      | 04                     | 0.5734284577550  | 01      | 0.0207402060 01   |
| 9.7 00     | 0.0984196645170   | 07                     | - 2573822330430      | 04                     | 0.5831887572050  | 01      | 0.01641871220 01  |
| 9.8 00     | 0.0982679286780   | 07                     | - 2538523306910      | 04                     | 0.599336.9104330 | 01      | 0.01184911600 01  |
| 9.9 00     | 0.09811455549850  | 07                     | - 2502611330530      | 04                     | 0.6039476335670  | 01      | 0.07265465660 01  |
| 10.0 00    | 0.0979542945650   | 07                     | - 2466046436920      | 04                     | 0.6149513904820  | 01      | 0.02668001000 00  |
| 10.1 00    | 0.09781864338470  | 07                     | - 2428808743640      | 04                     | 0.6263753663760  | 01      | 0.03598056970 03  |
| 10.2 00    | 0.09767674933 70  | 07                     | - 239 872953770      | 04                     | 0.6382215810650  | 01      | 0.03593432620 03  |
| 10.3 00    | 0.0975317531 260  | 07                     | - 23522135660170     | 04                     | 0.6504925820270  | 01      | 0.03588795240 03  |
| 10.4 00    | 0.0973917957260   | 07                     | - 2312805300020      | 04                     | 0.6631978372290  | 01      | 0.03584145000 03  |
| 10.5 00    | 0.09725423195470  | 07                     | - 2272622169800      | 04                     | 0.6763186276170  | 01      | 0.03579482290 03  |
| 10.6 00    | 0.09711919 9-10   | 07                     | - 2231638430700      | 04                     | 0.6898787895360  | 01      | 0.03574807320 03  |
| 10.7 00    | 0.096964519380    | 07                     | - 2189928114580      | 04                     | 0.7038715366000  | 01      | 0.03570120360 03  |
| 10.8 00    | 0.0968583755440   | 07                     | - 2147165130740      | 04                     | 0.718307499640   | 01      | 0.03565421760 03  |
| 10.9 00    | 0.0967389 96520   | 07                     | - 2103623271230      | 04                     | 0.7331676439520  | 01      | 0.03560711760 03  |





| TIME (MIN) | AZ RDT (DEG/SEC) | ELEVATION (DEG) | EL RATE (DEG/SEC) | EL RDT (DEG/SEC)     | REENTRY ANGLE | HEADING      |
|------------|------------------|-----------------|-------------------|----------------------|---------------|--------------|
| 5.800      | -0.2318761D-03   | 3.6683566D 00   | 0.26830312D-01    | -0.111953365D-03     | 0.2575250 03  | 0.268546 03  |
| 5.900      | -0.24399162D-03  | 3.836142D 00    | 0.276290D-01      | -0.112786759158D-03  | 0.257993D 03  | 0.268425D 03 |
| 6.000      | -0.24956353D-03  | 3.9999024D 00   | 0.2694967D-01     | -0.113624730424D-03  | 0.258463D 03  | 0.268277D 03 |
| 6.100      | -0.25883531D-03  | 3.1159550D 01   | 0.2626340D-01     | -0.114464749399D-03  | 0.258935D 03  | 0.268129D 03 |
| 6.200      | -0.26853365D-03  | 3.1315077D 01   | 0.2557605D-01     | -0.11531494040D-03   | 0.259409D 03  | 0.267981D 03 |
| 6.300      | -0.27690390D-03  | 3.1466453D 01   | 0.2488461D-01     | -0.116167048219D-03  | 0.259884D 03  | 0.267833D 03 |
| 6.400      | -0.28293434D-03  | 3.1613340D 01   | 0.2418204D-01     | -0.117023641560D-03  | 0.260361D 03  | 0.267686D 03 |
| 6.500      | -0.30532990D-03  | 3.1765627D 01   | 0.2347731D-01     | -0.117884621511D-03  | 0.260840D 03  | 0.267539D 03 |
| 6.600      | -0.3123 433D-03  | 3.1895363D 01   | 0.227641D-01      | -0.118749858466D-03  | 0.261320D 03  | 0.267392D 03 |
| 6.700      | -0.3247 924D-03  | 3.2029825D 01   | 0.2205831D-01     | -0.119619204248D-03  | 0.261802D 03  | 0.267245D 03 |
| 6.800      | -0.3378 135D-03  | 3.2159981D 01   | 0.213397D-01      | -0.120492502837D-03  | 0.262285D 03  | 0.267099D 03 |
| 6.900      | -0.3516494D-03   | 3.2285798D 01   | 0.206039D-01      | -0.12136957702D-03   | 0.262769D 03  | 0.266953D 03 |
| 7.000      | -0.3682118D-03   | 3.2407247D 01   | 0.1987553D-01     | -0.122250239031D-03  | 0.263254D 03  | 0.266807D 03 |
| 7.100      | -0.3819 217D-03  | 3.2524294D 01   | 0.1913730D-01     | -0.1231334286639D-03 | 0.263740D 03  | 0.266661D 03 |
| 7.200      | -0.39848513D-03  | 3.263690D 01    | 0.1839791D-01     | -0.124021498873D-03  | 0.264228D 03  | 0.266515D 03 |
| 7.300      | -0.41617735D-03  | 3.2745359D 01   | 0.176512D-01      | -0.124911643148D-03  | 0.264716D 03  | 0.266370D 03 |
| 7.400      | -0.4351 243D-03  | 3.284811D 01    | 0.168997D-01      | -0.125804463740D-03  | 0.265206D 03  | 0.266225D 03 |
| 7.500      | -0.4554 314D-03  | 3.2947835D 01   | 0.161446D-01      | -0.12669696440D-03   | 0.265696D 03  | 0.266080D 03 |
| 7.600      | -0.47724548D-03  | 3.3042398D 01   | 0.1537857D-01     | -0.127597050567D-03  | 0.266187D 03  | 0.265935D 03 |
| 7.700      | -0.5082365D-03   | 3.312367D 01    | 0.146129D-01      | -0.128496227144D-03  | 0.266678D 03  | 0.265790D 03 |
| 7.800      | -0.52836641D-03  | 3.321711D 01    | 0.1383661D-01     | -0.129396903723D-03  | 0.267170D 03  | 0.265645D 03 |
| 7.900      | -0.5541446D-03   | 3.329752D 01    | 0.1305752D-01     | -0.130298740514D-03  | 0.267663D 03  | 0.265501D 03 |
| 8.000      | -0.58448195D-03  | 3.337439D 01    | 0.122732D-01      | -0.131031378014D-03  | 0.268156D 03  | 0.265357D 03 |
| 8.100      | -0.61776827D-03  | 3.3445661D 01   | 0.114831D-01      | -0.132044403883D-03  | 0.268649D 03  | 0.265213D 03 |
| 8.200      | -0.65447725D-03  | 3.351217D 01    | 0.106877D-01      | -0.133010226875D-03  | 0.269143D 03  | 0.265069D 03 |
| 8.300      | -0.69519052D-03  | 3.357396D 01    | 0.988718D-02      | -0.133910226875D-03  | 0.269636D 03  | 0.264925D 03 |
| 8.400      | -0.74622984D-03  | 3.363081D 01    | 0.968095D-02      | -0.134812096291D-03  | 0.270130D 03  | 0.264781D 03 |
| 8.500      | -0.7917 244D-03  | 3.3682863D 01   | 0.9269275D-02     | -0.135712860609D-03  | 0.270624D 03  | 0.264637D 03 |
| 8.600      | -0.84956445D-03  | 3.3730031D 01   | 0.845232D-02      | -0.136611501098D-03  | 0.271117D 03  | 0.264494D 03 |
| 8.700      | -0.9151261D-03   | 3.3772280D 01   | 0.629942D-02      | -0.137508059120D-03  | 0.271611D 03  | 0.264350D 03 |
| 8.800      | -0.99211957D-03  | 3.3809379D 01   | 0.580211D-02      | -0.138401831633D-03  | 0.272104D 03  | 0.264207D 03 |
| 8.900      | -0.10814395D-02  | 3.3841896D 01   | 0.4969127D-02     | -0.139292275586D-03  | 0.272596D 03  | 0.264063D 03 |
| 9.000      | -0.118733 4D-02  | 3.3869198D 01   | 0.4130711D-02     | -0.140178827794D-03  | 0.273089D 03  | 0.263920D 03 |
| 9.100      | -0.13149773D-02  | 3.3891154D 01   | 0.328699D-02      | -0.14106900979D-03   | 0.273583D 03  | 0.263777D 03 |
| 9.200      | -0.14719833D-02  | 3.3908831D 01   | 0.243799D-02      | -0.141957788728D-03  | 0.274072D 03  | 0.263634D 03 |
| 9.300      | -0.16699545D-02  | 3.3920699D 01   | 0.1583746D-02     | -0.142809147061D-03  | 0.274562D 03  | 0.263491D 03 |
| 9.400      | -0.19275987D-02  | 3.3927626D 01   | 0.724236D-03      | -0.143674035762D-03  | 0.275052D 03  | 0.263348D 03 |
| 9.500      | -0.22769571D-02  | 3.3929380D 01   | -0.1403378D-03    | -0.144531873164D-03  | 0.275541D 03  | 0.263205D 03 |
| 9.600      | -0.27781251D-02  | 3.392532D 01    | -0.1010073D-02    | -0.145381958661D-03  | 0.276028D 03  | 0.263062D 03 |
| 9.700      | -0.3588437D-02   | 3.391749D 01    | -0.1884894D-02    | -0.14622356858D-03   | 0.276515D 03  | 0.262919D 03 |
| 9.800      | -0.49422061D-02  | 3.3903303D 01   | -0.2764738D-02    | -0.147055958255D-03  | 0.277001D 03  | 0.262776D 03 |
| 9.900      | -0.80765965D-02  | 3.3884163D 01   | -0.3649346D-02    | -0.14787835965D-03   | 0.277486D 03  | 0.262633D 03 |
| 10.000     | -0.22020205D-01  | 3.3859499D 01   | -0.539356D-02     | -0.148689978428D-03  | 0.277969D 03  | 0.262490D 03 |
| 10.100     | 0.30295167D-01   | 3.382982D 01    | -0.543393D-02     | -0.149490003006D-03  | 0.278451D 03  | 0.262347D 03 |
| 10.200     | 0.8972946 1D-02  | 3.3794383D 01   | -0.5333112D-02    | -0.150277593679D-03  | 0.278932D 03  | 0.262204D 03 |
| 10.300     | 0.5262298D-02    | 3.375375D 01    | -0.237307D-02     | -0.151151895842D-03  | 0.279411D 03  | 0.262061D 03 |
| 10.400     | 0.27212525D-02   | 3.3707429D 01   | -0.145706D-02     | -0.151912021708D-03  | 0.279889D 03  | 0.261918D 03 |
| 10.500     | 0.28759228D-02   | 3.365821D 01    | -0.905821D-02     | -0.152557072910D-03  | 0.280365D 03  | 0.261775D 03 |
| 10.600     | 0.23417411D-02   | 3.359814D 01    | -0.976359D-02     | -0.153286120460D-03  | 0.280840D 03  | 0.261632D 03 |
| 10.700     | 0.197333 8D-02   | 3.3536193D 01   | -0.1089322D-01    | -0.153998221899D-03  | 0.281312D 03  | 0.261489D 03 |
| 10.800     | 0.17336745D-02   | 3.3467927D 01   | -0.118230D-01     | -0.154692406935D-03  | 0.281783D 03  | 0.261346D 03 |
| 10.900     | 0.14975383D-02   | 3.3394193D 01   | -0.1275449D-01    | -0.155367689140D-03  | 0.282252D 03  | 0.261202D 03 |



| TIME (MIN) | AZ ROOT (DEG/SEC) | ELEVATION (DEG) | EL RATE (DEG/SEC) | EL ROOT (DEG/SEC)    | REENTRY ANGLE | HEADING      |
|------------|-------------------|-----------------|-------------------|----------------------|---------------|--------------|
| 11.0000    | 0.1348283D-02     | 0.3314865D 01   | -0.1368887D-01    | -0.1560330638554D-03 | 0.282720D 03  | 0.241050D 03 |
| 11.1000    | 0.1262919D-02     | 0.3229931D 01   | -0.1462632D-01    | -0.156657500018D-03  | 0.283185D 03  | 0.260910D 03 |
| 11.2000    | 0.10937558D-02    | 0.3139337D 01   | -0.1556852D-01    | -0.15729962783D-03   | 0.283680D 03  | 0.260770D 03 |
| 11.3000    | 0.1018441D-02     | 0.3043092D 01   | -0.1651392D-01    | -0.15789382481D-03   | 0.284100D 03  | 0.260620D 03 |
| 11.4000    | 0.92332577D-03    | 0.2944163D 01   | -0.1746228D-01    | -0.158434684241D-03  | 0.284570D 03  | 0.260480D 03 |
| 11.5000    | 0.854177D-03      | 0.2833352D 01   | -0.1841497D-01    | -0.15894477252D-03   | 0.285030D 03  | 0.260340D 03 |
| 11.6000    | 0.79605111D-03    | 0.2720177D 01   | -0.1937031D-01    | -0.159478544683D-03  | 0.285480D 03  | 0.260190D 03 |
| 11.7000    | 0.74366794D-03    | 0.2601082D 01   | -0.2032865D-01    | -0.159944874820D-03  | 0.285930D 03  | 0.260050D 03 |
| 11.8000    | 0.69706523D-03    | 0.2476328D 01   | -0.2128983D-01    | -0.160432625580D-03  | 0.286380D 03  | 0.259900D 03 |
| 11.9000    | 0.6533187D-03     | 0.2345599D 01   | -0.2225367D-01    | -0.160870663280D-03  | 0.286820D 03  | 0.259760D 03 |
| 12.0000    | 0.61763063D-03    | 0.2209479D 01   | -0.2321998D-01    | -0.16124782339D-03   | 0.287270D 03  | 0.259620D 03 |
| 12.1000    | 0.5834519D-03     | 0.206654D 01    | -0.2418888D-01    | -0.16161295334D-03   | 0.287710D 03  | 0.259470D 03 |
| 12.2000    | 0.5527491D-03     | 0.191812D 01    | -0.2515977D-01    | -0.161944871208D-03  | 0.288150D 03  | 0.259330D 03 |
| 12.3000    | 0.5237119D-03     | 0.1765039D 01   | -0.2613184D-01    | -0.162242413457D-03  | 0.288590D 03  | 0.259180D 03 |
| 12.4000    | 0.49739725D-03    | 0.1605326D 01   | -0.2710610D-01    | -0.162504403716D-03  | 0.289030D 03  | 0.259040D 03 |
| 12.5000    | 0.47308365D-03    | 0.1439763D 01   | -0.2808182D-01    | -0.162739662589D-03  | 0.289460D 03  | 0.258890D 03 |
| 12.6000    | 0.45033239D-03    | 0.1268342D 01   | -0.2905878D-01    | -0.162917014008D-03  | 0.289885D 03  | 0.258750D 03 |
| 12.7000    | 0.42953913D-03    | 0.1091956D 01   | -0.3003635D-01    | -0.163035284550D-03  | 0.290312D 03  | 0.258600D 03 |
| 12.8000    | 0.40993366D-03    | 0.9078993D 00   | -0.3101549D-01    | -0.163173308285D-03  | 0.290735D 03  | 0.258450D 03 |
| 12.9000    | 0.39157362D-03    | 0.7186688D 00   | -0.3199475D-01    | -0.163239923740D-03  | 0.291155D 03  | 0.258310D 03 |
| 13.0000    | 0.37434271D-03    | 0.5239618D 00   | -0.3297428D-01    | -0.163263989312D-03  | 0.291573D 03  | 0.258160D 03 |

END OF OUTPUT

|   |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |     |
|---|---|---|---|---|---|---|---|---|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|-----|
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 8  |    |    |    |    |    |    |    |    |    |    |    |     |

4 = 8

| TIME<br>MINUTES                      | SLANT RANGE<br>FEET | SL RANGE RATE<br>FEET/SEC. | ELEVATION<br>DEGREES | SL RANGE RATE DOT<br>FEET/SEC/SEC | ELEVATION RATE<br>DEGREES/SEC | ELEVATION RATE DOT<br>DEGREES/SEC/SEC | AZIMUTH<br>DEGREES | AZIMUTH RATE<br>DEGREES/SEC |
|--------------------------------------|---------------------|----------------------------|----------------------|-----------------------------------|-------------------------------|---------------------------------------|--------------------|-----------------------------|
| 5.800                                | 0.10165396160-04    | 0.27061306880-01           | 0.27061306880-01     | -0.47045566080-02                 | 0.42184256000-02              | 0.19072693200-04                      |                    |                             |
|                                      | 0.27758920960-06    | 0.61557273200-02           | 0.61557273200-02     | 0.19569238720-04                  | 0.27687491840-07              |                                       |                    |                             |
| ANGULAR SEPARATION IN RADAR BEAM = , |                     | 0.74624455040-02           |                      |                                   |                               |                                       |                    |                             |
| 5.900                                | 0.10326905580-04    | 0.26773313600-01           | 0.26773313600-01     | -0.48954309760-02                 | 0.43336199880-02              | 0.19325391360-04                      |                    |                             |
|                                      | 0.28778493760-06    | 0.62736475520-02           | 0.62736475520-02     | 0.19738600000-04                  | 0.28768874560-07              |                                       |                    |                             |
| ANGULAR SEPARATION IN RADAR BEAM = , |                     | 0.76248878720-02           |                      |                                   |                               |                                       |                    |                             |
| 6.000                                | 0.10486652800-04    | 0.26473828800-01           | 0.26473828800-01     | -0.50876209920-02                 | 0.44503292800-02              | 0.19577618720-04                      |                    |                             |
|                                      | 0.29867011360-06    | 0.63926034560-02           | 0.63926034560-02     | 0.19914724800-04                  | 0.29857057600-07              |                                       |                    |                             |
| ANGULAR SEPARATION IN RADAR BEAM = , |                     | 0.77891469440-02           |                      |                                   |                               |                                       |                    |                             |
| 6.100                                | 0.10644568540-04    | 0.26162771840-01           | 0.26162771840-01     | -0.52811752960-02                 | 0.45685501440-02              | 0.19829219360-04                      |                    |                             |
|                                      | 0.31031090880-06    | 0.65126343040-02           | 0.65126343040-02     | 0.20096897600-04                  | 0.30951271360-07              |                                       |                    |                             |
| ANGULAR SEPARATION IN RADAR BEAM = , |                     | 0.79552533760-02           |                      |                                   |                               |                                       |                    |                             |
| 6.200                                | 0.108000582720-04   | 0.258400059520-01          | 0.258400059520-01    | -0.54761427840-02                 | 0.46882784000-02              | 0.20080073280-04                      |                    |                             |
|                                      | 0.32278161920-06    | 0.66337794560-02           | 0.66337794560-02     | 0.20285912320-04                  | 0.32054421440-07              |                                       |                    |                             |
| ANGULAR SEPARATION IN RADAR BEAM = , |                     | 0.81232373120-02           |                      |                                   |                               |                                       |                    |                             |
| 6.300                                | 0.10954626080-04    | 0.25505608760-01           | 0.25505608760-01     | -0.56725720960-02                 | 0.48095092480-02              | 0.20330039040-04                      |                    |                             |
|                                      | 0.33616719580-06    | 0.67560784640-02           | 0.67560784640-02     | 0.20481548320-04                  | 0.333158260480-07             |                                       |                    |                             |
| ANGULAR SEPARATION IN RADAR BEAM = , |                     | 0.82931281920-02           |                      |                                   |                               |                                       |                    |                             |
| 6.400                                | 0.110662640-04      | 0.25159320640-01           | 0.25159320640-01     | -0.58705117440-02                 | 0.49322371200-02              | 0.20579030400-04                      |                    |                             |
|                                      | 0.35056280000-06    | 0.68795713280-02           | 0.68795713280-02     | 0.20683831680-04                  | 0.34269338880-07              |                                       |                    |                             |
| ANGULAR SEPARATION IN RADAR BEAM = , |                     | 0.84649550720-02           |                      |                                   |                               |                                       |                    |                             |
| 6.500                                | 0.11256513920-04    | 0.24801112960-01           | 0.24801112960-01     | -0.60700100480-02                 | 0.50564556160-02              | 0.20826920480-04                      |                    |                             |
|                                      | 0.36607806720-06    | 0.70042977920-02           | 0.70042977920-02     | 0.20892783360-04                  | 0.35381196800-07              |                                       |                    |                             |
| ANGULAR SEPARATION IN RADAR BEAM = , |                     | 0.86387459840-02           |                      |                                   |                               |                                       |                    |                             |
| 6.600                                | 0.11404215940-04    | 0.24430887360-01           | 0.24430887360-01     | -0.62711150080-02                 | 0.51821576960-02              | 0.21073536800-04                      |                    |                             |
|                                      | 0.38283731520-06    | 0.71302980480-02           | 0.71302980480-02     | 0.21108418240-04                  | 0.36496609280-07              |                                       |                    |                             |
| ANGULAR SEPARATION IN RADAR BEAM = , |                     | 0.88145282560-02           |                      |                                   |                               |                                       |                    |                             |
| 6.700                                | 0.11549660000-04    | 0.24048545920-01           | 0.24048545920-01     | -0.64738743680-02                 | 0.53093352960-02              | 0.21318746080-04                      |                    |                             |
|                                      | 0.40098417280-06    | 0.72576121600-02           | 0.72576121600-02     | 0.21330744800-04                  | 0.37610901120-07              |                                       |                    |                             |
| ANGULAR SEPARATION IN RADAR BEAM = , |                     | 0.89923287040-02           |                      |                                   |                               |                                       |                    |                             |
| 6.800                                | 0.11692774980-04    | 0.23653988480-01           | 0.23653988480-01     | -0.66783352960-02                 | 0.54379798400-02              | 0.21562473280-04                      |                    |                             |
|                                      | 0.42168289280-06    | 0.73862803840-02           | 0.73862803840-02     | 0.21559766400-04                  | 0.38728631360-07              |                                       |                    |                             |

|  |                  |                  |                   |                  |
|--|------------------|------------------|-------------------|------------------|
| ANGULAR SEPRATION IN RADAR BEAM = , 0.9172173312D-02 |                  |                  |                   |                  |
| 6.900  | 0.1183334836D-04 | 0.2324711072D-01 | -0.6884544320D-02 | 0.5568081600D-02 |
|  | 0.4421251254D-06 | 0.7516342784D-02 | 0.2179547904D-04  | 0.3984319936D-07 |
| ANGULAR SEPRATION IN RADAR BEAM = , 0.9354086912D-02 |                  |                  |                   |                  |
| 7.000  | 0.1197171376D-04 | 0.2282780704D-01 | -0.7092547584D-02 | 0.5699630336D-02 |
|  | 0.4655330550D-06 | 0.7647839488D-02 | 0.2203787264D-04  | 0.4095352768D-07 |
| ANGULAR SEPRATION IN RADAR BEAM = , 0.9538093824D-02 |                  |                  |                   |                  |
| 7.100  | 0.1210739216D-04 | 0.2239596832D-01 | -0.7302390336D-02 | 0.5832614784D-02 |
|  | 0.4911653550D-06 | 0.7780810560D-02 | 0.2286928960D-04  | 0.4206221024D-07 |
| ANGULAR SEPRATION IN RADAR BEAM = , 0.9724217600D-02 |                  |                  |                   |                  |
| 7.200  | 0.1224044000D-04 | 0.2195148256D-01 | -0.7514115928D-02 | 0.5967022656D-02 |
|  | 0.5193275520D-06 | 0.7915295872D-02 | 0.2254262432D-04  | 0.4316624064D-07 |
| ANGULAR SEPRATION IN RADAR BEAM = , 0.9912480512D-02 |                  |                  |                   |                  |
| 7.300  | 0.1237078448D-04 | 0.2149423584D-01 | -0.7727709440D-02 | 0.6102841088D-02 |
|  | 0.5513787200D-06 | 0.8051335232D-02 | 0.2280492608D-04  | 0.4426628160D-07 |
| ANGULAR SEPRATION IN RADAR BEAM = , 0.1010290392D-01 |                  |                  |                   |                  |
| 7.400  | 0.1249834496D-04 | 0.2102411056D-01 | -0.7943394816D-02 | 0.6240056064D-02 |
|  | 0.5847478848D-06 | 0.8188968192D-02 | 0.2307379488D-04  | 0.4535553792D-07 |
| ANGULAR SEPRATION IN RADAR BEAM = , 0.1029550872D-01 |                  |                  |                   |                  |
| 7.500  | 0.1262304912D-04 | 0.2054098880D-01 | -0.8161029888D-02 | 0.6378652736D-02 |
|  | 0.6229454160D-06 | 0.8328233856D-02 | 0.2334918240D-04  | 0.4643830016D-07 |
| ANGULAR SEPRATION IN RADAR BEAM = , 0.1049031408D-01 |                  |                  |                   |                  |
| 7.600  | 0.1274481134D-04 | 0.2004474640D-01 | -0.8380715968D-02 | 0.6518615488D-02 |
|  | 0.6655876992D-06 | 0.8469171264D-02 | 0.2363103392D-04  | 0.4750954816D-07 |
| ANGULAR SEPRATION IN RADAR BEAM = , 0.1068733872D-01 |                  |                  |                   |                  |
| 7.700  | 0.1286358872D-04 | 0.1953526064D-01 | -0.8602491904D-02 | 0.6659927488D-02 |
|  | 0.7134208256D-06 | 0.8611819008D-02 | 0.2391928448D-04  | 0.4857163776D-07 |
| ANGULAR SEPRATION IN RADAR BEAM = , 0.1088660000D-01 |                  |                  |                   |                  |
| 7.800  | 0.1297923816D-04 | 0.1901240464D-01 | -0.8826394624D-02 | 0.6802571136D-02 |
|  | 0.7673595840D-06 | 0.8756215296D-02 | 0.2421386080D-04  | 0.4961760704D-07 |
| ANGULAR SEPRATION IN RADAR BEAM = , 0.1108811440D-01 |                  |                  |                   |                  |
| 7.900  | 0.1309168112D-04 | 0.1847605024D-01 | -0.9052458648D-02 | 0.6946527936D-02 |
|  | 0.8245285696D-06 | 0.8902397824D-02 | 0.2451468064D-04  | 0.5065158528D-07 |
| ANGULAR SEPRATION IN RADAR BEAM = , 0.1129189696D-01 |                  |                  |                   |                  |
| 8.000  | 0.1321089200D-04 | 0.1792606512D-01 | -0.9280720512D-02 | 0.7091778240D-02 |
|  |                  |                  |                   | 0.2431505312D-04 |



|   |                  |                  |                   |
|---|------------------|------------------|-------------------|
| 0.8983304832D-06                                      | 0.9150403840D-02 | 0.2482165344D-04 | 0.5167024000D-07  |
| ANGULAR SEPARATION IN RADAR BEAM = , 0.1149796192D-01 |                  |                  |                   |
| 8.100   | 0.1330676358D-04 | 0.1736231856D-01 | -0.9511208960D-02 |
| 0.9785303296D-06                                      | 0.9200269824D-02 | 0.2513467680D-04 | 0.7238301568D-02  |
|   |                  |                  | 0.5267019200D-07  |
| ANGULAR SEPARATION IN RADAR BEAM = , 0.1170632192D-01 |                  |                  |                   |
| 8.200   | 0.1340921284D-04 | 0.1678467520D-01 | -0.9743954688D-02 |
| 0.1071373544D-05                                      | 0.9352031872D-02 | 0.2545364064D-04 | 0.7386076480D-02  |
|   |                  |                  | 0.5364802176D-07  |
| ANGULAR SEPARATION IN RADAR BEAM = , 0.1191698896D-01 |                  |                  |                   |
| 8.300   | 0.1350815350D-04 | 0.1619299872D-01 | -0.9978984832D-02 |
| 0.1179748944D-05                                      | 0.9505725056D-02 | 0.2577842368D-04 | 0.7535080512D-02  |
|   |                  |                  | 0.5460954830D-07  |
| ANGULAR SEPARATION IN RADAR BEAM = , 0.1212997312D-01 |                  |                  |                   |
| 8.400   | 0.1360349920D-04 | 0.1558715040D-01 | -0.1021532440D-01 |
| 0.1307437680D-05                                      | 0.9661384320D-02 | 0.2610889504D-04 | 0.7685290368D-02  |
|   |                  |                  | 0.5554570112D-07  |
| ANGULAR SEPARATION IN RADAR BEAM = , 0.1234528384D-01 |                  |                  |                   |
| 8.500   | 0.1369516920D-04 | 0.1496699296D-01 | -0.1045599592D-01 |
| 0.1145945252D-05                                      | 0.9819042944D-02 | 0.2644491168D-04 | 0.7836681472D-02  |
|   |                  |                  | 0.5645664448D-07  |
| ANGULAR SEPARATION IN RADAR BEAM = , 0.1256292880D-01 |                  |                  |                   |
| 8.600   | 0.1378307504D-04 | 0.1433238432D-01 | -0.1069801896D-01 |
| 0.1642561824D-05                                      | 0.9978733952D-02 | 0.2678632128D-04 | 0.7989228608D-02  |
|   |                  |                  | 0.5734064896D-07  |
| ANGULAR SEPARATION IN RADAR BEAM = , 0.1278291456D-01 |                  |                  |                   |
| 8.700   | 0.1386712928D-04 | 0.1368318336D-01 | -0.1094241024D-01 |
| 0.1866083248D-05                                      | 0.114048920D-01  | 0.2713295904D-04 | 0.8142905280D-02  |
|   |                  |                  | 0.5819965632D-07  |
| ANGULAR SEPARATION IN RADAR BEAM = , 0.1300524624D-01 |                  |                  |                   |
| 8.800   | 0.1394724512D-04 | 0.1301924784D-01 | -0.1118918352D-01 |
| 0.2143444736D-05                                      | 0.1030433960D-01 | 0.2748464928D-04 | 0.8297684352D-02  |
|   |                  |                  | 0.5902628416D-07  |
| ANGULAR SEPARATION IN RADAR BEAM = , 0.1322992736D-01 |                  |                  |                   |
| 8.900   | 0.1402332920D-04 | 0.1234043328D-01 | -0.1143834912D-01 |
| 0.2492710304D-05                                      | 0.1047031480D-01 | 0.2784120480D-04 | 0.8433537472D-02  |
|   |                  |                  | 0.5982053952D-07  |
| ANGULAR SEPARATION IN RADAR BEAM = , 0.1345696048D-01 |                  |                  |                   |
| 9.000   | 0.1409529836D-04 | 0.1164659744D-01 | -0.1168991424D-01 |
| 0.2943222560D-05                                      | 0.103844344D-01  | 0.2820242496D-04 | 0.8610435456D-02  |
|   |                  |                  | 0.6058053248D-07  |
| ANGULAR SEPARATION IN RADAR BEAM = , 0.1368634640D-01 |                  |                  |                   |
| 9.100   | 0.1416306064D-04 | 0.103759616D-01  | -0.1194388192D-01 |
| 0.3537852832D-05                                      | 0.1080872280D-01 | 0.2856809856D-04 | 0.8768348032D-02  |
|   |                  |                  | 0.6130433664D-07  |
| ANGULAR SEPARATION IN RADAR BEAM = , 0.1391808400D-01 |                  |                  |                   |

|   |                  |                  |                    |                  |                  |
|---|------------------|------------------|--------------------|------------------|------------------|
| 9.200   | 0.142654880-04   | 0.1.21328344D 01 | -0.1220025152D-01  | 0.8927244160D-02 | 0.2656287488D-04 |
|   | 0.13673132D-05   | 0.1096126912D-01 | 0.2693800128D-04   | 0.6198813184D-07 |                  |
| ANGULAR SEPARATION IN RADAR BEAM = , 0.1415217152D-01 |                  |                  |                    |                  |                  |
| 9.300   | 0.1438558736D 04 | 0.947351744D 00  | -0.1245901888D-01  | 0.9087091840D-02 | 0.2671873312D-04 |
|   | 0.548911234D-05  | 0.111560168D-01  | 0.2931189504D-04   | 0.6263363584D-07 |                  |
| ANGULAR SEPARATION IN RADAR BEAM = , 0.1438860480D-01 |                  |                  |                    |                  |                  |
| 9.400   | 0.143401732D 04  | 0.8718153856D 00 | -0.11272017472D-01 | 0.9247857792D-02 | 0.2686902592D-04 |
|   | 0.717963628D-05  | 0.113330192D-01  | 0.2968953024D-04   | 0.6323510336D-07 |                  |
| ANGULAR SEPARATION IN RADAR BEAM = , 0.1462737840D-01 |                  |                  |                    |                  |                  |
| 9.500   | 0.143901752D 04  | 0.7947049344D 00 | -0.1298370608D-01  | 0.9409508608D-02 | 0.2701359616D-04 |
|   | 0.9840101880D-05 | 0.1151229808D-01 | 0.3007064320D-04   | 0.6379418880D-07 |                  |
| ANGULAR SEPARATION IN RADAR BEAM = , 0.1486848544D-01 |                  |                  |                    |                  |                  |
| 9.600   | 0.143550336D 04  | 0.7160061568D 00 | -0.1324959456D-01  | 0.9572009216D-02 | 0.2715229120D-04 |
|   | 0.143953526D-04  | 0.1169387328D-01 | 0.3045495744D-04   | 0.6430322944D-07 |                  |
| ANGULAR SEPARATION IN RADAR BEAM = , 0.1511191696D-01 |                  |                  |                    |                  |                  |
| 9.700   | 0.144760624D 04  | 0.6357050880D 00 | -0.1351781760D-01  | 0.9735324160D-02 | 0.2728498688D-04 |
|   | 0.231506272D-04  | 0.1187776336D-01 | 0.3084218176D-04   | 0.6476196672D-07 |                  |
| ANGULAR SEPARATION IN RADAR BEAM = , 0.1535766272D-01 |                  |                  |                    |                  |                  |
| 9.800   | 0.1451175626D 04 | 0.5537877888D 00 | -0.1378834704D-01  | 0.9899416832D-02 | 0.2741154560D-04 |
|   | 0.4401171254D-04 | 0.1206398480D-01 | 0.3123201184D-04   | 0.6517197248D-07 |                  |
| ANGULAR SEPARATION IN RADAR BEAM = , 0.1560570992D-01 |                  |                  |                    |                  |                  |
| 9.900   | 0.145424828D 04  | 0.4702404096D 00 | -0.1406114928D-01  | 0.1006425008D-01 | 0.2753180320D-04 |
|   | 0.115262894D-03  | 0.1225255216D-01 | 0.3162412928D-04   | 0.6552551360D-07 |                  |
| ANGULAR SEPARATION IN RADAR BEAM = , 0.1585604496D-01 |                  |                  |                    |                  |                  |
| 10.000  | 0.145681536D 04  | 0.3850494784D 00 | -0.1433618560D-01  | 0.1022978568D-01 | 0.2764560224D-04 |
|   | 0.8244761152D-03 | 0.1244347824D-01 | 0.3201820160D-04   | 0.6582226688D-07 |                  |
| ANGULAR SEPARATION IN RADAR BEAM = , 0.1610865184D-01 |                  |                  |                    |                  |                  |
| 10.100  | 0.1458865744D 04 | 0.298201792D 00  | -0.1461341120D-01  | 0.1039598488D-01 | 0.2775299168D-04 |
|   | 0.169334534 D-02 | 0.1263677376D-01 | 0.3241389224D-04   | 0.6606003456D-07 |                  |
| ANGULAR SEPARATION IN RADAR BEAM = , 0.1636351280D-01 |                  |                  |                    |                  |                  |
| 10.200  | 0.1460390336D 04 | 0.209684312D 00  | -0.1489277520D-01  | 0.105628776D-01  | 0.2785359296D-04 |
|   | 0.1412686734D-03 | 0.1283244736D-01 | 0.3281080960D-04   | 0.6623660992D-07 |                  |
| ANGULAR SEPARATION IN RADAR BEAM = , 0.1662060800D-01 |                  |                  |                    |                  |                  |
| 10.300  | 0.146137872D 04  | 0.1194843616D 00 | -0.1517422248D-01  | 0.1073021440D-01 | 0.2794744448D-04 |
|   | 0.479774944D-04  | 0.1363650512D-01 | 0.3320860832D-04   | 0.6635163200D-07 |                  |
| ANGULAR SEPARATION IN RADAR BEAM = , 0.1687991600D-01 |                  |                  |                    |                  |                  |

|  |                  |                   |                    |                   |                  |
|--|------------------|-------------------|--------------------|-------------------|------------------|
| 10.400   | 0.1441820480 04  | 0.2758965216D-01  | -0.1545768352D-01  | 0.1089816336D-01  | 0.2803439840D-04 |
|  | 0.2863814450-04  | 0.1323095152D-01  | 0.3360688000D-04   | 0.6639731072D-07  |                  |
| ANGULAR SEPRATION IN RADAR BEAM = , 0.1714141312D-01 |                  |                   |                    |                   |                  |
| 10.500   | 0.1461764540 04  | -0.6601171648D-01 | -0.1574309376D-01  | 0.1106661328D-01  | 0.2811434720D-04 |
|  | 0.1396507648D-04 | 0.1343378800D-01  | 0.3400524352D-04   | 0.6637513920D-07  |                  |
| ANGULAR SEPRATION IN RADAR BEAM = , 0.1740507360D-01 |                  |                   |                    |                   |                  |
| 10.600   | 0.1461023216D 04 | -0.1613312208D 00 | -0.1603037424D-01  | 0.1123552144D-01  | 0.2848719040D-04 |
|  | 0.9185584000D-05 | 0.1363901376D-01  | 0.3440325568D-04   | 0.6628290176D-07  |                  |
| ANGULAR SEPRATION IN RADAR BEAM = , 0.1767086976D-01 |                  |                   |                    |                   |                  |
| 10.700   | 0.1459766848D 04 | -0.2583798176D 00 | -0.1631944000D-01  | 0.1140484512D-01  | 0.2825282848D-04 |
|  | 0.6480529152D-05 | 0.1384662544D-01  | 0.3480049024D-04   | 0.6611053632D-07  |                  |
| ANGULAR SEPRATION IN RADAR BEAM = , 0.1793877168D-01 |                  |                   |                    |                   |                  |
| 10.800   | 0.1457920912D 04 | -0.3571679488D 00 | -0.1661019952D-01  | 0.1157454080D-01  | 0.2831117248D-04 |
|  | 0.480583952D-05  | 0.1405661712D-01  | 0.3519649920D-04   | 0.6587385280D-07  |                  |
| ANGULAR SEPRATION IN RADAR BEAM = , 0.1820874736D-01 |                  |                   |                    |                   |                  |
| 11.0.900   | 0.145547752D 04  | -0.4577053568D 00 | -0.1690255392D-01  | 0.1174456448D-01  | 0.2836213152D-04 |
|  | 0.3699780540D-05 | 0.1426898016D-01  | 0.3559081920D-04   | 0.6555268160D-07  |                  |
| ANGULAR SEPRATION IN RADAR BEAM = , 0.1848076256D-01 |                  |                   |                    |                   |                  |
| 11.000   | 0.1452423134D 04 | -0.5600015104D 00 | -0.1719639456D-01  | 0.1191487136D-01  | 0.2840564160D-04 |
|  | 0.2932486656D-05 | 0.1448370272D-01  | 0.3598297248D-04   | 0.65515087680D-07 |                  |
| ANGULAR SEPRATION IN RADAR BEAM = , 0.1875478080D-01 |                  |                   |                    |                   |                  |
| 11.100   | 0.1448733776D 04 | -0.6640648832D 00 | -0.1749160672D-01  | 0.1208541712D-01  | 0.2844162656D-04 |
|  | 0.2379330160D-05 | 0.1470077056D-01  | 0.3637246752D-04   | 0.6466632768D-07  |                  |
| ANGULAR SEPRATION IN RADAR BEAM = , 0.1903076352D-01 |                  |                   |                    |                   |                  |
| 11.200   | 0.1444452816D 04 | -0.7699032960D 00 | -0.1778860720D-01  | 0.1225615568D-01  | 0.2847002304D-04 |
|  | 0.1968078352D-05 | 0.1492016608D-01  | 0.3675879968D-04   | 0.6409696064D-07  |                  |
| ANGULAR SEPRATION IN RADAR BEAM = , 0.1930866912D-01 |                  |                   |                    |                   |                  |
| 11.300   | 0.1439511376D 04 | -0.8775239168D 00 | -0.1808564320D-01  | 0.1242704208D-01  | 0.2849077632D-04 |
|  | 0.1854435104D-05 | 0.1514186880D-01  | 0.3714144800D-04   | 0.6343889344D-07  |                  |
| ANGULAR SEPRATION IN RADAR BEAM = , 0.1958845688D-01 |                  |                   |                    |                   |                  |
| 11.400   | 0.1433919040D 04 | -0.9869329536D 00 | -0.18388419472D-01 | 0.1259802976D-01  | 0.2850383872D-04 |
|  | 0.1410082496D-05 | 0.1536585488D-01  | 0.3751880640D-04   | 0.6269015168D-07  |                  |
| ANGULAR SEPRATION IN RADAR BEAM = , 0.1987007424D-01 |                  |                   |                    |                   |                  |
| 11.500   | 0.1427664576D 04 | -0.1098135904D 01 | -0.1868357184D-01  | 0.1276907244D-01  | 0.2850917024D-04 |
|  | 0.1216268128D-05 | 0.1559209776D-01  | 0.3789355008D-04   | 0.6185067392D-07  |                  |

ANGULAR SEPRATION IN RADAR BEAM = , 0.2015347936D-01

11.600 0.142073728D 04 -0.1211137168D 01 -0.1888361680D-01 0.1324012432D-01 0.2850673824D-04  
0.1086108320D-05 0.1582056688D-01 0.3826189920D-04 0.6091675904D-07

ANGULAR SEPRATION IN RADAR BEAM = , 0.20438661904D-01

11.700 0.1413127350D 04 -0.1325940304D 01 -0.1928416192D-01 0.1311111372D-01 0.2849651808D-04  
0.9325814272D-06 0.1605122864D-01 0.3862435520D-04 0.5988663360D-07

ANGULAR SEPRATION IN RADAR BEAM = , 0.2072544032D-01

11.800 0.141482800D 04 -0.1442547760D 01 -0.1958503088D-01 0.1328206672D-01 0.2847849472D-04  
0.8271928128D-06 0.1628404624D-01 0.3898033440D-04 0.5875675648D-07

ANGULAR SEPRATION IN RADAR BEAM = , 0.2101388736D-01

11.900 0.1395813216D 04 -0.1560960928D 01 -0.1988603776D-01 0.1345286432D-01 0.2845265984D-04  
0.7391783424D-06 0.1651897856D-01 0.3932924288D-04 0.5752738624D-07

ANGULAR SEPRATION IN RADAR BEAM = , 0.2130390128D-01

12.000 0.1366087664D 04 -0.1681180096D 01 -0.2018698800D-01 0.1362346320D-01 0.2841901472D-04  
0.6649795776D-06 0.1675596192D-01 0.3967047392D-04 0.5619888256D-07

ANGULAR SEPRATION IN RADAR BEAM = , 0.2159542112D-01

12.100 0.1375635408D 04 -0.1803204272D 01 -0.2048767632D-01 0.1379387690D-01 0.2837756896D-04  
0.601894560D-06 0.1699500768D-01 0.4000341184D-04 0.5476429824D-07

ANGULAR SEPRATION IN RADAR BEAM = , 0.2188838336D-01

12.200 0.1364445648D 04 -0.1927031248D 01 -0.2078788992D-01 0.1396339984D-01 0.2832834048D-04  
0.5478455350D-06 0.1723600480D-01 0.4032743072D-04 0.5322607616D-07

ANGULAR SEPRATION IN RADAR BEAM = , 0.2218272096D-01

12.300 0.1352507488D 04 -0.2052657552D 01 -0.2108740464D-01 0.1413380128D-01 0.2827135584D-04  
0.5012111680D-06 0.1747891776D-01 0.4084189568D-04 0.5157937344D-07

ANGULAR SEPRATION IN RADAR BEAM = , 0.2247836512D-01

12.400 0.1339810128D 04 -0.2180078240D 01 -0.2138598800D-01 0.1430323920D-01 0.2820665088D-04  
0.4617135550D-06 0.1772368720D-01 0.4094616416D-04 0.4982689984D-07

ANGULAR SEPRATION IN RADAR BEAM = , 0.2277524416D-01

12.500 0.1326342944D 04 -0.2309287040D 01 -0.2168339840D-01 0.1447226592D-01 0.2813427040D-04  
0.4253340320D-06 0.1797024992D-01 0.4123958624D-04 0.4796409984D-07

ANGULAR SEPRATION IN RADAR BEAM = , 0.2307328256D-01

12.600 0.1312095152D 04 -0.2440276192D 01 -0.2197938400D-01 0.1464083520D-01 0.2805426752D-04  
0.3942517952D-06 0.1821853920D-01 0.4152150528D-04 0.4599213568D-07

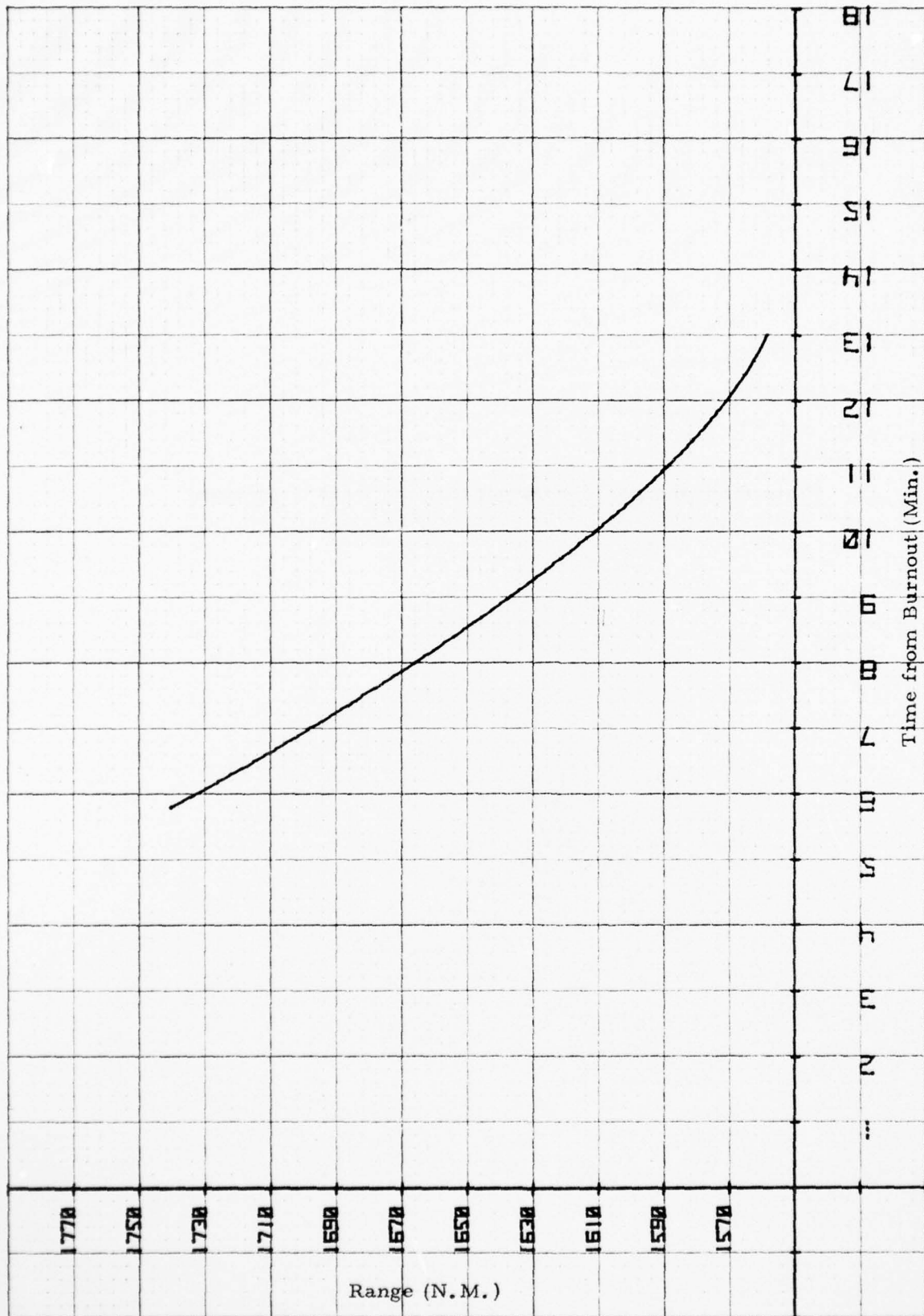
ANGULAR SEPRATION IN RADAR BEAM = , 0.2337240320D-01

12.700 0.1297058180D 04 -0.2573136288D 01 -0.2227368544D-01 0.1480890192D-01 0.2796670432D-04  
0.3648008736D-06 0.1846848384D-01 0.4179126048D-04 0.4390863296D-07

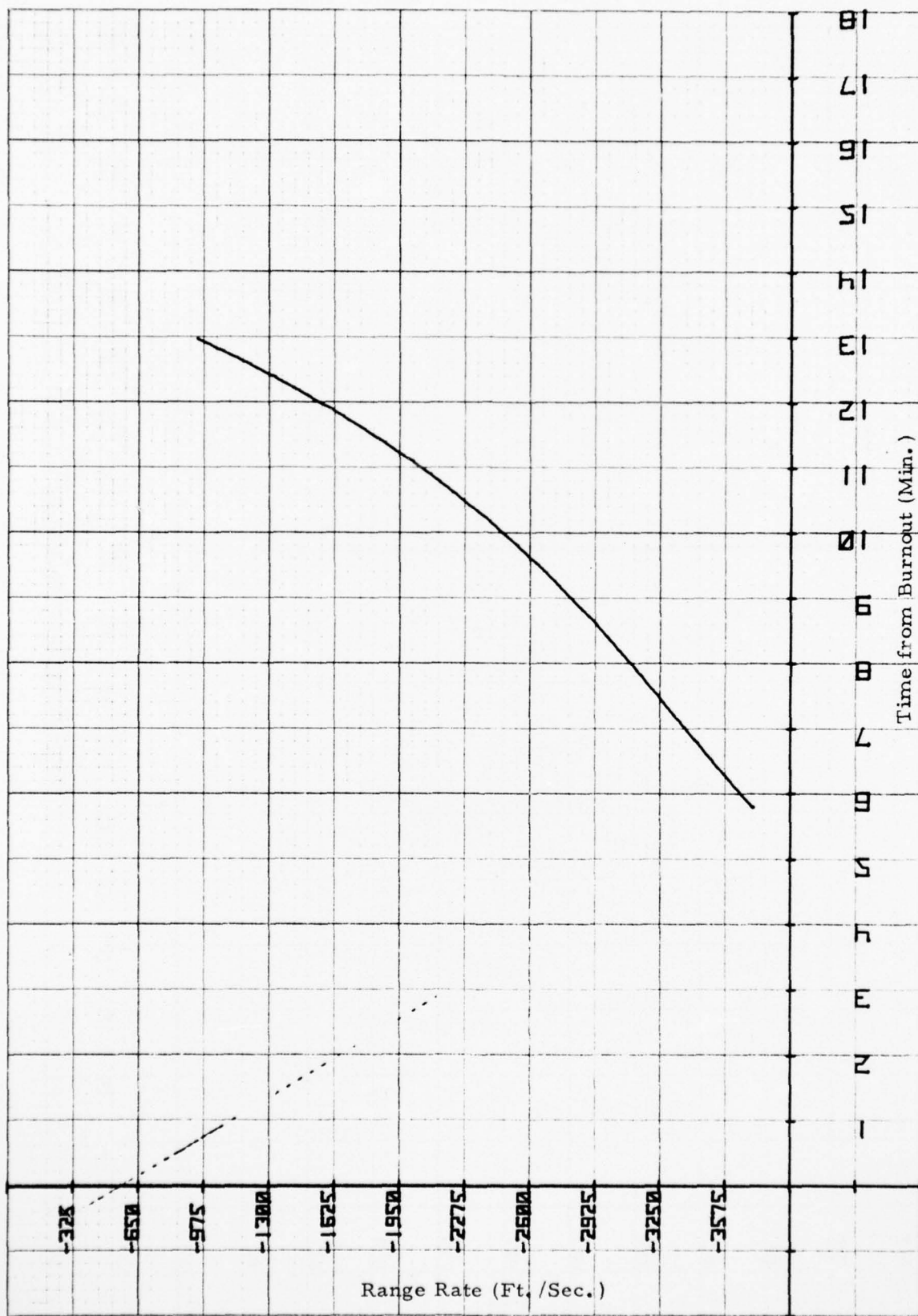




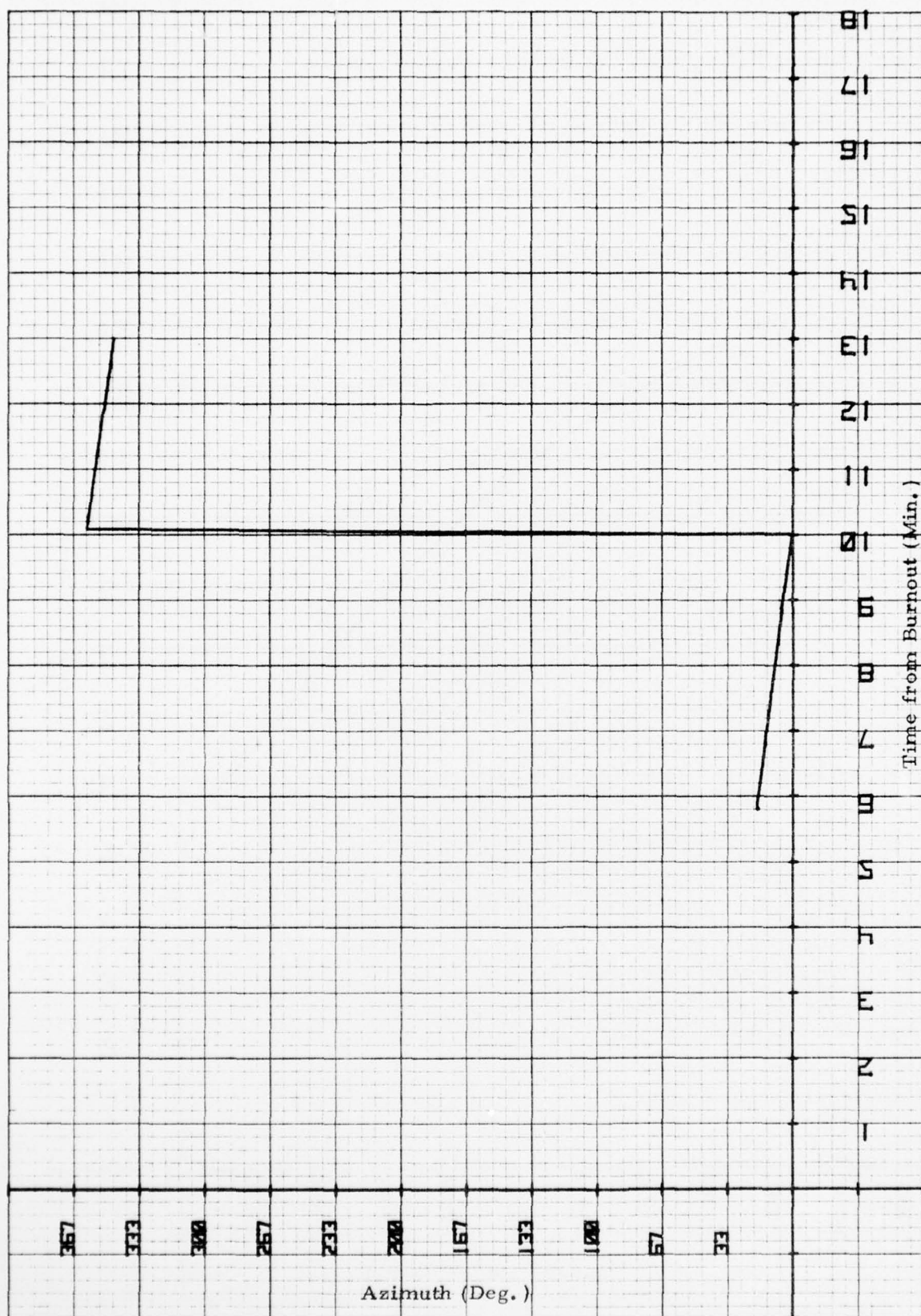
Plots from the Sample Output (for the first trajectory)



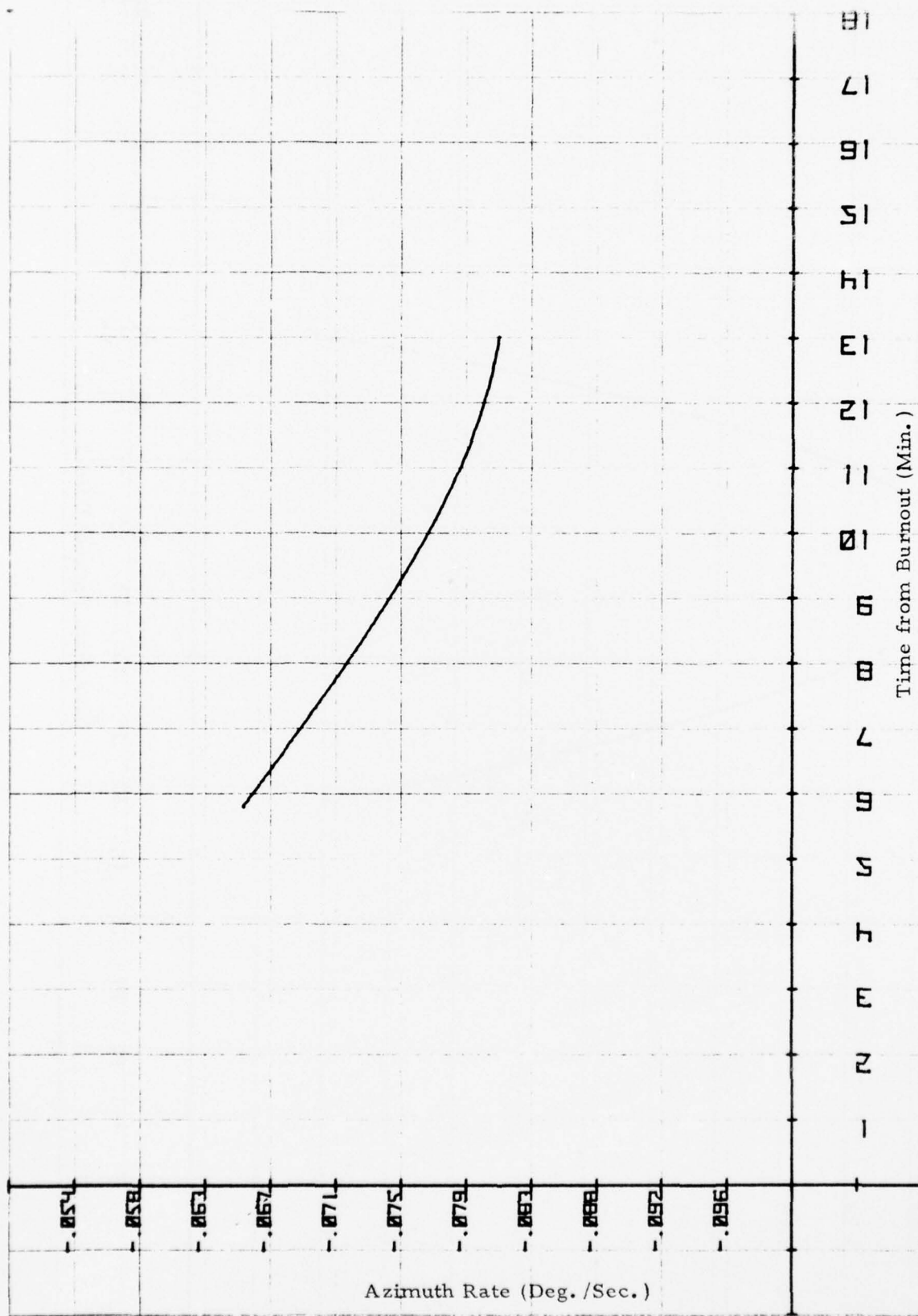
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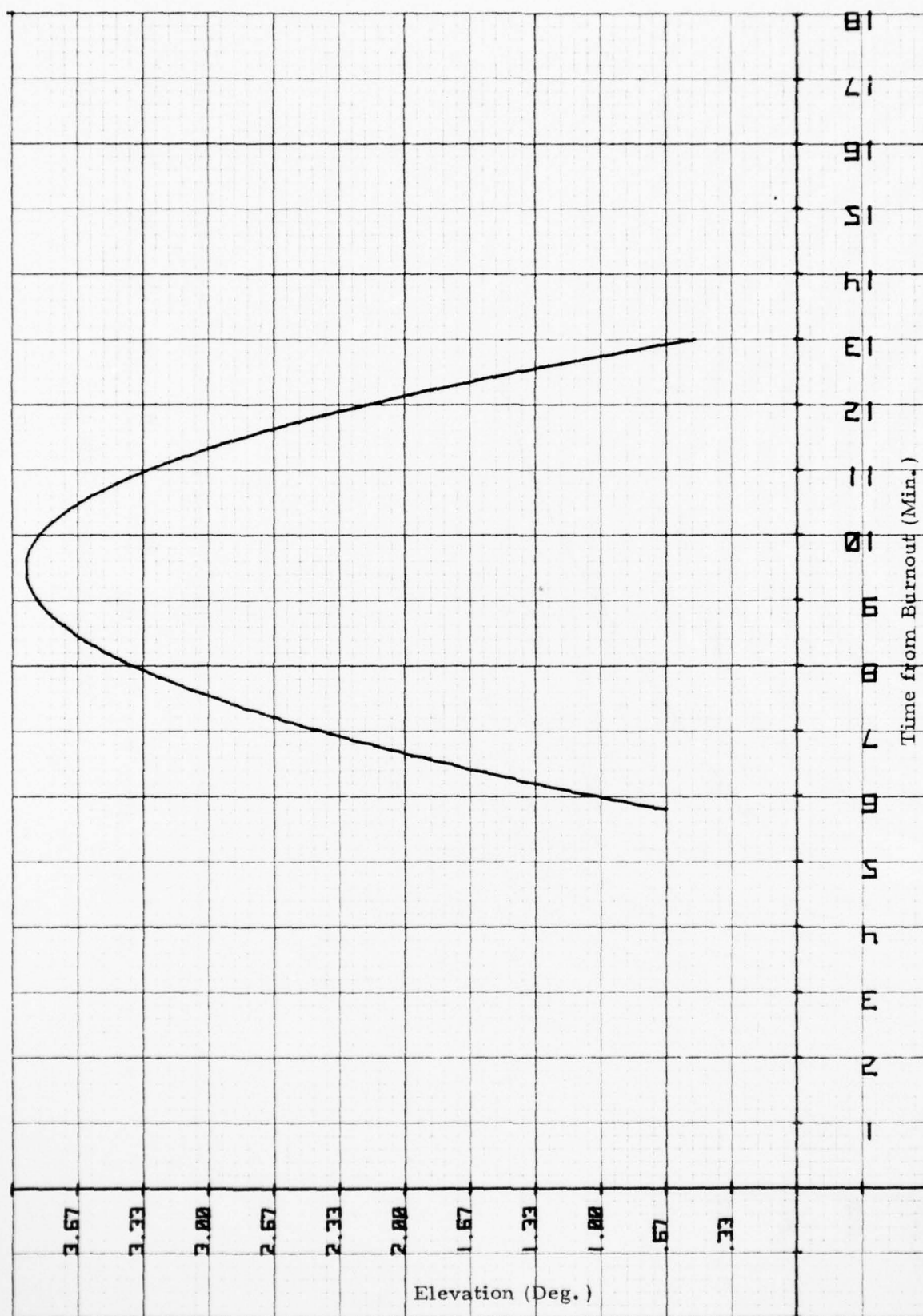




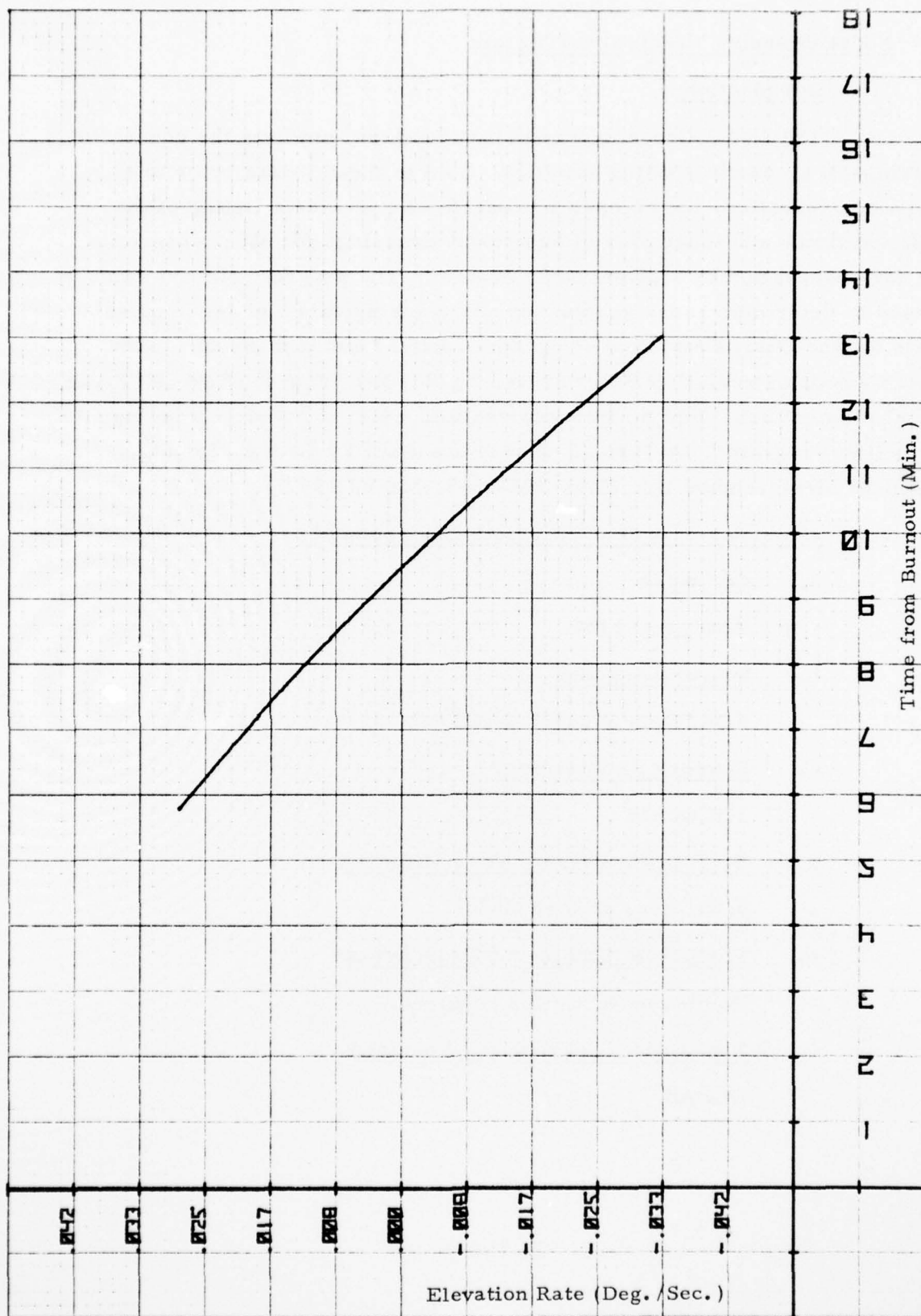


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#### D. Nodal Crossing Prediction Program

##### 1. Introduction

The Nodal Crossing Prediction Program predicts the equatorial crossings of an earth-orbiting satellite. Two to three weeks prior to a satellite observation, the computer program can provide a listing of the predicted times and longitudes of equatorial crossings for all passes suitable for observation by a given radar system. The program outputs can be used to determine radar acquisition and tracking data and are used as inputs for the Orbit Prediction Program. Orbital element inputs for the Nodal Crossing Prediction Program can be obtained from the SPACETRACK orbital element set. For further information, refer to "Nodal Crossing Prediction Program", by John C. Cleary and Paul E. Brown, 1st Lt., Technical Memorandum No. EMA-TM-66-9, March 1967.

##### 2. Computer Program Operating Environment

###### a. Computer

Honeywell 6180.

###### b. Source Language

FORTRAN Y under GCOS.

###### c. Memory Requirement

17K words

###### d. Typical Processing Time Required

0.001 hrs. (3.6 seconds)

###### e. Peripheral Equipment Requirement

No disc or tape files required.

###### f. Non-system Subroutines Required

CLEAR

### 3. Inputs

The following set of input parameters are required for the execution of the Nodal Crossing Prediction Program.

#### NAMelist IN1

NCASE - Number of cases to be run.

#### NAMelist IN2

HED - Array containing the heading for the output. The dimension of HED is 24.

#### NAMelist IN3

NTYPE - Switch for selecting orbital elements type to be input.

=1 SPACETRACK or Smithsonian elements used as inputs.

=2 NASA elements.

NREV0 - First revolution of satellite to be examined for visibility from radar. The revolutions are counted from epoch time of the SPACETRACK bulletin.

NREV1 - Last revolution of satellite to be examined for visibility from radar.

#### NAMelist IN4

BGT - Epoch time of nodal crossing bulletin in decimal days.  $BGT = 39125 - T$  where 39125 is January 1, 1966 in Julian Days and T is the epoch time.

XM0 - Mean anomaly in degrees.

RA0 - Right ascension of ascending node in degrees.

OMEGA0 - Argument of perigee (degrees).

E - Orbit eccentricity.

A - Mean motion (revolutions/day).

#### NAMelist IN5

B - Rate of change of A (revolutions/day<sup>2</sup>).

RA1 - Rate of change of RA0 (degrees/day).

OMEGA1 - Rate of change of OMEGA0 (degrees/day).

GHA0 - Greenwich hour angle of Aries at midnight, 30 December of the previous year.

#### NAMELIST IN6

ZLAM1 - Longitude of northbound nodal crossings that will give a Zenith pass at the radar (degrees).

ZLAM2 - Longitude of southbound nodal crossings that will give a Zenith pass at the radar (degrees).

DLAMDA - Longitude interval of nodal crossings that will give usable passes at the radar (degrees).

CHR - Difference between local time and Greenwich time.

= 4.0 EDT

= 5.0 EST

#### 4. Output

Output from the Nodal Crossing Prediction Program first consists of a list of the input parameters. This is followed by a listing of the nodal crossing data in the following form:

| <u>Variable Name</u> | <u>Units</u> | <u>Description</u>  |
|----------------------|--------------|---|
| HED                  | None         | Heading for output as input.  |
| BGT                  | Decimal Days | Epoch time of nodal crossing bulletin.  |
| NREV0, NREV1         | None         | Pass number. Indicates the first through last revolution of the satellite to be examined for visibility from the radar. |
| ZLAM1                | Degrees      | Longitude of northbound nodal crossings that will give a Zenith pass at the radar.                                      |
| ZLAM2                | Degrees      | Longitude of southbound nodal crossings that will give a Zenith pass at the radar.                                      |
| DLAMDA               | Degrees      | Longitude interval of nodal crossings that will give usable passes at the radar.  |
| NDAY                 | Days         | Day of year of nodal crossing.  |
| NHR                  | Hours        | Hour of day of nodal crossing.  |
| MIN                  | Minutes      | Minute of hour of nodal crossing.   |
| NSEC                 | Seconds      | Second of minute of nodal crossing.   |

| <u>Variable Name</u> | <u>Units</u> | <u>Description</u>           |
|----------------------|--------------|------------------------------|
| PLAMDA               | Degrees      | Longitude of nodal crossing. |

The printout produced from the variables HED through DLAMDA above serves as a heading for each page of nodal crossing data printed out. The nodal crossing times and longitude (variables NDAY through PLAMDA) are printed out in the order of ascending times on each page. Refer to the sample output.



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SPACE SURVEILLANCE SOFTWARE SUPPORT. VOLUME 1, PART 1, BOOK 1, --ETC(U)

OCT 76 P R CONTI

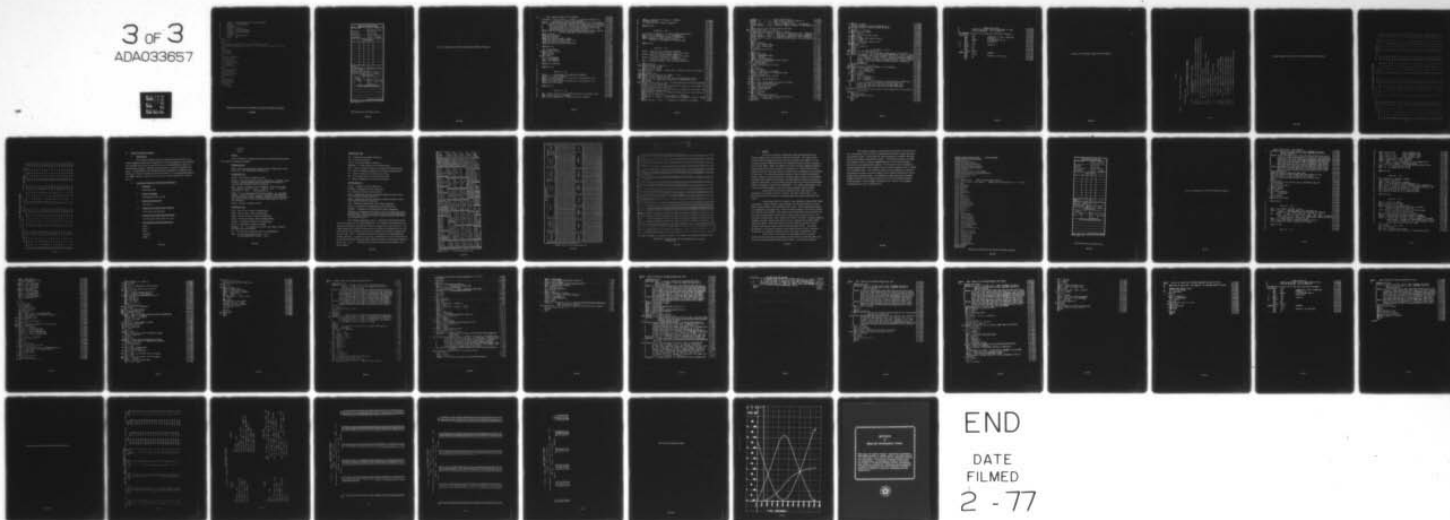
F30602-75-C-0167

UNCLASSIFIED

RADC-TR-76-261-VOL-1-PT-1- NL

3 of 3

ADA033657



END

DATE  
FILMED  
2 - 77

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$      IDENT  CLEARY,NEUFFER ,65121104RADC
$      USERID CLEARY$THREE
$      LOULOAD
$      OPTION  FORTAN
$      SELECT  CLEARY/ONODAL
$      SELECT  CLEARY/OCLEAR
$      EXECUTE
$      LIMITS  20,20K,,10K
$      DATA   05

$IN1
  NCASE=1 $
$IN2
  HED(4)=34N NODAL CROSSING PREDICTION PROGRAM,
  HED(14)=47MSATELLITE NO. 049 - SPACETRACK - BLTN. 342 EDT3
$IN3
  NTYPE=1,
  NREVO=75,
  NREVI=460 $
$IN4
  BGT=118.08902403,
  LMO=203.7813,
  RAO=234.2461,
  OMEGA0=158.7564,
  E=0.0570891,
  A=12.76771656 $
$IN5
  B=0.255741E-03,
  RA1=-3.46557,
  OMEGA1=3.31952,
  GHAO=99.210 $
$IN6
  ZLAM1=134.2,
  ZLAM2=191.9,
  DLAMDA=50.0,
  CHR=4.0 $
$      ENDJOB

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Sample Job Stream for the Nodal Crossing Prediction Program

| <b>RADC 635/645 BATCH JOB</b>  |       |   |              |       |
|--|-------|---|--------------|-------|
| SNUM# NUMBER   |       | DATE  | TIME         |       |
|  |       | 4/5/76  | 1115         |       |
| PROGRAMMER   |       | TELEPHONE   |              |       |
| CONTI  |       | 339-1360  |              |       |
| RADC ENGINEER  |       | TELEPHONE   | SYMBOL       |       |
| CLEARY   |       | 3573  | OCSA         |       |
| TAPES ASSIGNED   |       |   |              |       |
| REEL NO.   | WRITE | READ  | DEN.         | TITLE |
|  |       |   |              |       |
|  |       |   |              |       |
|  |       |   |              |       |
|  |       |   |              |       |
|  |       |   |              |       |
|  |       |   |              |       |
|  |       |   |              |       |
|  |       |   |              |       |
|  |       |   |              |       |
| PERIPHERALS ASSIGNED <input checked="" type="checkbox"/> READER <input checked="" type="checkbox"/> PRINTER <input type="checkbox"/> PUNCH<br><input type="checkbox"/> DISC. # OF LINKS <input type="checkbox"/> DRUM # OF LINKS |       |   |              |       |
| CORE SIZE    20K   |       | ACTIVITIES    1   |              |       |
| PROCESSOR TIME    .01  |       | ESTIMATED LINES OF PRINT    1,000                                       |              |       |
| TOTAL RUN TIME    .01  |       |   |              |       |
| DECKS EXPECTED   |       |   |              |       |
| NO. OF BINARY DECKS<br>None  |       | NO. OF COMDECKS   |              |       |
| BMC  |       | TAPE <input type="checkbox"/> DUMP <input type="checkbox"/> COPY        |              |       |
| FROM:  | TO:   | MODE<br><input type="checkbox"/> BCD<br><input type="checkbox"/> BINARY | NO. OF FILES |       |
| SPECIAL OPERATOR INSTRUCTIONS  |       |   |              |       |
|  |       |   |              |       |
|  |       |   |              |       |
|  |       |   |              |       |
|  |       |   |              |       |
|  |       |   |              |       |
| (Use reverse side if required)   |       |   |              |       |

RADC FORM 0-56 PREVIOUS EDITION WILL BE USED  
APR 69

HIS 6000 Batch Submittal Form

Source Listing of the Nodal Crossing Prediction Program



|    |   |          |
|----|---|----------|
| C  | NODAL CROSSING PREDICTION PROGRAM                                 | 00001000 |
| C  |   | 00001010 |
|    | DIMENSION TO(1000),NDAY(100),NHR(1000),MIN(1000),NSEC(1000),      | 00001020 |
| 1  | XLAMDA(1000),PLAMDA(1000),HED(24)                                 | 00001030 |
|    | COMMON TO,NDAY,NHR,MIN,NSEC,XLAMDA,PLAMDA,HED,RAD,PI,NTYPE,NREVO, | 00001040 |
| 1  | NREV1,X,BGT,E,OMEGA,OMEGA1,XM0,P,DELP,A,B,C,GHA0,GHA1,RA0,        | 00001050 |
| 2  | RA1,ZLAM1,ZLAM2,PN,COSW,SINW,TERM,COSPH,SINPH,PHIP,DLAMDA,        | 00001060 |
| 3  | XMP,TERN1,NPASS,REV,J,I,DAY,HOUR,YMIN,SEC,NPAGE,IPAGE,            | 00001070 |
| 4  | JSTART,JEND,NCOL,JC1,JC2,JC3,JC4,CHR,CDAY                         | 00001080 |
|    | DOUBLE PRECISION GHA1,BGT,XM0,RA0,OMEGA0,E,A,B,RA1,OMEGA1,GHA0,P, | 00001090 |
| 1  | PN,TERM,TERM1,DELP,C,XMP,PI,RAD,DSQRT                             | 00001100 |
|    | DATA BLANK/6H /   | 00001110 |
|    | NAMelist/IN1/NCASE  | 00001120 |
|    | NAMelist/IN2/HED  | 00001130 |
|    | NAMelist/IN3/NTYPE,NREVO,NREV1                                    | 00001140 |
|    | NAMelist/IN4/BGT,XM0,RA0,OMEGA0,E,A                               | 00001150 |
|    | NAMelist/IN5/B,RA1,OMEGA1,GHA                                     | 00001160 |
|    | NAMelist/IN6/ZLAM1,ZLAM2,DLAMDA,CHR                               | 00001170 |
| G  |   | 00001180 |
|    | READ(05,IN1)  | 00001190 |
| C  |   | 00001200 |
|    | DO 51 N=1,NCASE   | 00001210 |
| 2  | CALL CLEAR(TO,CDAY)   | 00001220 |
|    | DO 99 I=1,24  | 00001230 |
|    | HED(I)=BLANK  | 00001240 |
| 99 | CONTINUE  | 00001250 |
|    | PI = 3.1415926536   | 00001260 |
|    | RAD = .0174532925   | 00001270 |
|    | GHA1 = 360.9856473  | 00001280 |
| C  |   | 00001290 |
|    | READ(05,IN2,END=51)   | 00001300 |
| C  |   | 00001310 |
|    | READ(05,IN3)  | 00001320 |
| C  |   | 00001330 |
| C  |   | 00001340 |
| C  | NAMelist - IN3  | 00001350 |
| C  |   | 00001360 |
| C  | NTYPE = 1 - SPACETRACK OR SMITHSONIAN ELEMENTS                    | 00001370 |
| C  | NTYPE = 2 - NASA ELEMENTS   | 00001380 |
| C  | NREVO = FIRST REVOLUTION OF SATELLITE TO BE EXAMINED FOR          | 00001390 |
| C  | VISIBILITY FROM RADAR   | 00001400 |
| C  | NREV1 = LAST REVOLUTION OF SATELLITE TO BE EXAMINED FOR           | 00001410 |
| C  | VISIBILITY FROM RADAR   | 00001420 |
| C  |   | 00001430 |
|    | READ(05,IN4)  | 00001440 |
| C  |   | 00001450 |
| C  |   | 00001460 |
| C  | NAMelist - IN4  | 00001470 |
| C  |   | 00001480 |
| C  | BGT = EPOCH TIME OF NODAL CROSSING BULLETIN IN DECIMAL DAYS       | 00001490 |
| C  | XM0 = MEAN ANOMALY IN DEGREES                                     | 00001500 |
| C  | RA0 = RIGHT ASCENSION OF ASCENDING NODE IN DEGREES                | 00001510 |

|      |   |         |
|------|---|---------|
| C    | OMEGAO = ARGUMENT OF PERIGEE IN DEGREES                           | 0001520 |
| C    | E = ECCENTRICITY  | 0001530 |
| C    | A = MEAN MOTION IN REVOLUTIONS/DAY                                | 0001540 |
| C    |   | 0001550 |
|      | READ(05,IN5)  | 0001560 |
| C    |   | 0001570 |
| C    |   | 0001580 |
| C    | NAMELIST - IN5  | 0001590 |
| C    |   | 0001600 |
| C    | B = RATE OF CHANGE OF A IN REVOLUTIONS/(DAY-SQUARED)              | 0001610 |
| C    | RA1 = RATE OF CHANGE OF RA IN DEGREES/DAY                         | 0001620 |
| C    | OMEGA1 = RATE OF CHANGE OMEGA0 IN DEGREES/DAY                     | 0001630 |
| C    | GMA0 = GREENWICH HOUR ANGLE OF ARIES AT                           | 0001640 |
| C    | MIDNIGHT, 30 DECEMBER OF PREVIOUS YEAR                            | 0001650 |
| C    |   | 0001660 |
|      | READ(05,IN6)  | 0001670 |
| C    |   | 0001680 |
| C    |   | 0001690 |
| C    | NAMELIST - IN6  | 0001700 |
| C    |   | 0001710 |
| C    | LAM1 = LONGITUDE OF NORTHBOUND CROSSING                           | 0001720 |
| C    | THAT WILL GIVE A ZENITH PASS AT THE RADAR                         | 0001730 |
| C    | LAM2 = LONGITUDE OF SOUTHBOUND CROSSING                           | 0001740 |
| C    | THAT WILL GIVE A ZENITH PASS AT THE RADAR                         | 0001750 |
| C    | LAMDA = LONGITUDE INTERVAL OF CROSSINGS                           | 0001760 |
| C    | THAT WILL GIVE USEABLE PASSES AT RADAR                            | 0001770 |
| C    | EMR = DIFFERENCE BETWEEN LOCAL AND GREENWICH TIME                 | 0001780 |
| C    |   | 0001790 |
|      | WRITE(06,9001)  | 0001800 |
| 9001 | FORMAT(1H1,49X,'- INPUTS -')                                      | 0001810 |
|      | IF(N.GT.1) GO TO 998  | 0001820 |
|      | WRITE(06,9002) NCASE  | 0001830 |
| 9002 | FORMAT(//19X,'NCASE = ',12,5X,'TOTAL NUMBER OF CASES TO BE RUN')  | 0001840 |
|      | GO TO 999   | 0001850 |
| 998  | WRITE(06,9003) N  | 0001860 |
| 9003 | FORMAT(//19X,'THIS IS RUN NUMBER ',12)                            | 0001870 |
| 999  | WRITE(06,9004) (HED(I),I=1,24)                                    | 0001880 |
| 9004 | FORMAT(//19X,'OUTPUT HEADING (HED)',/24X,12A6,/24X,12A6)          | 0001890 |
|      | WRITE(06,9005) NTYPE,NREV,NREV1,BGT,XMC,RAO,OMEGA,E,A,B,          | 0001900 |
|      | RA1,OMEGA1  | 0001910 |
| 9005 | FORMAT(//19X,'NTYPE = ',15,' 1-SPACETRACK OR SMITHSONIAN ELEMENTS | 0001920 |
|      | 1,32X,' =2-NASA ELEMENTS',  | 0001930 |
|      | 19X,'NERVO = ',16,' FIRST REVOLUTION OF SATELLITE FROM EPOCH TIME | 0001940 |
|      | E OF THE SPACETRACK BULLETIN',                                    | 0001950 |
|      | 19X,'NREV1 = ',16,' LAST REVOLUTION OF SATELLITE FROM EPOCH TIME  | 0001960 |
|      | OF THE SPACETRACK BULLETIN',                                      | 0001970 |
|      | 19X,'BGT = ',F16.10,' BGT=39125-T(39125 IS JULIAN DAYS FOR JAN 10 | 0001980 |
|      | 986,T IS THE EPOCH TIME',   | 0001990 |
|      | 19X,'XMC = ',F16.10,' MEAN ANOMALY IN DEGREES',                   | 0002000 |
|      | 19X,'RAO = ',F16.10,' RIGHT ASCENSION OF ASCENDING NODE IN DEGREE | 0002010 |
|      | 8S',  | 0002020 |
|      | 19X,'OMEGAO = ',F16.10,' ARGUMENT OF PERIGEE IN DEGREES',         | 0002030 |





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19  DO 20 I=1,NPASS                                00002560
   IF (ABS (XLAMDA(I)-ZLAM1)-DLAMDA) 21,21,20      00002570
20  IF (ABS (XLAMDA(I)-ZLAM2)-DLAMDA) 21,21,20      00002580
21  J = J+1                                           00002590
   PLAMDA(J) = XLAMDA(I)                             00002600
22  NDAY(J) = TO(I)-CDAY                             00002610
   DAY = NDAY(J)                                       01002620
   HOUR = (TO(I)-DAY)*24.0-CHR                       00002630
23  NHR(J)=HOUR                                       00002640
   YMIN = (HOUR-FLOAT (NHR(J)))*60.0                00002650
24  MIN(J) = YMIN                                     00002660
   SEC = (YMIN-FLOAT (MIN(J)))*60.0                  00002670
25  NSEC(J) = SEC+.5                                  00002680
26  CONTINUE                                           00002690
   NPAGE = (J+99)/100                                00002700
   IPAGE = 1                                           00002710
27  WRITE (6,1003) (HED(I),I=1,24)                  00002720
1003  FORMAT(1W1,23X12A6/24X12A6//)                  00002730
   WRITE (6,1004) BGT,NREVU,NREV1,ZLAM1,ZLAM2,DLAMDA 00002740
1004  FORMAT(18X12HEPOCH TIME =F9.5,5H DAYS,37X8HPASS NO. 14,2H - 14/11X00002750
1      10HLAMBDAZ1 =F8.3,22X10HLAMBDAZ2 =F8.3,20X14HDELTA LAMBDA =00002760
2      F8.3 //3X3HDAY,1X3HHR,1X4HMIN,,1X4HSEC,,1X6HLAMBDA,6X3HDAY00002770
3      1X3HHR,,1X4HMIN,,1X4HSEC,,1X6HLAMBDA,6X3HDAY,1X3HHR,1X4HMIN.00002780
4      1X4HSEC,,1X6HLAMBDA,6X3HDAY,1X3HHR,1X4HMIN,,1X4HSEC,,1X00002790
5      6HLAMBDA )
   IF (NPAGE) 28,28,29                                00002800
28  WRITE (6,1005)                                     00002810
1005  FORMAT(43X34HNO VISIBLE PASSES IN THIS INTERVAL ) 00002820
29  JSTART = 100*(IPAGE-1)+1                          00002830
   JEND = MIN0 (JSTART+99,J)                          00002840
   NCOL = (JEND-JSTART+4)/4                            00002850
30  DO 32 I=1,NCOL                                    00002860
   JC1 = JSTART+I-1                                    00002870
   JC2 = MIN0 (JC1+NCOL,J)                            00002880
   JC3 = MIN0 (JC2+NCOL,J)                            00002890
   JC4 = MIN0 (JC3+NCOL,J)                            00002900
31  WRITE (6,1006) NDAY(JC1),NHR(JC1),MIN(JC1),NSEC(JC1), 00002910
1      PLAMDA(JC1),NDAY(JC2),NHR(JC2),MIN(JC2),NSEC(JC2), 00002920
2      PLAMDA(JC2),NDAY(JC3),NHR(JC3),MIN(JC3),NSEC(JC3), 00002930
3      PLAMDA(JC3),NDAY(JC4),NHR(JC4),MIN(JC4),NSEC(JC4), 00002940
4      PLAMDA(JC4)                                     00002950
1006  FORMAT(/16,14,14,14,F9.2,19,14,14,14,F9.2,19,14, 00002960
1      14,14,F9.2 )                                   00002970
32  CONTINUE                                           00002980
   IPAGE = IPAGE+1                                     00002990
   IF (IPAGE-NPAGE) 27,27,51                          00003000
51  CONTINUE                                           00003010
   STOP                                               00003020
   END                                               00003030

```



|       |   |        |       |          |
|-------|---|--------|-------|----------|
| •     | SUBROUTINE CLEAR  |        |       | 00001000 |
| •     | SUBROUTINE TO SET FORTRAN LOCATIONS TO ZERO               |        |       | 00001010 |
| •     | CALLING SEQUENCE - CALL CLEAR(X,Y)                        |        |       | 00001020 |
| •     |   |        |       | 00001030 |
| •     | THE PURPOSE OF CLEAR IS TO ZERO OUT LOCATIONS X THROUGH Y |        |       | 00001040 |
|       | CLEAR   | SAVE   | 1,4   | 00001050 |
|       |   | LDA    | 2,1   | 00001060 |
|       |   | SBA    | 3,1   | 00001070 |
|       |   | TPL    | ORDER | 00001080 |
|       |   | LDX4   | 2,1   | 00001090 |
| A2    |   | STZ    | 0,4   | 00001100 |
|       |   | EAX4   | 1,4   | 00001110 |
| A1    |   | CMPLX4 | 3,1   | 00001120 |
|       |   | TNC    | A2    | 00001130 |
|       |   | TZE    | A2    | 00001140 |
|       |   | RETURN | CLEAR | 00001150 |
| ORDER |   | LDX4   | 3,1   | 00001160 |
|       |   | LDQ    | -1,DU | 00001170 |
|       |   | ASQ    | A1    | 00001180 |
|       |   | TRA    | A2    | 00001190 |
|       |   | END    |       | 00001200 |

ADDRESS OF X INTO A REGISTER  
 ADDRESS OF Y  
 Y IS GREATER THAN X  
 RESTORE X4  
 INCRE X4  
 REORDER  
 CHANGE A1 TO CMPL 2,1

Listing of the Sample Input for the Program

- INPUTS -

NCASE = 1 TOTAL NUMBER OF CASES TO BE RUN

OUTPUT HEADING (HED)

NODAL CROSSING PREDICTION PROGRAM  
SATELLITE NO. 049 = SPACETRACK - RLTN. 342 EDT

NTYPE = 1 1-SPACETRACK OR SMITHSONIAN ELEMENTS  
=2-NASA ELEMENTS

NERV = 75 FIRST REVOLUTION OF SATELLITE FROM EPOCH TIME OF THE SPACETRACK BULLETIN

NREV1 = 46 LAST REVOLUTION OF SATELLITE FROM EPOCH TIME OF THE SPACETRACK BULLETIN

33T = 118.690247800 HGT=39125-T(39125 IS JULIAN DAYS FOR JAN 1966,T IS THE EPOCH TIME

XV = 213.7418 00000 MEAN ANOMALY IN DEGREES

RA = 234.24610 000 RIGHT ASCENSION OF ASCENDING NODE IN DEGREES

OMEGA1 = 158.756400000 ARGUMENT OF PERIGEE IN DEGREES

E = 0.570891000 ORBIT ECCENTRICITY

A = 12.7677165632 MEAN MOTION IN REVOLUTIONS/DAY

B = 0.02557410 RATE IN CHANGE OF A

RA1 = -3.46557 0032 RATE OF CHANGE OF RA IN DEGREES/DAY

OMEGA1 = 3.319520000 RATE OF CHANGE OF OMEGA IN DEGREES/DAY

GA10 = 99.21000 000 GREENWICH HOUR ANGLE OF ARIES AT NIGHT

Z-AM1 = 134.20 00076 LONGITUDE OF NORTHRound NODAL CROSSING

Z-AM2 = 191.89999962 LONGITUDE OF SOUTHRound NODAL CROSSING

D-LMNA = 50.0 000 000 LONGITUDE INTERVAL OF NODAL CROSSING

CHR = 4. 000 000 DIFFERENCE BETWEEN LOCAL TIME AND GREENWICH TIME

Sample Output for the Nodal Crossing Prediction Program



# SATELLITE NO. 849 NODAL CROSSING PREDICTION PROGRAM - SPACE TRACK - LTN. 342 EDT

EPOCH TIME = 116.000 2 DAYS

LAMBDAZ1 = 134.2

LAMBDAZ2 = 191.900

PASS NO. 75 - 460

DELTA LAMBDA = 50.000

| DAY | HR. | MIN. | SEC. | LAMBDA | DAY | HR. | MIN. | SEC.   | LAMBDA | DAY | HR. | MIN. | SEC.  | LAMBDA |     |    |    |        |        |
|-----|-----|------|------|--------|-----|-----|------|--------|--------|-----|-----|------|-------|--------|-----|----|----|--------|--------|
| 124 | 2   | 29   | 54   | 166.35 | 128 | 6   | 42   | 177.51 | 132    | 22  | 38  | 54   | 87.95 | 137    | 2   | 7  | 35 | 158.57 |        |
| 124 | 4   | 22   | 34   | 134.86 | 128 | 7   | 53   | 21     | 206.2  | 133 | 3   | 31   | 32    | 116.45 | 137 | 4  | 0  | 12     | 187.07 |
| 124 | 6   | 15   | 14   | 153.38 | 128 | 9   | 45   | 60     | 234.53 | 133 | 2   | 24   | 9     | 144.96 | 137 | 5  | 52 | 48     | 215.57 |
| 124 | 8   | 7    | 54   | 191.89 | 129 | 0   | 47   | 9      | 102.61 | 133 | 4   | 16   | 47    | 173.46 | 137 | 22 | 46 | 15     | 112.06 |
| 124 | 10  | 0    | 34   | 22.41  | 129 | 2   | 39   | 43     | 131.11 | 133 | 6   | 9    | 24    | 201.97 | 138 | 0  | 38 | 51     | 140.56 |
| 125 | 1   | 1    | 52   | 55.52  | 129 | 4   | 32   | 27     | 159.62 | 133 | 8   | 2    | 2     | 230.47 | 138 | 2  | 31 | 27     | 169.06 |
| 125 | 2   | 54   | 32   | 117.03 | 129 | 6   | 25   | 5      | 186.13 | 133 | 23  | 3    | 1     | 98.50  | 138 | 4  | 24 | 3      | 197.56 |
| 125 | 4   | 47   | 11   | 145.55 | 129 | 8   | 17   | 44     | 216.64 | 134 | 0   | 55   | 35    | 127.00 | 138 | 6  | 16 | 40     | 226.06 |
| 125 | 6   | 39   | 51   | 174.06 | 129 | 25  | 13   | 51     | 84.71  | 134 | 2   | 48   | 15    | 155.51 | 138 | 21 | 17 | 28     | 24.04  |
| 125 | 8   | 32   | 31   | 22.57  | 13  | 1   | 11   | 30     | 113.21 | 134 | 4   | 40   | 53    | 184.01 | 138 | 23 | 10 | 4      | 192.54 |
| 125 | 10  | 25   | 1    | 231.09 | 13  | 3   | 4    | 8      | 141.72 | 134 | 6   | 33   | 30    | 212.51 | 139 | 1  | 2  | 40     | 151.04 |
| 126 | 1   | 26   | 25   | 39.19  | 13  | 4   | 50   | 47     | 170.23 | 134 | 8   | 26   | 7     | 241.02 | 139 | 2  | 55 | 16     | 179.54 |
| 126 | 3   | 19   | 6    | 127.7  | 13  | 6   | 42   | 25     | 198.74 | 134 | 23  | 27   | 4     | 109.04 | 139 | 4  | 47 | 52     | 218.03 |
| 126 | 5   | 11   | 45   | 156.22 | 13  | 8   | 42   | 3      | 227.24 | 135 | 1   | 19   | 41    | 137.54 | 139 | 6  | 40 | 28     | 236.53 |
| 126 | 7   | 4    | 25   | 194.73 | 13  | 23  | 43   | 9      | 95.3   | 135 | 3   | 12   | 16    | 166.04 | 139 | 21 | 41 | 14     | 14.51  |
| 126 | 8   | 57   | 4    | 213.24 | 131 | 1   | 35   | 47     | 123.61 | 135 | 5   | 4    | 55    | 194.55 | 139 | 23 | 33 | 49     | 173.00 |
| 126 | 10  | 49   | 43   | 241.75 | 131 | 3   | 23   | 25     | 152.72 | 135 | 6   | 57   | 32    | 223.05 | 140 | 1  | 26 | 25     | 161.50 |
| 127 | 1   | 50   | 57   | 1.955  | 131 | 5   | 21   | 3      | 180.82 | 135 | 21  | 58   | 26    | 91.06  | 140 | 3  | 19 | 0      | 190.00 |
| 127 | 3   | 43   | 46   | 133.36 | 131 | 7   | 13   | 41     | 209.33 | 135 | 23  | 51   | 3     | 119.56 | 140 | 5  | 11 | 36     | 218.49 |
| 127 | 5   | 36   | 15   | 156.87 | 131 | 9   | 6    | 19     | 237.84 | 136 | 1   | 43   | 40    | 146.06 | 140 | 20 | 12 | 20     | 56.46  |
| 127 | 7   | 28   | 45   | 193.38 | 132 | 0   | 7    | 22     | 105.49 | 136 | 3   | 36   | 17    | 176.56 | 140 | 22 | 4  | 56     | 114.96 |
| 127 | 9   | 21   | 34   | 223.89 | 132 | 1   | 52   | 60     | 131.39 | 136 | 5   | 28   | 53    | 205.06 | 140 | 23 | 57 | 31     | 143.45 |
| 128 | 0   | 22   | 40   | 91.98  | 132 | 3   | 52   | 34     | 162.9  | 136 | 7   | 21   | 30    | 233.57 | 141 | 1  | 50 | 6      | 171.95 |
| 128 | 2   | 15   | 14   | 12.49  | 132 | 5   | 43   | 15     | 191.4  | 136 | 22  | 22   | 22    | 101.57 | 141 | 3  | 42 | 42     | 200.44 |
| 128 | 4   | 8    | 3    | 147.1  | 132 | 7   | 37   | 53     | 217.01 | 137 | 0   | 14   | 59    | 130.07 | 141 | 5  | 35 | 17     | 208.94 |

NODAL CROSSING PREDICTION PROGRAM  
SATELLITE NO. 049 - SPACETRACK - 9LTN, 342 EDT

EPOCH TIME = 118.08912 DAYS  
LAMBDAZ1 = 134.230

LAMBDAZ2 = 191.900

PASS NO. 75 - 460  
DELTA LAMBDA = 50.000

| DAY HR. MIN. SEC. LAMBDA | DAY HR. MIN. SEC. LAMBDA | DAY HR. MIN. SEC. LAMBDA | DAY HR. MIN. SEC. LAMBDA | DAY HR. MIN. SEC. LAMBDA |
|--------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| 141 20 35 59 96.90       | 144 21 46 33 128.11      | 148 0 49 9 187.68        | 151 16 58 59 86.49       |                          |
| 141 22 28 34 125.39      | 144 23 39 8 156.60       | 148 2 41 42 216.17       | 151 18 51 31 114.97      |                          |
| 142 0 21 9 153.89        | 145 1 31 42 185.10       | 148 19 34 43 112.55      | 151 20 44 3 143.45       |                          |
| 142 2 13 44 192.38       | 145 3 24 16 213.59       | 148 21 27 16 141.04      | 151 22 36 36 171.94      |                          |
| 142 4 6 19 21.87         | 145 20 17 24 110.00      | 148 23 19 49 169.52      | 152 0 29 8 200.42        |                          |
| 142 5 58 54 239.37       | 145 22 9 58 138.49       | 149 1 12 22 198.01       | 152 2 21 41 228.90       |                          |
| 142 20 59 34 137.32      | 146 0 2 32 166.98        | 149 3 4 55 226.49        | 152 17 21 59 96.76       |                          |
| 142 22 52 9 135.81       | 146 1 55 6 195.47        | 149 18 5 20 94.38        | 152 19 14 31 125.24      |                          |
| 143 0 44 44 164.30       | 146 3 47 40 223.96       | 149 19 57 53 122.87      | 152 21 7 3 153.73        |                          |
| 143 2 37 18 192.80       | 146 18 48 11 91.87       | 149 21 50 26 151.35      | 152 22 59 35 182.21      |                          |
| 143 4 29 53 221.29       | 146 20 40 45 120.36      | 149 23 42 59 179.84      | 153 0 52 7 210.69        |                          |
| 143 19 30 31 99.23       | 146 22 33 18 148.85      | 150 1 35 32 208.32       | 153 2 44 40 239.17       |                          |
| 143 21 23 5 117.72       | 147 0 25 52 177.34       | 150 3 28 5 236.81        | 153 17 44 56 107.02      |                          |
| 143 23 15 40 146.22      | 147 2 18 26 205.83       | 150 16 28 27 104.68      | 153 19 37 28 135.50      |                          |
| 144 1 8 15 174.71        | 147 4 10 60 234.31       | 150 20 21 0 133.17       | 153 21 29 59 163.98      |                          |
| 144 3 0 49 233.20        | 147 19 11 29 102.22      | 150 22 13 33 161.65      | 153 21 29 59 163.98      |                          |
| 144 4 53 24 231.69       | 147 21 4 2 130.71        | 151 0 6 5 190.14         | 153 21 29 59 163.98      |                          |
| 144 19 53 59 99.62       | 147 22 56 35 159.10      | 151 1 58 38 218.62       | 153 21 29 59 163.98      |                          |

E. Orbit Prediction Program

1. Introduction

The Orbit Prediction Program simulates the trajectory of an earth-orbiting satellite and computes the radar look angles for the satellite. The satellite trajectory is generated from the SPACETRACK orbital elements and parameters obtained from the Nodal Crossing Prediction Program. A description of the Orbit Prediction Program is contained in the document: "Nodal Crossing Prediction Program", Technical Memorandum No. EMA-TM-66-9, March 1967, by John C. Cleary and Paul E. Brown, 1st Lt.

2. Computer Program Operating Environment

a. Computer

Honeywell 6180

b. Source Language

FORTRAN Y under GCOS.

c. Memory Requirement

32K words

d. Typical Processing Time Required

0.005 hours (18 seconds)

e. Peripheral Equipment Requirement

Two disc files (file codes: 01, 02)

f. Non-system Subroutines Required

OUT1

OUT2

OUT3

PARALX

NEWT

CLEAR  
OUT4

3. Inputs

The following set of input parameters is required for execution of the Orbit Prediction Program:

NAMelist IN1

HED - Array containing the heading for the output from a program run. The dimension of HED is 24.

NAMelist IN2

NRUN - Run number assigned to pass.

NPRLX - Used in original version of program, no longer valid. If not 0, a punched paper tape for parallex correction of a transportable station would be produced.

NDL - Number of passes to be computed. First the on time pass, then the one for  $\lambda + \Delta \lambda$ , then  $\lambda - \Delta \lambda$ ,  $\lambda + 2\Delta \lambda$  and finally  $\lambda - 2\Delta \lambda$ . Normally use 2.

NOPT - If = 0, Subroutine OUT3 is not called. If = any other number, Subroutine OUT3 is called to print out the satellite orbit look angles, range, azimuth, elevation, and also Subroutine OUT4 is called to place this look angle data on a file for later plotting.

NDCH - Program division check.

NAMelist IN3

DAY - Day of year, nodal crossing time.

THR - Hour of day, nodal crossing time.

TMIN - Minute of hour, nodal crossing time.

TSEC - Second of minute, nodal crossing time.

AMDA0 - Longitude of nodal crossing (deg.).

BGT0 - Epoch time of nodal crossing.

DAMDA -  $\Delta \lambda$  (-.5 degrees is 2 min. early pass, which is normally the second pass).

DT - The interval in seconds between computations.

CHR - If converting GMT to EDT, = 4.0.  
If converting GMT to EST, = 5.0.



#### NAMELIST IN4

W0 - Argument of perigee (degrees).  
E0 - Orbit eccentricity.  
ANCL - Orbit inclination (degrees).  
ASMTH - A, mean motion in revolutions/day.  
RA1 - Rate of change of right ascending node (degrees/day).  
W1 - Rate of change of argument of perigee (degrees/day).  
E1 - Rate of change of eccentricity, per day.  
A0 - Semi-major axis of orbit in earth radii.  
A1 - Rate of change of A0 in earth radii/day.

#### NAMELIST IN5

XLAT - Latitude of radar (degrees).  
XLONG - Longitude of radar (degrees).  
AD - Radius of earth at radar in Km.  
AZTH - Maximum allowed azimuth deviation of beam center from satellite position (degrees).  
ALTH - Maximum allowed elevation deviation of beam center from satellite position (degrees).  
ALO - Initial elevation angle of the pass (degrees).  
XLAT1 - Latitude of transportable station (degrees).  
XLONG1 - Longitude of transportable station (degrees).  
TDELAY - Transmitter time delay, used to compute the range mark number. This is a number that describes the setting of 5 switches at the transmitter to get a properly timed range mark for starting the pass.

The following page (Fig. III-3) represents the format for the six card element set from SPACETRACK. The orbital element parameters used in this program (NAMELIST IN4) are obtained from this card set. The orbital parameters needed in the program can also be obtained from the two card element set and hand calculation of required parameters missing from the set. Fig. III-4 illustrates this latest format for the SPACETRACK orbital elements. A punched card deck, containing the two card element set, as received by RADC from the Space Defense Center in Colorado is illustrated in Fig. III-5. The first card of the actual deck is the bottom card in the figure.







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#### 4. Output

There are a number of different output quantities produced during a typical run of the Orbit Prediction Program. By means of Subroutine OUT1 the input heading for the run (variable name HED), the run and pass numbers (NRUN and M), the satellite rise time in hours, minutes, and seconds (MHR, IMIN, and ISEC), the nodal crossing longitude (AMBA), and the epoch time in days (BGT0) are printed out. This is followed by a listing of various radar parameters versus times of visibility of the satellite to the radar. The radar parameters listed are the elevation count period (ECP), azimuth count period (ACP), elevation angle in degrees and minutes (variable names MELD and MELM), azimuth angle in degrees and minutes (MAZD and MAZM), range in kilometers (R) and return time in milliseconds (RM), and Doppler in kilocycles (DOPLER). For further explanation of the count periods and Doppler refer to the last paragraph of this section.

Subroutine OUT2 produces printout of the input data and parameters associated with the recorder, director, and tracker. The printout from OUT2 occurs on a separate page following the printout from OUT1.

If Subroutine OUT3 is invoked, then additional output of the radar look angles, range, azimuth, and elevation, will be generated for various times of observation of the satellite by the radar. These observation times are separated by the input DT. First the input heading for the run is printed out (variable name HED). Then follows the run and pass number (NRUN and M), nodal crossing time in day of year, hour of day, minute of hour, and second of minute (DAY, THR, TMIN, and TSEC), the nodal crossing longitude (AMBA), and the satellite rise time in hours, minutes, and seconds (MHR, IMIN, and ISEC). After this follows a list of radar parameters versus satellite observation times, separated by intervals of DT. The radar parameters are azimuth in degrees and radians (AZ and AZR), elevation in degrees and radians (ALPH and ELR), and range in kilometers (R).

When NOPT is not equal to 0, Subroutine OUT4 is called. OUT4 will place the radar data printed out by OUT3 on a data file (file code 02) for use in producing off-line plots of range, azimuth, and elevation.

The outputs elevation count period and azimuth count period are the count periods to be set into the programmed antenna tracker elevation and azimuth clocks. These data are used to prepare a magnetic tape that controls an antenna programmed tracker. This tape has pulses recorded at the proper rates to control stepping motors which in turn, position synchros to command pointing angles. The data shown in the output are actually proportional to the required periods between pulses to be recorded on the program tape. The numbers shown are the settings to be entered into present counters to produce pulses at the required spacing for use in preparing the program tape. An additional column shows the requisite Doppler frequency corrections required due to the translational motion of the satellite. These Doppler frequencies are used to cut a Doppler compensator cam for a satellite pass.

```

0010$:IDENT:CLEARY,CONT1 ,65121104RADC
0020$:USERID:CLEARY$THREE .
0030$:LOWLOAD
0040$:OPTION:FORTAN
0050$:SELECT:CLEARY/00R3
0060$:SELECT:CLEARY/0CLEAR
0065$:SELECT:CLEARY/0OUT4
0070$:EXECUTE
0080$:LIMITS:10,32K,-5K,12000
0085$:PRMFL:02,R/W,L,CLEARY/STORE1
0086$:DISC:01,AIR,5L
0090$:DATA:05
0100 $INI
0110 HED(5)=30H ORBIT PREDICTION PROGRAM ,
0120 HED(13)=54H 1 MIN EARLY OBJECT NO. 2103 BLTN NO. 7 4/1/66 $
0130 $IN2
0140 NRUN=302,
0150 NPRLX=0,
0160 NDL=1,
0170 NOPT=10,
0180 NDCH=-10 $
0190 $IN3
0200 DAY=91.0,
0210 THR=3.0,
0220 TMIN=32.0,
0230 TSEC=57.0,
0240 AMDA0=96.100,
0250 BGT0=36.0134,
0260 DAMDA=0.0,
0270 DT=5.0,
0280 CHR=4.0 $
0290 $IN4
0300 W0=53.070,
0310 E0=0.021690,
0320 ANCL=72.090,
0330 RA1=-2.52163,
0340 W1=-2.16126,
0350 ASMTH=15.67614,
0360 E1=-2.4600E-04,
0370 A0=1.05752,
0380 A1=-2.6600E-04 $
0390 $IN5
0400 XLAT=43.15250,
0410 XLONG=75.61722,
0420 AD=6365.30,
0430 AZTH=0.100,
0440 ALTH=0.100,
0450 XLAT1=0.0,
0460 XLONG=0.0,
0470 TDELAY=25.0 $
0480$:ENDJOB
0490***EOF

```

Sample Job Stream for the Orbit Prediction Program

| RADC 635/645 BATCH JOB   |       |  |              |       |
|--|-------|--|--------------|-------|
| SNUM# NUMBER   |       | DATE   | TIME         |       |
|  |       | 3/30/76  | 910          |       |
| PROGRAMMER   |       | TELEPHONE  |              |       |
| CONTI  |       | 339-1360   |              |       |
| RADC ENGINEER  |       | TELEPHONE  | SYMBOL       |       |
| CLEARY   |       | 3573   | OCSA         |       |
| TAPES ASSIGNED   |       |  |              |       |
| REEL NO  | WRITE | READ   | DEN          | TITLE |
|  |       |  |              |       |
|  |       |  |              |       |
|  |       |  |              |       |
|  |       |  |              |       |
|  |       |  |              |       |
|  |       |  |              |       |
|  |       |  |              |       |
|  |       |  |              |       |
|  |       |  |              |       |
| PERIPHERALS ASSIGNED <input checked="" type="checkbox"/> READER <input checked="" type="checkbox"/> PRINTER <input type="checkbox"/> PUNCH<br><input checked="" type="checkbox"/> DISC # OF LINKS 10 <input type="checkbox"/> DRUM # OF LINKS<br>CORE SIZE 32K ACTIVITIES 1<br>PROCESSOR TIME .01 ESTIMATED LINES OF PRINT 500<br>TOTAL RUN TIME .02 |       |  |              |       |
| DECKS EXPECTED   |       |  |              |       |
| NO. OF BINARY DECKS  |       | NO. OF COMDECKS  |              |       |
| None   |       |  |              |       |
| BMC  |       | TAPE <input type="checkbox"/> DUMP <input type="checkbox"/> COPY |              |       |
| FROM:  | TO:   | MODE   | NO. OF FILES |       |
|  |       | <input type="checkbox"/> BCD                                     |              |       |
|  |       | <input type="checkbox"/> BINARY                                  |              |       |
| SPECIAL OPERATOR INSTRUCTIONS  |       |  |              |       |
|  |       |  |              |       |
|  |       |  |              |       |
|  |       |  |              |       |
|  |       |  |              |       |
|  |       |  |              |       |
| (Use reverse side if required)   |       |  |              |       |

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Source Listing of the Orbit Prediction Program

|    |  |          |
|----|--|----------|
| C  | ORBIT PREDICTION - MAIN PROGRAM                                      | 00001000 |
|    | DIMENSION TM(1500),AZ(1500),ALPH (1500),R(1500),PHI(1500),           | 00001010 |
| 1  | THETA(1500),RHO(1500),D(1500),ECP(750),ACP(750),                     | 00001020 |
| 2  | HED(24),XLAM(5)  | 00001030 |
|    | COMMON TM,AZ,ALPH,R,PHI,THETA,RHO,D,ECP,ACP,ICP,HED,XLAM,TO,DT,      | 00001040 |
| 1  | CTO,AMDA,AMDA1,DAMDA,W0,W1,E0,E1,ANCL,A,P,XLAT,XLONG,AD,             | 00001050 |
| 2  | SANCL,CANCL,SLAT,CLAT,RLONG,L,M,J,T,W,AMDA,AMBA,E,V,PHIG,            | 00001060 |
| 3  | CTH,TH,DELL,SD,CD;CDL,SDL,COSB,SINE,TANALF,RSQ,COSAZ,TAZ,            | 00001070 |
| 4  | NN,N1,N2,XW,XL,XE,TRAMDA,RQ,CP0,PHI0,SP0,STH,X,SINAZ,RW1,            | 00001080 |
| 5  | SPHI,CON,AZTH,ALTH,ALO,1,IALS,JJ,KK,NO2,OPT,DELN,GAMN,               | 00001090 |
| 6  | MMIN,MSEC,DPLR,DEN,DFN,TT,MHR,HR,IMIN,YMIN,ISEC,TMIN,J1              | 00001100 |
|    | COMMON NRUN,NRRLX,NDL,NOPT,NDCH,DAY,THR,TSEC,AZMTH,CHR,PI,RA1,       | 00001110 |
| 1  | RAD,NA,NB,NC,ND,NE,RRATE,BGTO,A0,A1,XLAT1,XLONG1,TDELAY,             | 00001120 |
| 2  | DOPLER,V,INDX,TMTP,NERL,CTIME,ASMTW,RLONG1,SLAT1,CLAT1               | 00001130 |
|    | NAMLIST/IN1/HED  | 00001140 |
|    | NAMLIST/IN2/NRUN,NRRLX,NDL,NOPT,NDCH                                 | 00001150 |
|    | NAMLIST/IN3/DAY,THR,TMIN,TSEC,AMDA0,BGTO,DAMDA,DT,CHR                | 00001160 |
|    | NAMLIST/IN4/W0,E0,ANCL,ASMTW,RA1,W1,E1,A0,A1                         | 00001170 |
|    | NAMLIST/IN5/XLAT,XLONG,AD,AZTH,ALTH,ALO,XLAT1,XONG1,                 | 00001180 |
|    | *TDELAY  | 00001190 |
|    | LOGICAL SL1  | 00001200 |
|    | DATA EST,EDT/44 EST,4H EDT/,XRLY,XLTE/5HEARLY,4HLATE/                | 00001210 |
|    | DATA BLANK/6H /  | 00001220 |
| 1  | CALL CLEAR(TM,INDX)  | 00001230 |
|    | DO 99 II=1,24  | 00001240 |
|    | HED(II)=BLANK  | 00001250 |
| 99 | CONTINUE   | 00001260 |
|    | PI = 3.1415926536  | 00001270 |
|    | QAD = .0174532925  | 00001280 |
|    | SL1 = .FALSE.  | 00001290 |
|    | AB = 6378.174  | 00001300 |
| 2  | READ(05,IN1,END=999)   | 00001310 |
|    |  | 00001320 |
| C  | BRAD(05,IN2)   | 00001330 |
| C  |  | 00001340 |
| C  |  | 00001350 |
| C  | NAMLIST - IN2  | 00001360 |
| C  |  | 00001370 |
| C  | NRUN = RUN NUMBER ASSIGNED TO PASS                                   | 00001380 |
| C  | NRRLX = IF NOT 0, PUNCHED PAPER TAPE FOR PARALLEX                    | 00001390 |
| C  | CORRECTION OF TRANSPORTABLE STATION WILL BE COMPUTED                 | 00001400 |
| C  | NDL = NUMBER OF PASSES TO BE COMPUTED, FIRST TIME ON TIME            | 00001410 |
| C  | PASS, THEN ONE FOR LAMDA+ DELTALAMDA, THEN LAMDA- DELTALAMDA, 001420 |          |
| C  | LAMDA+2DELTALAMDA, THEN LAMDA- 2DELTALAMDA. NORMALLY USE 2           | 00001430 |
| C  | NOPT = 0, SUBROUTINE OUT 3 IS NOT CALLED.                            | 00001440 |
| C  | NOPT = ANY OTHER NUMBER, SUBROUTINE OUT3 IS CALLED                   | 00001450 |
| C  | ALSO SUBROUTINE OUT4 IS CALLED FOR PLOTTING                          | 00001455 |
| C  |  | 00001460 |
| C  | READ(05,IN3)   | 00001470 |
| C  |  | 00001480 |
| C  |  | 00001490 |
| C  | NAMLIST - IN3  | 00001500 |

|   |   |                     |          |
|---|---|---------------------|----------|
| G |   |                     | 00001510 |
| C | DAY = DAY OF YEAR   | NODAL CROSSING TIME | 00001520 |
| C | YHR = HOUR OF DAY   | NODAL CROSSING TIME | 00001530 |
| C | TMIN = MIN. OF HOUR   | NODAL CROSSING TIME | 00001540 |
| C | TSEC = SEC. OF MIN.   | NODAL CROSSING TIME | 00001550 |
| C | AMDAO = LONGITUDE OF NODAL CROSSING                         |                     | 00001560 |
| C | BGTO = EPOCH TIME OF NODAL CROSSING                         |                     | 00001570 |
| C | DAMDA = DELTA LAMDA (-.5DEGREES IS 2 MIN? EARLY PASS,       |                     | 00001580 |
| C | WHICH IS NORMALLY THE SECOND PASS                           |                     | 00001590 |
| C | DY = 30.0, THE INTERVAL IN SECONDS BETWEEN COMPUTATIONS     |                     | 00001600 |
| C | CMR = 4.0 IF CONVERTING GMT TO EDT                          |                     | 00001610 |
| C | CMR = 5.0 IF CONVERTING GMT TO EST                          |                     | 00001620 |
| C |   |                     | 00001630 |
| C | READ(05,IN4)  |                     | 00001640 |
| C |   |                     | 00001650 |
| C |   |                     | 00001660 |
| C | NAMELIST - IN4  |                     | 00001670 |
| C |   |                     | 00001680 |
| C | W0 = ARGUMENT OF PERIGEE, DEGREES                           |                     | 00001690 |
| C | EO = ORBIT ECCENTRICITY                                     |                     | 00001700 |
| C | ANCL = ORBIT INCLINATION, DEGREES                           |                     | 00001710 |
| C | ASMTN = A, MEAN MOTION, REVOLUTIONS/DAY                     |                     | 00001720 |
| C | BA1 = RATE OF CHANGE OF RIGHT ASCENDING NODE, DEGREES/DAY   |                     | 00001730 |
| C | W1 = RATE OF CHANGE OF ARGUMENT OF PERIGEE IN DEGREES / DAY |                     | 00001740 |
| C | E1 = RATE OF CHANGE OF ECCENTRICITY, PER DAY                |                     | 00001750 |
| C | A0 = SEMIMAJOR AXIS OF ORBIT IN EARTH RADII                 |                     | 00001760 |
| C | A1 = RATE OF CHANGE OF A0 IN EARTH RADII/DAY                |                     | 00001770 |
| C |   |                     | 00001780 |
| C | READ(05,IN5)  |                     | 00001790 |
| C |   |                     | 00001800 |
| C |   |                     | 00001810 |
| C | NAMELIST - IN5  |                     | 00001820 |
| C |   |                     | 00001830 |
| C | RLAT = LATITUDE OF RADAR                                    |                     | 00001840 |
| C | RLONG = LONGITUDE OF RADAR                                  |                     | 00001850 |
| C | RD = EARTH'S RADIUS AT RADAR IN KM                          |                     | 00001860 |
| C | AZTH = MAXIMUM ALLOWED AZIMUTH DEVIATION OF BEAM            |                     | 00001870 |
| C | CENTER FROM SATELLITE POSITION                              |                     | 00001880 |
| C | EUTH = MAXIMUM ALLOWED ELEVATION DEVIATION OF BEAM          |                     | 00001890 |
| C | CENTER FROM SATELLITE POSITION                              |                     | 00001900 |
| C | ALO = INITIAL ELEVATION ANGLE OF THE PASS                   |                     | 00001910 |
| C | RLAT1 = TRANSPORTABLE STATION LOCATION, LATITUDE            |                     | 00001920 |
| C | RLONG1 = TRANSPORTABLE STATION LOCATION, LONGITUDE          |                     | 00001930 |
| C | TDELAY = TRANSMITTER TIME DELAY, USED TO COMPUTE THE RANGE  |                     | 00001940 |
| C | MARK NUMBER( A NUMBER THAT DESCRIBES THE SETTING OF         |                     | 00001950 |
| C | 5 SWITCHES AT TRANSMITTER TO GET A PROPERLY TIMED           |                     | 00001960 |
| C | RANGE MARK FOR STARTING THE PASS).                          |                     | 00001970 |
| C | TMTF = EST  |                     | 00001980 |
| C | IF (CHR.EQ.4.) TMTF = EDT                                   |                     | 00001990 |
| C | NDL = MINO(NDL,5)   |                     | 00002000 |
| C | TO = 3600.0*THR+60.0*TMIN+TSEC                              |                     | 00002010 |
| C | DT0 = DAY+(THR*CHR)/24.0+TMIN/1440.0+TSEC/86400.0-BGTO      |                     | 00002020 |

|     |   |          |
|-----|---|----------|
|     | AMDA1 = 360.983-RA1                         | 00002030 |
| G   | 86400 = SECONDS IN A DAY                    | 00002040 |
|     | P = 86400.0/AS4TH                           | 00002050 |
| 3   | 8ANCL = SIN (ANCL*RAD)                      | 00002060 |
|     | 8ANCL = COS (ANCL*RAD)                      | 00002070 |
|     | 8LAT = SIN (XLAT*RAD)                       | 00002080 |
|     | 8LAT = COS (XLAT*RAD)                       | 00002090 |
| 4   | 8LONG = XLONG*RAD                           | 00002100 |
|     | 8LAT1 = SIN(XLAT1*RAD)                      | 00002110 |
|     | 8LAT1 = COS(XLAT1*RAD)                      | 00002120 |
|     | 8LONG1 = XLONG1*RAD                         | 00002130 |
|     | DAMDA = AMDA1*RAD/86400.0                   | 00002140 |
|     | 8W1 = W1*RAD/86400.0                        | 00002150 |
|     | L = 1                                       | 00002160 |
|     | M = 1                                       | 00002170 |
| 5   | T = T0                                      | 00002180 |
|     | E = E0+CT0*E1                               | 00002190 |
|     | AMDA = AMDA0                                | 00002200 |
|     | W = W0+W1*CT0+720.0                         | 00002210 |
|     | A = AB*(A0+CT0*A1)                          | 00002220 |
|     | W = AMOD(W,360.0)                           | 00002230 |
|     | 8W = W*RAD                                  | 00002240 |
|     | CP0 = (E+COS (RW))/(1.0+E+COS (RW))         | 00002250 |
|     | BP0 = SIGN (SQRT (1.0-CP0**2), SIN (RW))    | 00002260 |
|     | IF (CP0) 501,500,502                        | 00002270 |
| 500 | PMI0 = SP0*PI/2.0-PI                        | 00002280 |
|     | GO TO 503                                   | 00002290 |
| 501 | PMI0 = -PI+ATAN (SP0/CP0)                   | 00002300 |
|     | GO TO 503                                   | 00002310 |
| 502 | PMI0 = -AMOD(ATAN (SP0/CP0)+2.0*PI,2.0*PI)  | 00002320 |
| 503 | CON = E*SP0+PMI0                            | 00002330 |
| 6   | KLAM(1) = AMDA*RAD                          | 00002340 |
|     | KLAM(2) = (AMDA+DAMDA)*RAD                  | 00002350 |
|     | KLAM(3) = (AMDA-DAMDA)*RAD                  | 00002360 |
|     | KLAM(4) = (AMDA+2.0*DAMDA)*RAD              | 00002370 |
|     | KLAM(5) = (AMDA-2.0*DAMDA)*RAD              | 00002380 |
| 7   | YM(L) = T                                   | 00002390 |
|     | V = 2.0*PI*(T-T0)/P+CON                     | 00002400 |
|     | IF (V.NE.0.0) GO TO 9                       | 00002410 |
| 8   | PHI(L) = 0.0                                | 00002420 |
|     | GO TO 10                                    | 00002430 |
| 9   | PMIG = V/(1.0-E)                            | 00002440 |
|     | CALL NEWT(PHIG,PHI(L),E,V)                  | 00002450 |
| 10  | 8PHI = SIN (PHI(L))                         | 00002460 |
|     | CTH = (COS (PHI(L))-E)/(1.0+E+COS (PHI(L))) | 00002470 |
|     | 8TH = SIGN ((SQRT (1.0-CTH**2)),SPH1)       | 00002480 |
|     | IF (CTH) 12,11,12                           | 00002490 |
| 11  | YM = PI-STH*PI/2.0                          | 00002500 |
|     | GO TO 17                                    | 00002510 |
| 12  | YM = ATAN (STH/CTH)                         | 00002520 |
|     | IF (TH) 13,13,16                            | 00002530 |
| 13  | YM = PI*(1.0-CTH) / 2.0                     | 00002540 |



|   |          |
|---|----------|
| IF (TH-THETA(L-1)) 14,17,17                           | 00002550 |
| 14 YH = 2.0*PI  | 00002560 |
| GO TO 17  | 00002570 |
| 15 YH = TH + 3.5*PI*SIGN ((PI/2.0),CTH)               | 00002580 |
| GO TO 17  | 00002590 |
| 16 YH = TH+PI/2.0-SIGN ((PI/2.0),CTH)                 | 00002600 |
| 17 YHETA(L) = YH                                      | 00002610 |
| RHO(L) = A*(1.0-E*COB (PHI(L)))                       | 00002620 |
| DEL = RW*RW1*(T-T0)*THETA(L)                          | 00002630 |
| 18 DELL = XLAM(M)*RLONG*RAMDA*(TH(L)-T0)              | 00002640 |
| BD = COS (D(L))                                       | 00002650 |
| BD = SIN (D(L))                                       | 00002660 |
| BDL = COS (DELL)                                      | 00002670 |
| BDL = SIN (DELL)                                      | 00002680 |
| UB = 0  | 00002690 |
| IF (CD) 181,180,181                                   | 00002700 |
| 180 R = SIGN (PI/2.0,CANCL*SD)                        | 00002710 |
| GO TO 182   | 00002720 |
| 181 R = ATAN (CANCL*SD/CD)                            | 00002730 |
| 182 IF (X*CANCL) 183,19,19                            | 00002740 |
| 183 R = X-SIGN (PI,X)                                 | 00002750 |
| 19 COSE = SANCL*SLAT*SD+CLAT*CDL*CD+CANCL*CLAT*BDL*SD | 00002760 |
| SINE = SORT (1.0-COSE**2)                             | 00002770 |
| IF (SINE,NE,0.0) GO TO 20                             | 00002780 |
| TANALF = 10.0E+30                                     | 00002790 |
| GO TO 21  | 00002800 |
| 20 TANALF = (COSE-AD/RHO(L))/SINE                     | 00002810 |
| 21 IF (TANALF) 22,25,25                               | 00002820 |
| 22 IF (SL1) GO TO 35                                  | 00002830 |
| 23 IF (M-1) 24,24,26                                  | 00002840 |
| 24 T = T+DT   | 00002850 |
| GO TO 7   | 00002860 |
| 25 SL1 = .TRUE.                                       | 00002870 |
| 26 RSQ = AD**2+RHO(L)**2-2.0*AD*RHO(L)*COSE           | 00002880 |
| IF (SINE) 28,27,28                                    | 00002890 |
| 27 COSAZ = 1.0  | 00002900 |
| GO TO 29  | 00002910 |
| 28 COSAZ = (SANCL*SD-SLAT*COSE)/(CLAT*SINE)           | 00002920 |
| 29 SINAZ = SIGN (SORT (1.0-COSAZ**2),(X*DELL))        | 00002930 |
| IF (COSAZ) 31,30,31                                   | 00002940 |
| 30 TAZ = SINAZ*PI/2.0                                 | 00002950 |
| GO TO 322   | 00002960 |
| 31 TAZ = ATAN (SINAZ/COSAZ)                           | 00002970 |
| IF (TAZ) 320,32,321                                   | 00002980 |
| 32 TAZ = PI*(1.0-COSAZ)/2.0                           | 00002990 |
| GO TO 322   | 00003000 |
| 320 TAZ = TAZ+1.5*PI*SIGN ((PI/2.0),COSAZ)            | 00003010 |
| GO TO 322   | 00003020 |
| 321 TAZ = TAZ+PI/2.0-SIGN ((PI/2.0),COSAZ)            | 00003030 |
| 322 AZ(L) = TAZ/RAD                                   | 00003040 |
| ALPH(L) = ATAN (TANALF)/RAD                           | 00003050 |
| R(L) = SORT (RSQ)                                     | 00003060 |

|     |                                   |          |
|-----|-----------------------------------|----------|
| 83  | L = L+1                           | 00003070 |
|     | IF (M.LE.1) GO TO 34              | 00003080 |
|     | IF (TM(L).EQ.TM(L-1)+DT) GO TO 18 | 00003090 |
| 34  | T = T+DT                          | 00003100 |
|     | GO TO 7                           | 00003110 |
| 89  | BL1 = .FALSE.                     | 00003120 |
|     | AMBA = XLAM(M)/RAD                | 00003130 |
|     | EARLY = (AMBA-AMDA0)*4.0          | 00003140 |
|     | NERLY = EARLY+SIGN(.5,EARLY)      | 00003150 |
|     | NERL = IABS(NERLY)                | 00003160 |
|     | CTIME = XRLY                      | 00003170 |
|     | IF (NERLY.GT.0) CTIME = XLTE      | 00003180 |
|     | CALL OUT1                         | 00003190 |
|     | CALL OUT2                         | 00003200 |
|     | IF (NOPT.NE.0) CALL OUT3          | 00003210 |
|     | IF (NOPT.NE.0) CALL OUT4          | 00003215 |
|     | IF (NPRX.NE.0) CALL PARALX        | 00003220 |
|     | IF (M.GE.NDL) GO TO 1             | 00003230 |
|     | M = M+1                           | 00003240 |
|     | L = 1                             | 00003250 |
|     | GO TO 18                          | 00003260 |
| 999 | CONTINUE                          | 00003270 |
|     | STOP                              | 00003280 |
|     | END                               | 00003290 |

ROUT1 ORBIT PREDICTION PROGRAM-SUBROUTINE OUT1

```

SUBROUTINE OUT1
DIMENSION TM(1500),AZ(1500),ALPH(1500),R(1500),PHI(1500),
1 THETA(1500),RHO(1500),D(1500),ECP(750),ACP(750),
2 HED(24),XLAM(5),ICP(750)
COMMON TM,AZ,ALPH,R,PHI,THETA,RHO,D,ECP,ACP,XXX,HED,XLAM,TO,DT,
1 CT,AMDA,AMDA1,DAMDA,WO,W1,E0,E1,ANCL,A,P,XLAT,XLONG,AD,
2 SANCL,CANCL,SLAT,CLAT,RLONG,L,M,J,T,W,AMDA,AMBA,E,V,PHIG,
3 CTH,TH,DELL,SD,CD,CDL,SDL,COSB,SINE,TANALF,RSQ,COSAZ,TAZ,
4 NN,N1,N2,XW,XL,XE,RAMDA,EW,CPO,PHIO,SPO,STH,X,SINAZ,RW1,
5 SPHI,CN,AZTH,ALTH,AL,I,IALS,JJ,KK,NO2,OPT,DELN,GAMN,
6 MMIN,MSEC,DPLR,DEN,DFW,TT,MHR,HR,IMIN,YMIN,ISEC,TMIN,J1
COMMON NRUN,NPRLX,NDL,NOPT,NDCH,DAY,THR,TSEC,AZMTF,CHR,PI,RA1,
1 RA,NA,NB,NC,ND,NE,RRATE,BGTO,A0,A1,XLAT1,XLONG1,TDELAY,
2 DOPLER,N,INDX,TMTP,NPRL,CTIME,ASMT,RLONG1,SLAT1,CLAT1
1 NN = L-1
DO 2 I=1,NN
IF (ALPH(I).LT.AL) GO TO 2
IALS = I
GO TO 3
2 CONTINUE
WRITE(6,1000) (HEI(I),I=1,24),NRUN,M,TMTP,AMBA,BGTO,NPRL,CTIME
1000 FORMAT(1H1,29X12A6/3 X12A6 / 2X7HRUN NO.16,1H-11,2X11HRISE TIME -
1 3X5H HRS.3X5H MIN.3X6H SEC. A4,2X8H LAMBDA =F8.3,5H DEG.
2 2X12H EPOCH TIME =F8.3,5H DAYS ,2X13,6H MIN. A6,4H PASS //
3 5 X32HORBIT NOT HIGH ENOUGH TO BE SEEN)
NOPT = 1
RETURN
3 DOPLER = '9*(R(IALS-1)-R(IALS+1))/(TM(IALS+1)-TM(IALS-1))
RRATE = .35*DOPLER
N = R(IALS)/.15+TDELAY
NA = N/10
IB = N-1 *NA
NB = (IB+1)/20 +1
IC = IB-NB*2 0+3 0
IF (NB.GE.4) GO TO 4
NB = IB/2
IC = IB-NB*2 0
4 NC = IC/25
IC = IC-25*NC
ND = IC/32
IC = IC-32*ND
NE = IC/4
5 JJ = 1
KK = IALS+2
DO 7 I=KK,NN,2
NO2 = (I+KK)/2-1
DELN = ALPH(NO2)-(ALPH(I)+ALPH(KK-2))/2.0
IF (ABS(DELN).GT.ALTH) GO TO 8
GAMN = AZ(NO2)-(AZ(I)+AZ(KK-2))/2.0
IF (ABS(GAMN).GE.150.0) GAMN = GAMN-SIGN(180.0,GAMN)

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*      IF (ABS(GAMN).GT.AZTH/COS(RAD*ALPH(NO2))) GO TO 8      00003810
*      7 CONTINUE      00003820
*      JJ = JJ-1      00003830
*      GO TO 9      00003840
*      8 ICP(JJ) = I      00003850
*      DEN = 3.0*(ALPH(I)-ALPH(KK-2))      00003860
*      ECP(JJ) = 1000.0*DT*FLOAT(I-KK+2)/DEN      00003870
*      DFN = 3.0*(AZ(I)-AZ(KK-2))      00003880
*      IF (ABS(DFN).GE.9. ) DFN = DFN-SIGN(1080.0,DFN)      00003890
*      ACP(JJ) = 1000.0*DT*FLOAT(I-KK+2)/DFN      00003900
*      JJ = JJ+1      00003910
*      KK = I+2      00003920
*      GO TO 6      00003930
*      9 LLL = 0      00003940
*      TT = TM(IALS)      00003950
*      MHR = TT/360.0      00003960
*      HR = MHR      00003970
*      IMIN = ABS(TT-360.0*HR)/60.0      00003980
*      IMIN = IMIN      00003990
*      ISEC = ABS(TT-360.0*HR-60.0*YMIN)      00004000
*      MMIN = 0      00004010
*      NSEC = 0      00004020
*      INDX = IALS      00004030
*      MELD = ALPH(INDX)      00004040
*      MELM = (ALPH(INDX)-FLOAT(MELD))*60.0+.5      00004050
*      IF(MELM.LT.6.0)GO TO 90      00004060
*      MELD = MELD+1      00004070
*      MELM = MELM-6      00004080
*      90 MAZD = ABS(AZ(INDX))      00004090
*      MAZM = (ABS(AZ(INDX))-FLOAT(MAZD))*60.0+.5      00004100
*      IF(MAZM.LT.6.0)GO TO 91      00004110
*      MAZD = MAZD+1      00004120
*      MAZM = MAZM-6      00004130
*      91 MAZD = ISIGN(MAZD,AZ(INDX))      00004140
*      RM = R(INDX)/5.      00004150
*      10 IF(MOD(LLL,27).NE.0)GO TO 11      00004160
*      WRITE(6,1001)(HED(I),I=1,24),NRUN,N,MHR,IMIN,ISEC,TMTP,AMBA,BGTC,      00004170
*      1      NERL,CTIME      00004180
*      1001 FORMAT(1H1,2G12,6/3 X12A6 / 2X7NRUN NO.I6,1H-I1, 2X11RISE TIME -0000419
*      1      I3,5H HRS.I3,5H MIN.I3,5H SEC. A4, 2X8HLAMEDA =F8,3,5H DEG.0000420
*      2      2X12EPOCH TIME =F8,3,5H DAYS, 2X13,6H MIN. A6,4HPASS//      0000421
*      3      7X4HTIME,1 X9HELEVATION,10X7HAZIMUTH,9X9HEL. ANGLE,7X      0000422
*      4      9HAZ. ANGLE, 9X5HRANGE,15X7HDOPPLER 7X4HTIME/5X9HMIN. SEC.0000423
*      5      7X1HCNTG. PER.1,8X1HCNTG. PER.,7X9HDEG. MIN,7X9HDEG. MIN.0000424
*      6      6X3HKM,6X3HMS.,13X4HK.C.,7X9HMIN. SEC. )      0000425
*      IF (LLL.EQ.0)WRITE(6,1002)IMMIN,MSEC,MELD,MELM,MAZD,MAZM,R(INDX),      0000426
*      1      RM,DOPLER      0000427
*      1002 FORMAT(I8,I4,I47,I5,I12,I4,F13.3,F9.3,F16.3)      0000428
*      11 LLL = LLL+1      0000429
*      INDX1 = INDX      0000430
*      INDX = ICP(LLL)      0000431
*      DOPLER = '9. *(R(INDX1)-R(INDX))/(TM(INDX)-TM(INDX1))      0000432

```



|    |   |         |
|----|---|---------|
| 12 | MELD = ALPH(INDX)   | 0000433 |
| 13 | MELM = (ALPH(INDX)-FLOAT(MELD))*60.0+.5                             | 0000434 |
| 14 | MAZD = ABS(AZ(INDX))  | 0000435 |
| 15 | MAZM = (ABS(AZ(INDX))-FLOAT(MAZD))*60.0+.5                          | 0000435 |
| 16 | MAZD = ISIGN(MAZD,AZ(INDX))   | 0000437 |
| 17 | RM = R(INDX)/.50  | 0000438 |
| 18 | TT = TM(INDX)-TM(IALS)  | 0000439 |
| 19 | MMIN1 = TT/60.0   | 0000440 |
| 20 | ZMIN = MMIN1  | 0000441 |
| 21 | MSEC1 = ABS(TT-60.0*ZMIN)   | 0000442 |
| 22 | MTMP = (60*(MMIN1+MMIN)+MSEC1+MSEC)/2                               | 0000443 |
| 23 | MSEC2 = MOD(MTMP,60)  | 0000444 |
| 24 | MMIN2 = (MTMP-MSEC2)/60   | 0000445 |
| 25 | MMIN = MMIN1  | 0000446 |
| 26 | MSEC = MSEC1  | 0000447 |
| 27 | WRITE(6,1) ECP(LLL),ACP(LLL),DOPLER,MMIN2,MSEC2,MMIN,MSEC,MELD,     | 0000448 |
| 28 | 1 MELM,MAZD,MAZM,R(INDX),RM   | 0000449 |
| 29 | 1003 FORMAT(F29. ,F18. ,F71.3,I8,I4/I8,I4,I47,I5,I12,I4,F13,3,F9.3) | 000045  |
| 30 | IF (LLL.LT.JJ) GO TO 10   | 0000451 |
| 31 | RETURN  | 0000452 |
| 32 | END   | 0000453 |

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COUT2  ORBIT PREDICTION PROGRAM-SUBROUTINE OUT2 00004540
C 00004545
SUBROUTINE OUT2 00004550
DIMENSION TH(1500),AZ(1500),ALPH(1500),R(1500),PHI(1500), 00004560
1 THETA(1500),RHO(1500),D(1500),ECF(750),ACP(750), 00004570
2 HED(24),XLAN(8) 00004580
COMMON TH,AZ,ALPH,R,PHI,THETA,RHO,D,ECF,ACP,ICP,HED,XLAN,TO,DT, 00004590
1 CT,DAMDA,DAMDA1,DAMDA,W0,W1,E0,E1,ANCL,A,P,XLAT,XLONG,AD, 00004600
2 SANCL,CANCL,SLAT,CLAT,RLONG,L,M,J,T,W,AMDA,AMBA,E,V,PHIQ, 00004610
3 CTH,TH,DEEL,SD,CD,CBL,SBL,COSB,SINB,TANALF,RSQ,COSAS,TAS, 00004620
4 NM,N1,N2,NW,XL,XE,RAMDA,RV,CPO,PHIQ,SFO,STH,X,SINAS,RW1, 00004630
5 SPHI,CON,XZTH,ALTH:ALO,I,XALS,JJ,KK,NO2,OPT,DELM,GANN, 00004640
6 HMIN,MSECADPLR,DEN:DPN,TT,MHR,HR,IMIN,YMIN,ISEC,TMIN,J1 00004650
COMMON NRUN,NPRLX,NDL,NOPT,NDCH,DAY,THR,TSEC,ASMTM,CHR,PI,RA1, 00004660
1 RAD,NA,NB,NC,ND,NE,RRATE,BGTO,A0,A1,XLAT1,XLONG1,TDLAY, 00004670
2 DOPLER,M,INDX,TMTP;NERL,CTIME,ASMTM,RLONG1,SLAT1,CLAT1 00004680
1 ELMLS = ALPH(IALS)*17.7778 00004690
AZMLS = AZ(IALS)*17.7778 00004700
HELD = ALPH(IALS) 00004710
HELM = (ALPH(IALS)-FLOAT(HELD))*60.0+.5 00004720
HAZD = ABS(AZ(IALS)) 00004730
HAZM = (ABS(AZ(IALS))-FLOAT(HAZD))*60.0+.5 00004740
HAZD = ISIGN(HAZD,AZ(IALS)) 00004750
RM = R(IALS)/1500 00004760
2 WRITE(6,1000)(HED(I),I=1,24) 00004770
1000 FORMAT(1H1,29X12A6/3 X12A6 ///4) 00004780
WRITE(6,1001)NRUN,M,NRUN,M,MHR,IMIN,ISEC,ALPH(IALS),MHR,TMIN,ISEC, 00004790
1 AR(IALS),HELD,HELM,MELM,ELMLS,RM,HAZD,HAZM,AZMLS,R(IALS), 00004800
2 RM,RRATE,NA,NB,NC,ND,NE 00004810
1001 FORMAT(29X8HRECORDE,58X8HDIRECTOR //10X4HDATE,62X4HDATE//10X 00004820
1 1HPASS NUMBER,I6,1H-I1,45X11HPASS NUMBER,I6,1H-I1//10X 00004830
2 9HRISE TIME,I3,5H HRS.,I3,5H MIN.,I3,5H SEC.,33X 00004840
3 13HOBJECT NUMBER//10X14HRISE ELEVATION F7,3,8H DEGREES,37X 00004850
4 9HRISE TIME,I3,5H HRS.,I3,5H MIN.,I3,5H SEC.,//10X 00004860
5 12HRISE AZIMUTH F9,3,8H DEGREES,37X14HRISE ELEVATION,I3, 00004870
6 5H DEG.,I3,7H MIN.,F10.5,5H MILS//10X11HRANGE AT T0,F10.5, 00004880
7 4H MS.,41X12HRISE AZIMUTH,I5,5H DEG.,I3,7H MIN.,F10.5, 00004890
8 5H MILS//76X11HRANGE AT T0,F8,1,4H KM.,F10.5,4H MS.,//76X 00004900
916HRANGE RATE AT T0,F10.5,5H US/S//76X19HRANGE MARK NUMBER SI1) 00004910
3 WRITE(6,1002)NRUN,NPRLX,NDL,NOPT,NDCH,NRUN,M,DAY,THR,TMIN,TSEC, 00004920
1 AMDA,BGT,DAMDA,DT,CHR,MHR,IMIN,ISEC,W0,E0,ANCL,ASMTM,RM, 00004930
2 RA1,W1,E1 00004940
1002 FORMAT(//////3 X7HTRACKER,57X11HINPUT CARDS //10X4HDATE,52X 00004950
1 6HNRUN =I6, 9H NPRLX =I6,7H NDL =I4,8H NOPT =I4, 00004960
2 8H NDCH =I6//10X8HPASS NO,I8,1H-I1,38X5HDAY =F5,0,7H THR = 00004970
3 F4,0,8H TMIN =F4,0,8H TSEC =F4,0,9H AMDA0 =F8,3//10X 00004980
4 8HREEL NO,52X6HBGTO =F9,4,9H DAMDA =F7,3,6H DT =F4,1, 00004990
5 7H CHR =F3,0//10X9HRISE TIME,I3,5H HRS.,I3,5H MIN.,I3, 00005000
6 5H SEC.,23X4HW0 =F9,4,6H E0 =F9,6,8H ANCL =F7,3, 00005010
7 9H ASMTM =F9,5//71 X11HRANGE AT T0,F10.5,4H MS.,35X6H RA1 = 00005020
8 F9,5,6H 01 =F9,5,6H E1 =IPE12,4) 00005030
4 WRITE(6,1003)NA,NB,NC,ND,NE,A,A1,RRATE,XLAT,XLONG,AD,AZTM,ALTH, 00005040

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|   |      |                 |           |            |             |                  |          |
|---|------|-----------------|-----------|------------|-------------|------------------|----------|
| 1 | 1003 | FORMAT(//10X19H | AL        | XLAT1      | XLONG1      | TDDELAY          | 00005050 |
| 1 |      | 16H             | 511,37X4H | AO         | =F9.5,6H    | A1 =15E12,4      | 00005060 |
| 2 |      | 9H              | XLONG     | =F9.5,6H   | AD =F8.2,8H | A2H =F7.3//10X8H | 00005070 |
| 3 |      | 53X6H           | AL        | =F5.1,9H   | XLAT1       | =F9.5,10H        | 00005080 |
| 4 |      | F9.5//10X8H     | STOP      | TIRE,52X8H | TDDELAY     | =F7.2 )          | 00005090 |
|   |      | RETURN          |           |            |             |                  | 00005100 |
|   |      | END             |           |            |             |                  | 00005110 |
|   |      |                 |           |            |             |                  | 00005120 |



|       |  |         |
|-------|--|---------|
| COUT3 | ORBIT PREDICTION PROGRAM-SUBROUTINE OUT3                           | 0005130 |
| C     |  | 0005135 |
|       | SUBROUTINE OUT3  | 0005140 |
|       | DIMENSION TM(1500),AZ(1500),ALPH(1500),R(1500),PHI(1500),          | 0005150 |
| 1     | THETA(1500),RHO(1500),D(1500),ECP(750),ACP(750),                   | 0005160 |
| 2     | HED(24),XLAM(5)  | 0005170 |
|       | COMMON TM,AZ,ALPH,R,PHI,THETA,RHO,D,ECP,ACP,ICP,HED,XLAM,TO,DT,    | 0005180 |
| 1     | CTO,AMDA0,AMDA1,DAMDA,W0,W1,E0,E1,ANCL,A,P,XLAT,XLONG,AD,          | 0005190 |
| 2     | SANGL,CANCL,SLAT,CLAT,RLONG,L,M,J,T,W,AMDA,AMBA,E,V,PHIG,          | 0005200 |
| 3     | CTH,TH,BELL,SD,CD,CDL,SLC,COSB,SINE,TANALF,RSQ,COSAZ,TAZ,          | 0005210 |
| 4     | NN,N1,N2,XW,XL,XE,AMDA,RW,CPO,PHIO,SP0,STH,X,SINAZ,RW1,            | 0005220 |
| 5     | SPHI,CON,AZTH,ALTH,ALO,I,IALS,JJ,KK,NQ2,OPT,DELN,GAMN,             | 0005230 |
| 6     | MMIN,MSSC,DPLR,DEN,DFN,TT,MHR,HR,IMIN,YMIN,ISEC,TMIN,J1            | 0005240 |
|       | COMMON NRUN,NPRLX,NDL,NOPT,NDCH,DAY,THR,TSEC,AZMTH,CWR,PI,RA1,     | 0005250 |
| 1     | RAD,NA,NB,NC,ND,NE,RRATE,BGT0,A0,A1,XLAT1,XLONG1,TDELAY,           | 0005260 |
| 2     | DOPLER,N,INDX,TMTP,NERL,CTIME,ASMTN,RLONG1,SLAT1,CLAT1             | 0005270 |
| 1     | NSEC = TM(1)-TM(IALS)  | 0005280 |
|       | IDT = DT   | 0005290 |
|       | N1 = 1   | 0005300 |
| 2     | N2=MIN0(N1+48,VN)  | 0005310 |
|       | WRITE(6,1000) (HED(I),I=1,24),NRUN,M,NERL,CTIME,DAY,THR,TMIN,TSEC, | 0005320 |
| 1     | AMBA,MHR,IMIN,ISEC,TMTP  | 0005330 |
| 1000  | FORMAT(1H1,29X12A6/30X12A6//50X8HPASS NO: I6,1H-11,2H -,12,6H MIN. | 0005340 |
| 1     | A6//25X29H NODAL CROSSING DATA - DAY NO.,F4.0,2H ,F4.0,            | 0005350 |
| 2     | 5H HRS.,F4.0,5H MIN.,F4.0,16H SEC. - LAMBDA = F9.3 //45X           | 0005360 |
| 3     | 11HRISE TIME -I4,5H HRS.,I4,5H MIN.,I4,5H SEC.,A4 // 9X            | 0005370 |
| 4     | 4HTIME,28X7HAZIMUTH,36X9HELEVATION,25X5HRANGE/9X4HSECT,17X,        | 0005380 |
| 5     | 7HDEGREES,15X7HRADIANS,15X7HDEGREES,15X7HRADIANS,16X3HKM, )        | 0005390 |
| 3     | DO 4 I=N1,N2   | 0005400 |
|       | AZR = AZ(I)*RAD  | 0005410 |
|       | ELR = ALPH(I)*RAD  | 0005420 |
|       | WRITE(6,1001) NSEC,AZ(I),AZR,ALPH(I),ELR,R(I)                      | 0005430 |
| 1001  | FORMAT(I13,F24.3,F22.5,F21.3,F23.5,F21.2)                          | 0005440 |
|       | NSEC = NSEC+IDT  | 0005450 |
| 4     | CONTINUE   | 0005460 |
|       | N1 = N2+1  | 0005470 |
|       | IF(N1.LE.NN) GO TO 2   | 0005480 |
|       | RETURN   | 0005490 |
|       | END  | 0005500 |



|      |  |          |
|------|--|----------|
| CPRX | ORBIT PREDICTION PROGRAM-SUBROUTINE PARALX                     | 00005510 |
| C    |  | 00005515 |
|      | SUBROUTINE PARALX  | 00005520 |
|      | DIMENSION TM(1500),AZ(1500),ALPH(1500),R(1500),PHI(1500),      | 00005530 |
| 1    | THETA(1500),RHO(1500),D(1500),BCP(750),ACP(750),               | 00005540 |
| 2    | HED(24),XLAM(9)  | 00005550 |
|      | COMMON TM,ALPH,R,PHI,THETA,RHO,D,BCP,ACP,ICP,HED,XLAM,TO,DT,   | 00005560 |
| 1    | CTO,AMDA,AMDA1,DAMDA,W0,W1,E0,E1,CANCL,A,P,XLAT,XLONG,AD,      | 00005570 |
| 2    | SANCL,CANCL,SLAT,CLAT,RLONG,LCH,J,TTW,AMDA,AMBATE,V,PHIS,      | 00005580 |
| 3    | CTH,TH,DELL,SD,CD,CDL,SDL,COSB,SINE,CANALF,RSQ,COSAZ,TAZ,      | 00005590 |
| 4    | NN,N1,N2,XH,XL,XE,RAMDA,RH,CPO,PHIO,SP0,STH,X,SINAZ,RM1,       | 00005600 |
| 5    | SPH1,CON,AZTH,ALTH,AL0,IALS,JJ,KK,N02,OPT,DELN,GAMN,           | 00005610 |
| 6    | MMIN,MSEC,DPLR,DEN,DFN,TTMHR,HR,IMIN,YMIN,ISEC,THIN,J1         | 00005620 |
|      | COMMON NRUN,NPRLX,NCL,NOPT,NDCN,DAY,THR,TSEC,AZMTH,CHR,PI,RA1, | 00005630 |
| 1    | RAD,NA,NB,NC,ND,NE,RRATE,BGT0,AD,X1,XLAT1,XLONG1,YDELAY,       | 00005640 |
| 2    | DOPLER,V,INDX,TMTP,NERL,CTIME,ASHTH,RLONG1,SLAT1,SLAT1         | 00005650 |
|      | DIMENSION PAZ(600),PEL(600),EL(3750),AZ1(3750)                 | 00005660 |
|      | EQUIVALENCE (EL,AZ),(AZ1,R(751))                               | 00005670 |
|      | NPT = 6.25*DT  | 00005680 |
|      | NPT = XPT  | 00005690 |
|      | NYRA = XPT*FLOAT(NPT)  | 00005700 |
|      | NX = 4000  | 00005710 |
|      | IF(XTRA.NE.0.0) NX = 1.0/XTRA+.3                               | 00005720 |
|      | IDT = DT   | 00005730 |
|      | LT = L-1   | 00005740 |
|      | JTOT = L-IALS  | 00005750 |
|      | IF(JTOT*IDT.LE.60) GO TO 1                                     | 00005760 |
|      | WRITE(6,1000) NRUN,M   | 00005770 |
| 1000 | FORMAT(9HOPASS NO. 17,1H-11,23H LONGER THAN 10 MINUTES)        | 00005780 |
|      | JTOT = 600/IDT   | 00005790 |
|      | LT = IALS+JTOT-1   | 00005800 |
| 1    | DO 3 I=IALS,LT   | 00005810 |
|      | J = I-IALS+1   | 00005820 |
|      | TCON = TM(I)-TO  | 00005830 |
|      | DELL = XLAM(M)-RLONG1+RAMDA*TCON                               | 00005840 |
|      | DD = COS(D(I))   | 00005850 |
|      | SD = SIN(D(I))   | 00005860 |
|      | DDL = COS(DELL)  | 00005870 |
|      | SLL = SIN(DELL)  | 00005880 |
|      | R = ATAN2(GANCL*SD,CD)   | 00005890 |
| 2    | COSE = SANCL*SLAT1+SD*CLAT1+CDL*CD+CANCL*CLAT1+SDL*SD          | 00005900 |
|      | SINE = SQRT(1.0-COSE**2)                                       | 00005910 |
|      | REL(J) = ALPH(I)-ATAN2(COSE-AD/RHO(I),SINE)/RAD                | 00005920 |
|      | COSAZ = 1.0  | 00005930 |
|      | IF(SINE.NE.0.0) COSAZ = (SANCL*SD-SLAT1*COSE)/(CLAT1*SINE)     | 00005940 |
|      | SINAZ = SIGN(SQRT(1.0-COSAZ**2),X-DELL)                        | 00005950 |
|      | PAZ(J) = AZ(I)-ATAN2(SINAZ,COSAZ)/RAD                          | 00005960 |
|      | IF(ABS(PAZ(J)).GT.180.0)PAZ(J) = PAZ(J)-SIGN(360.0,PAZ(J))     | 00005970 |
| 3    | CONTINUE   | 00005980 |
|      | JT = JTOT-1  | 00005990 |
|      | R = 0  | 00006000 |
|      | Y11 = TM(IALS)   | 00006010 |

|   |                                     |          |
|---|-------------------------------------|----------|
| 4 | DO 7 I=1,JY                         | 00006020 |
|   | J = I+IALS-1                        | 00006030 |
|   | T2 = TM(J)                          | 00006040 |
|   | T2 = T1+DT                          | 00006050 |
|   | DELAZ = (PAZ(I+1)-PAZ(I))/DT        | 00006060 |
|   | DELEL = (PEL(I+1)-PEL(I))/DT        | 00006070 |
|   | NPT1 = NPT                          | 00006080 |
|   | IF(MOD(I,NX).EQ.0) NPT1 = NPT1+1    | 00006090 |
| 5 | DO 6 J=1,NPT1                       | 00006100 |
|   | K = K+1                             | 00006110 |
|   | T12 = T11+.08                       | 00006120 |
|   | AZ1(K) = PAZ(I+1)-(T2-T11)*DELAZ    | 00006130 |
|   | EL(K) = PEL(I+1)-(T2-T12)*DELEL     | 00006140 |
|   | T21 = T12+.08                       | 00006150 |
|   | IF(T11-GE-T2)GO TO 7                | 00006160 |
| 6 | CONTINUE                            | 00006170 |
| 7 | CONTINUE                            | 00006180 |
|   | WRITE(1)NRUN,M,K,MHR,IMIN,ISEC,AMBA | 00006190 |
|   | WRITE(1)(AZ1(I),EL(I),I=1,K)        | 00006200 |
|   | RETURN                              | 00006210 |
|   | END                                 | 00006220 |

|       |   |          |
|-------|---|----------|
| QNEWT | SATELLITE PREDICTION PROGRAM-SUBROUTINE NEWT+4/26/63            | 00006230 |
| C     |   | 00006235 |
| C     | SOLUTION OF EQUATION - $Q=X-P\sin X$ - BY NEWTON-RAPHSON METHOD | 00006240 |
| C     |   | 00006245 |
| C     | SUBROUTINE NEWT(X,Y,P,Q)  | 00006250 |
| C     | Q = INITIAL GUESS   | 00006260 |
| C     | Y = SOLUTION  | 00006270 |
| 1     | NR = 0  | 00006280 |
|       | X = X   | 00006290 |
| 2     | FX = X - P * SIN(X) - Q   | 00006300 |
|       | FRX = 1.0 - P * COS(X)  | 00006310 |
|       | H = FX / FRX  | 00006320 |
| 3     | X = X - H   | 00006330 |
| 4     | IF (ABS(H/X) - .000001) 7,7,5                                   | 00006340 |
| 5     | NR = NR + 1   | 00006350 |
|       | IF (NR - 50) 2,2,6  | 00006360 |
| 6     | CONTINUE  | 00006370 |
|       | GO TO 2   | 00006380 |
| 7     | X = X   | 00006390 |
|       | RETURN  | 00006400 |
|       | END   | 00006410 |

|       |   |        |         |          |
|-------|---|--------|---------|----------|
| •     | SUBROUTINE CLEAR  |        |         | 00001000 |
| •     | SUBROUTINE TO SET FORTRAN LOCATIONS TO ZERO               |        |         | 00001010 |
| •     | CALLING SEQUENCE - CALL CLEAR(X,Y)                        |        |         | 00001020 |
| •     | THE PURPOSE OF CLEAR IS TO ZERO OUT LOCATIONS X THROUGH Y |        |         | 00001030 |
|       | CLEAR   | SAVE   | 1,4     | 00001040 |
|       |   | LDA    | 2,1     | 00001050 |
|       |   | SBA    | 3,1     | 00001060 |
|       |   | TPL    | ORDER   | 00001070 |
|       |   | LDX4   | 2,1     | 00001080 |
|       |   | STZ    | 0,4     | 00001090 |
| A2    |   | BAX4   | 1,4     | 00001100 |
|       |   |        | INCR X4 | 00001110 |
| A1    |   | CMPLX4 | 3,1     | 00001120 |
|       |   | TVC    | A2      | 00001130 |
|       |   | TZE    | A2      | 00001140 |
|       | RETURN  | CLEAR  |         | 00001150 |
| ORDER |   | LDX4   | 3,1     | 00001160 |
|       |   | LDQ    | -1,DU   | 00001170 |
|       |   | ASQ    | A1      | 00001180 |
|       |   | TFA    | A2      | 00001190 |
|       | END   |        |         | 00001200 |



|       |   |          |
|-------|---|----------|
| ROUT4 | ORBIT PREDICTION PROGRAM-SUBROUTINE OUT4                                      | 00000050 |
| C     |   | 00000055 |
|       | SUBROUTINE OUT4   | 00000060 |
|       | DIMENSION VM(1500), AZ(1500), ALPH(1500), R(1500), PHI(1500),                 | 00000070 |
| 1     | THETA(1500), RHO(1500), D(1500), BCP(150), ACP(750),                          | 00000080 |
| 2     | HED(24), XLAM(5)  | 00000090 |
|       | COMMON TM, AZ, ALPH, R, PHI, THETA, RHO, D, BCP, ACP, ICR, HED, XLAM, TO, DT, | 00000100 |
| 1     | CTO, AMDA, AMDA1, DAMDA, WO, W1, EO, E1, ANCL, A, P, XLAT, XLONG, AD,         | 00000110 |
| 2     | SANGL, CANCL, SLAT, CLAT, RLONG, L, M, J, T, W, AMDA, AMBA, E, V, PHI,        | 00000120 |
| 3     | CTH, TH, DELL, SD, CD, CDL, SDL, COSE, SINE, TANALF, RSQ, COSAZ, YAZ,         | 00000130 |
| 4     | NN, N1, N2, XH, XL, XE, RAMDA, RW, CP, PHI, SM, ISTH, X, SINAZ, RW1,          | 00000140 |
| 5     | SPHI, CON, AZTH, ALTH, ALO, I, IALS, JJ, KK, NQ, NOPT, DELN, GAMN,            | 00000150 |
| 6     | MMIN, MSEC, DPLR, DEN, DFN, TT, MHR, HR, IMIN, YMIN, ISEC, TMIN, J1           | 00000160 |
|       | COMMON NRUN, NPLX, NDL, NOPT, NDCH, DAY, THR, TSEC, AZMTH, CHR, PI, RA1,      | 00000170 |
| 1     | RADANA, VB, NC, ND, NE, RRATE, BGT, A0, A1, XLAT1, XLONG1, TDELAY,            | 00000180 |
| 2     | DOPLER, V, INDXT, MTP, NERL, CTIME, ASMTH, RLONG1, SLAT1, CLAT1               | 00000190 |
|       | IF(NN.EQ.0) RETURN  | 00000200 |
| 1     | MSEC = TM(1) - TM(IALS)   | 00000210 |
|       | IDT = DT  | 00000220 |
|       | GOVIND 2  | 00000230 |
|       | WRITE(02) MSEC, IDT, NN   | 00000240 |
|       | WRITE(02) (R(IP), IP=1, NN)   | 00000250 |
|       | WRITE(02) (AZ(IP), IP=1, NN)  | 00000260 |
|       | WRITE(02) (ALPH(IP), IP=1, NN)  | 00000270 |
|       | RETURN  | 00000280 |
|       | END   | 00000290 |
|       | ***EOF  | 00000310 |

Sample Output for the Orbit Prediction Program

ORBIT PREDICTION PROGRAM  
 RUN NO. 302-1 RISE TIME - 12 MRS. 4 MIN. 47 SEC. OBJECT NO. 2108 BLN NO. 7 4/1/66  
 EPOCH TIME = 85.018 DAYS 0 MIN. EARLY PASS  
 AZ. ANGLE EL. ANGLE AZ. ANGLE  
 DEG. MIN. DEG. MIN. DEG. MIN.  
 352 32 356 51 352 32  
 1 MIN. EARLY 4 MIN. 47 SEC. EDIT LAMBDA = 96.100 DEG.

| TIME<br>MIN. SEC. | ELEVATION<br>CNTG. PER. | AZIMUTH<br>CNTG. PER. | EL. ANGLE<br>DEG. MIN. | AZ. ANGLE<br>DEG. MIN. | RANGE<br>KM. | DOPPLER<br>K.C. | TIME<br>MIN. SEC. |
|-------------------|-------------------------|-----------------------|------------------------|------------------------|--------------|-----------------|-------------------|
| 0 40              | 5055.                   | 3392.                 | 2 38                   | 356 51                 | 1778.261     | 11.895          | 0 55              |
| 1 10              | 4539.                   | 2440.                 | 4 51                   | 352 32                 | 2031.203     | 13.541          | 1 25              |
| 1 40              | 4116.                   | 1951.                 | 7 16                   | 6 4                    | 1424.434     | 9.496           | 1 55              |
| 2 10              | 3758.                   | 1536.                 | 9 56                   | 12 35                  | 1266.489     | 8.443           | 2 20              |
| 2 30              | 3557.                   | 1251.                 | 11 48                  | 17 54                  | 1171.894     | 7.813           | 2 40              |
| 2 50              | 3521.                   | 1062.                 | 13 42                  | 24 11                  | 1088.538     | 7.297           | 3 0               |
| 3 10              | 3685.                   | 910.                  | 15 31                  | 31 30                  | 1019.209     | 6.795           | 3 20              |
| 3 30              | 4254.                   | 796.                  | 17 5                   | 39 53                  | 966.939      | 6.446           | 3 45              |
| 4 0               | 6769.                   | 708.                  | 18 33                  | 54 1                   | 926.608      | 6.177           | 4 15              |
| 4 30              | 643377.                 | 680.                  | 18 34                  | 68 44                  | 936.690      | 6.245           | 4 45              |
| 5 0               | -7273.                  | 737.                  | 17 12                  | 82 18                  | 995.569      | 6.037           | 5 10              |
| 5 20              | -4669.                  | 849.                  | 15 46                  | 91 9                   | 1058.128     | 7.094           | 5 30              |
| 5 40              | -4093.                  | 983.                  | 14 8                   | 96 56                  | 1135.823     | 7.572           | 5 50              |
| 6 0               | -3928.                  | 1154.                 | 12 26                  | 102 43                 | 1225.727     | 8.172           | 6 15              |
| 6 30              | -3998.                  | 1418.                 | 9 56                   | 109 46                 | 1378.044     | 9.187           | 6 45              |
| 7 0               | -4269.                  | 1811.                 | 7 36                   | 115 18                 | 1545.585     | 10.304          | 7 15              |
| 7 30              | -4644.                  | 2282.                 | 5 27                   | 119 41                 | 1723.716     | 11.491          | 7 50              |
| 8 10              | -5130.                  | 2919.                 | 2 51                   | 124 15                 | 1972.364     | 13.149          | 8 30              |
| 8 50              | -5693.                  | 3770.                 | 0 3                    | 127 47                 | 2229.388     | 14.863          | 8 55              |
| 9 0               | -6633.                  | -26.                  | 0 0                    | 0 0                    | 0.           | 0.              |                   |

1 MIN EARLY      OBJECT NO. 2108 BLTN NO. 7      ORBIT PREDICTION PROGRAM  
4/1/66

# RECORDER

DATE  
PASS NUMBER 302-1  
RISE TIME 12 HRS. 4 MIN. 47 SEC.  
RISE ELEVATION 0.003 DEGREES  
RISE AZIMUTH 352.53 DEGREES  
RANGE AT TO 13.54135 MS.

# DIRECTOR

DATE  
PASS NUMBER 302-1  
OBJECT NUMBER  
RISE TIME 12 HRS. 4 MIN. 47 SEC.  
RISE ELEVATION 0 DEG. 0 MIN. , 0.04861 MILS  
RISE AZIMUTH 352 DEG. 32 MIN. , 6267.21478 MILS  
RANGE AT TO 2031.2 KM. 13.54135 MS.  
RANGE RATE AT TO -0.30566 US/S  
RANGE MARK NUMBER 11620

# TRACKER

DATE  
PASS NO. 302-1  
REEL NO.  
RISE TIME 12 HRS. 4 MIN. 47 SEC.  
RANGE AT TO 13.54135 MS.  
RANGE MARK NUMBER 11620  
RANGE RATE AT TO -0.3566 US/S  
HELIDIAL  
STOP TIME

# INPUT CARDS

NRUN = 302 NPRUX = 0 NDL = 1 NOPT = 10 NOCH = -10  
DAY = 91. THR = 8. TMIN = 32. TSEC = 57. AMDAO = 96.100  
BGT0 = 86.0184 DAMDA = 0. DT = 5.0 CHR = 4.  
W0 = 58.0700 E0 = 0.021690 ANCL = 72.090 ASMTM = 15.67614  
RA1 = -2.52168 W1 = -2.16126 E1 = -2.4600E-04  
A0 = 1.05752 A1 = -2.6600E-04  
XLAT = 43.15250 XLONG = 0. AD = 6365.30 AZTM = 0.100  
ALTM = 0.100 ALD = 0. XLAT1 = 0. XLONG1 = 0.  
TDELAY = 25.00



1 MIN EARLY OBJECT NO. 2188 BLTN NO. 3 4/1986

RASS NO. 302-1 - 0 MIN. EARLY

NODAL CROSSING DATA - DAY NO. 91. , 8. HRS. 32. MIN. 57. SEC. - LAMBDA = 96.100

RISE TIME - 12 HRS. 4 MIN. 47 SEC. EDT

| TIME<br>SEC. | DEGREES | AZIMUTH | RADIANS | DEGREES | ELEVATION | RADIANS | RANGE<br>KM. |
|--------------|---------|---------|---------|---------|-----------|---------|--------------|
| 5            | 352.530 |         | 6.15282 | 0.003   |           | 0.00005 | 2031.20      |
| 10           | 353.011 |         | 6.16121 | 0.316   |           | 0.00952 | 1999.07      |
| 15           | 353.507 |         | 6.16986 | 0.634   |           | 0.01106 | 1967.08      |
| 20           | 354.019 |         | 6.17880 | 0.956   |           | 0.01669 | 1935.81      |
| 25           | 354.547 |         | 6.18802 | 1.283   |           | 0.02239 | 1903.20      |
| 30           | 355.093 |         | 6.19754 | 1.615   |           | 0.02818 | 1871.94      |
| 35           | 355.657 |         | 6.20738 | 1.951   |           | 0.03406 | 1840.54      |
| 40           | 356.240 |         | 6.21755 | 2.293   |           | 0.04002 | 1809.31      |
| 45           | 356.842 |         | 6.22808 | 2.640   |           | 0.04608 | 1778.26      |
| 50           | 357.466 |         | 6.23896 | 2.993   |           | 0.05224 | 1747.41      |
| 55           | 358.112 |         | 6.25024 | 3.351   |           | 0.05849 | 1716.75      |
| 60           | 358.782 |         | 6.26192 | 3.715   |           | 0.06484 | 1686.32      |
| 65           | 359.475 |         | 6.27401 | 4.085   |           | 0.07130 | 1656.11      |
| 70           | 360.196 |         | 0.00342 | 4.461   |           | 0.07786 | 1626.14      |
| 75           | 360.941 |         | 0.01642 | 4.843   |           | 0.08453 | 1596.42      |
| 80           | 361.715 |         | 0.02994 | 5.232   |           | 0.09131 | 1566.98      |
| 85           | 362.520 |         | 0.04398 | 5.627   |           | 0.09821 | 1537.83      |
| 90           | 363.355 |         | 0.05856 | 6.028   |           | 0.10522 | 1508.97      |
| 95           | 364.224 |         | 0.07372 | 6.437   |           | 0.11234 | 1480.44      |
| 100          | 365.127 |         | 0.08948 | 6.851   |           | 0.11958 | 1452.26      |
| 105          | 366.067 |         | 0.10588 | 7.273   |           | 0.12693 | 1424.43      |
| 110          | 367.045 |         | 0.12293 | 7.701   |           | 0.13440 | 1397.00      |
| 115          | 368.063 |         | 0.14072 | 8.135   |           | 0.14199 | 1369.97      |
| 120          | 369.123 |         | 0.15923 | 8.576   |           | 0.14968 | 1343.38      |
| 125          | 370.228 |         | 0.17851 | 9.023   |           | 0.15748 | 1317.25      |
| 130          | 371.379 |         | 0.19860 | 9.476   |           | 0.16535 | 1291.61      |
| 135          | 372.578 |         | 0.21954 | 9.934   |           | 0.17338 | 1266.49      |
| 140          | 373.829 |         | 0.24136 | 10.397  |           | 0.18146 | 1241.92      |
| 145          | 375.132 |         | 0.26411 | 10.864  |           | 0.18961 | 1217.94      |
| 150          | 376.491 |         | 0.28782 | 11.335  |           | 0.19783 | 1194.59      |
| 155          | 377.913 |         | 0.31253 | 11.808  |           | 0.20609 | 1171.89      |
| 160          | 379.382 |         | 0.33827 | 12.282  |           | 0.21437 | 1149.90      |
| 165          | 380.918 |         | 0.36509 | 12.757  |           | 0.22266 | 1128.65      |
| 170          | 382.518 |         | 0.39311 | 13.231  |           | 0.23092 | 1108.18      |
| 175          | 384.182 |         | 0.42206 | 13.701  |           | 0.23913 | 1088.54      |
| 180          | 385.913 |         | 0.45226 | 14.167  |           | 0.24725 | 1069.77      |
| 185          | 387.710 |         | 0.48363 | 14.625  |           | 0.25525 | 1051.93      |
| 190          | 389.575 |         | 0.51618 | 15.074  |           | 0.26308 | 1035.06      |
| 195          | 391.517 |         | 0.54990 | 15.510  |           | 0.27070 | 1019.21      |
| 200          | 393.535 |         | 0.58478 | 15.932  |           | 0.27806 | 1004.42      |
| 205          | 395.569 |         | 0.62080 | 16.336  |           | 0.28511 | 990.75       |
| 210          | 397.697 |         | 0.65793 | 16.719  |           | 0.29180 | 978.24       |
| 215          | 399.884 |         | 0.69611 | 17.077  |           | 0.29806 | 966.94       |
| 220          | 402.129 |         | 0.73529 | 17.409  |           | 0.30384 | 956.89       |
| 225          | 404.425 |         | 0.77537 | 17.710  |           | 0.30910 | 948.12       |
| 230          | 406.769 |         | 0.81627 | 18.000  |           | 0.31377 | 940.88       |
| 235          | 409.152 |         | 0.85787 | 18.209  |           | 0.31781 | 934.80       |
| 240          | 411.569 |         | 0.90005 | 18.402  |           | 0.32118 | 929.90       |
| 245          | 414.012 |         | 0.94268 | 18.555  |           | 0.32384 | 926.61       |

1 MIN EARLY ORBIT PREDICTION PROGRAM  
 OBJECT NO. 2108 RLTY NO. 7 4/1/66  
 PASS NO. 302-1 - 3 MIN. EARLY  
 NODAL CROSSING DATA - DAY NO. 91. , 8. HRS. 32. MIN. 57. SEC. - LAMBDA = 96.100  
 RISE TIME - 12 HRS. 4 MIN. 47 SEC. EDT

| TIME | DEGREES | AZIMUTH | RADIANS | DEGREES | ELEVATION | RADIANS | RANGE   |
|------|---------|---------|---------|---------|-----------|---------|---------|
| SFC. |         |         |         |         |           |         | KM.     |
| 245  | 56.472  |         | 0.98562 | 18.565  |           | 0.32577 | 924.73  |
| 251  | 58.940  |         | 1.02870 | 18.733  |           | 0.32694 | 924.28  |
| 255  | 61.4 9  |         | 1.07179 | 18.756  |           | 0.32736 | 925.26  |
| 261  | 63.868  |         | 1.11471 | 18.737  |           | 0.32792 | 927.66  |
| 265  | 66.311  |         | 1.15734 | 18.674  |           | 0.32593 | 931.48  |
| 271  | 68.727  |         | 1.19951 | 18.570  |           | 0.32411 | 936.69  |
| 275  | 71.110  |         | 1.24111 | 18.426  |           | 0.32160 | 943.27  |
| 281  | 73.453  |         | 1.28199 | 18.245  |           | 0.31843 | 951.19  |
| 285  | 75.748  |         | 1.32206 | 18.028  |           | 0.31465 | 960.42  |
| 291  | 77.992  |         | 1.36121 | 17.779  |           | 0.31030 | 970.93  |
| 295  | 8 178   |         | 1.39938 | 17.500  |           | 0.30544 | 982.65  |
| 301  | 82.3 4  |         | 1.43648 | 17.195  |           | 0.30010 | 995.57  |
| 305  | 84.367  |         | 1.47248 | 16.866  |           | 0.29436 | 1009.62 |
| 311  | 86.364  |         | 1.5 734 | 16.516  |           | 0.28826 | 1024.76 |
| 315  | 88.294  |         | 1.54183 | 16.149  |           | 0.28185 | 1040.95 |
| 321  | 9 157   |         | 1.57354 | 15.767  |           | 0.27518 | 1058.13 |
| 325  | 91.953  |         | 1.61488 | 15.372  |           | 0.26830 | 1076.25 |
| 331  | 93.681  |         | 1.63505 | 14.968  |           | 0.26124 | 1095.27 |
| 335  | 95.344  |         | 1.66486 | 14.556  |           | 0.25405 | 1115.15 |
| 341  | 96.941  |         | 1.69194 | 14.138  |           | 0.24675 | 1135.82 |
| 345  | 98.476  |         | 1.71872 | 13.716  |           | 0.23939 | 1157.26 |
| 351  | 99.949  |         | 1.74443 | 13.292  |           | 0.23198 | 1179.42 |
| 355  | 1 1.362 |         | 1.76910 | 12.865  |           | 0.22456 | 1202.25 |
| 361  | 1 2.718 |         | 1.79277 | 12.441  |           | 0.21713 | 1225.73 |
| 365  | 1 4.019 |         | 1.81547 | 12.017  |           | 0.20973 | 1249.80 |
| 371  | 1 5.266 |         | 1.83724 | 11.595  |           | 0.20236 | 1274.44 |
| 375  | 1 6.463 |         | 1.85813 | 11.175  |           | 0.19504 | 1299.62 |
| 381  | 1 7.611 |         | 1.87817 | 10.759  |           | 0.18779 | 1325.30 |
| 385  | 1 8.713 |         | 1.89740 | 10.347  |           | 0.18059 | 1351.45 |
| 391  | 1 9.770 |         | 1.91585 | 9.940   |           | 0.17348 | 1378.04 |
| 395  | 11. 785 |         | 1.93356 | 9.536   |           | 0.16644 | 1405.06 |
| 401  | 111.760 |         | 1.95058 | 9.138   |           | 0.15949 | 1432.47 |
| 405  | 112.696 |         | 1.96692 | 8.745   |           | 0.15263 | 1460.24 |
| 411  | 113.596 |         | 1.98262 | 8.357   |           | 0.14586 | 1488.37 |
| 415  | 114.461 |         | 1.99772 | 7.974   |           | 0.13918 | 1516.82 |
| 421  | 115.293 |         | 2.01224 | 7.597   |           | 0.13259 | 1545.59 |
| 425  | 116.093 |         | 2.02621 | 7.225   |           | 0.12610 | 1574.64 |
| 431  | 116.864 |         | 2.03966 | 6.858   |           | 0.11970 | 1603.97 |
| 435  | 117.6 6 |         | 2.05262 | 6.497   |           | 0.11339 | 1633.55 |
| 441  | 118.321 |         | 2.06510 | 6.141   |           | 0.10718 | 1663.38 |
| 445  | 119.011 |         | 2.07713 | 5.790   |           | 0.10105 | 1693.44 |
| 451  | 119.676 |         | 2.08874 | 5.444   |           | 0.09501 | 1723.72 |
| 455  | 12 317  |         | 2.09994 | 5.103   |           | 0.08906 | 1754.19 |
| 461  | 12. 937 |         | 2.11075 | 4.767   |           | 0.08319 | 1784.86 |
| 465  | 121.535 |         | 2.12119 | 4.435   |           | 0.07741 | 1815.72 |
| 471  | 122.114 |         | 2.13128 | 4.108   |           | 0.07170 | 1846.74 |
| 475  | 122.673 |         | 2.14154 | 3.786   |           | 0.06608 | 1877.93 |
| 481  | 123.213 |         | 2.15148 | 3.468   |           | 0.06053 | 1909.26 |
| 485  | 123.737 |         | 2.15961 | 3.154   |           | 0.05505 | 1940.75 |

ORBIT PREDICTION PROGRAM  
 1 MIN EARLY      OBJECT NO. 2108 BLTN NO. 7      4/1/66

RASS NO.      302-1 - 0 MIN. EARLY

NODAL CROSSING DATA - DAY NO. 91. , 8. HRS. 32. MIN. 57. SEC. - LAMBDA = 96.100

RISE TIME - 12 HRS. 4 MIN. 47 SEC. EDT

| TIME<br>SEC. | DEGREES | AZIMUTH | RADIANS | DEGREES | ELEVATION | RADIANS | RANGE<br>KM. |
|--------------|---------|---------|---------|---------|-----------|---------|--------------|
| 490          | 124.243 |         | 2.16845 | 2.845   |           | 0.04965 | 1972.36      |
| 495          | 124.734 |         | 2.17702 | 2.539   |           | 0.04432 | 2004.11      |
| 500          | 125.210 |         | 2.18532 | 2.238   |           | 0.03905 | 2035.98      |
| 505          | 125.671 |         | 2.19337 | 1.940   |           | 0.03385 | 2067.96      |
| 510          | 126.118 |         | 2.20117 | 1.645   |           | 0.02872 | 2100.05      |
| 515          | 126.552 |         | 2.20875 | 1.355   |           | 0.02364 | 2132.25      |
| 520          | 126.973 |         | 2.21610 | 1.067   |           | 0.01863 | 2164.54      |
| 525          | 127.382 |         | 2.22324 | 0.783   |           | 0.01367 | 2196.92      |
| 530          | 127.780 |         | 2.23018 | 0.503   |           | 0.00877 | 2229.39      |
| 535          | 128.166 |         | 2.23692 | 0.225   |           | 0.00393 | 2261.94      |

Plot from the Sample Output





*MISSION  
of  
Rome Air Development Center*

*RADC plans and conducts research, exploratory and advanced development programs in command, control, and communications (C<sup>3</sup>) activities, and in the C<sup>3</sup> areas of information sciences and intelligence. The principal technical mission areas are communications, electromagnetic guidance and control, surveillance of ground and aerospace objects, intelligence data collection and handling, information system technology, ionospheric propagation, solid state sciences, microwave physics and electronic reliability, maintainability and compatibility.*

